

THE NORTHERN PASS

# PROPOSED STRUCTURE DESIGNS

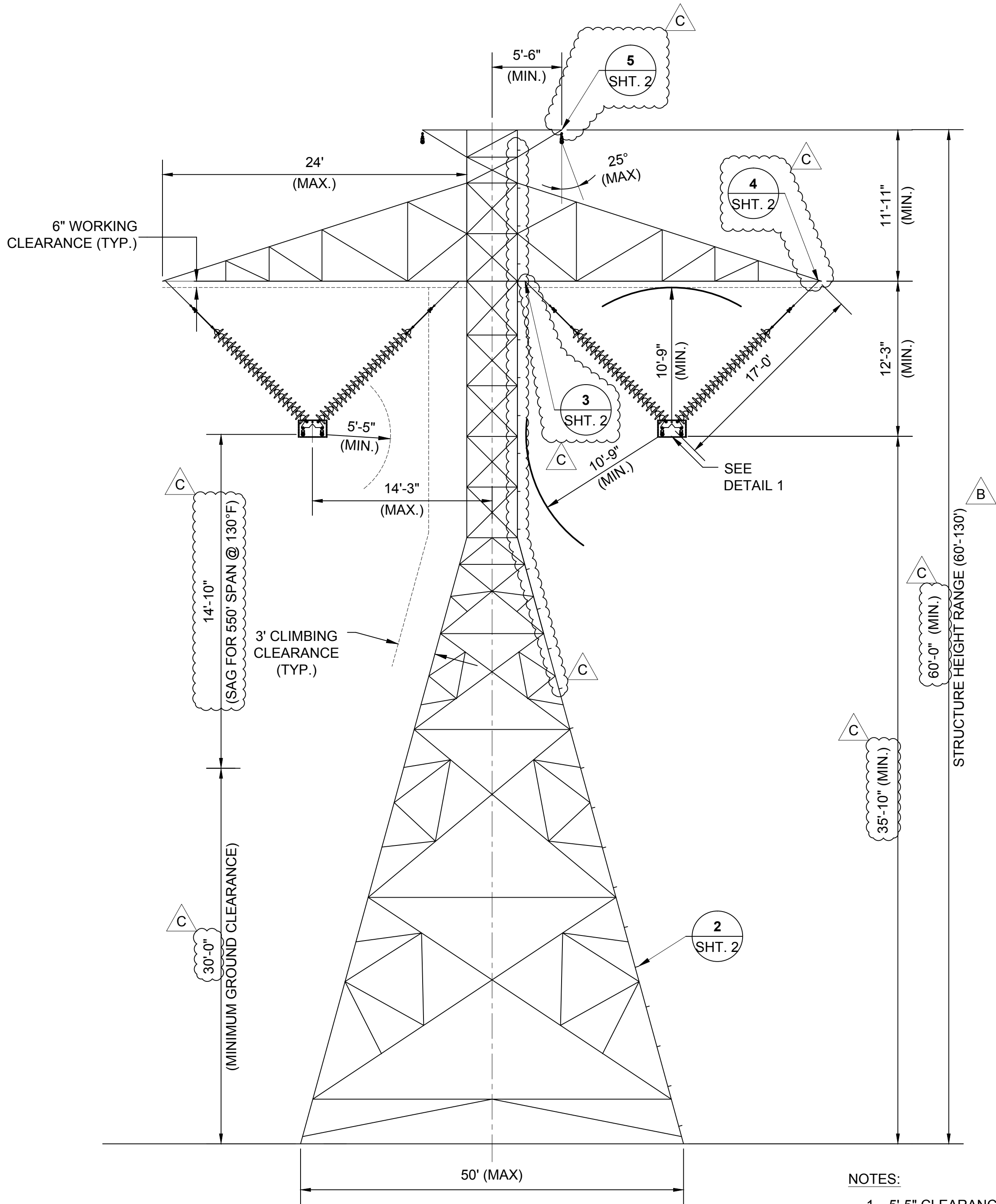
PRELIMINARY - NOT  
FOR CONSTRUCTION

A	10/8/15	ISSUED FOR PERMIT USE	MSP	DAB				
NO.	DATE	REVISIONS	BY	CHK	APP	APP		



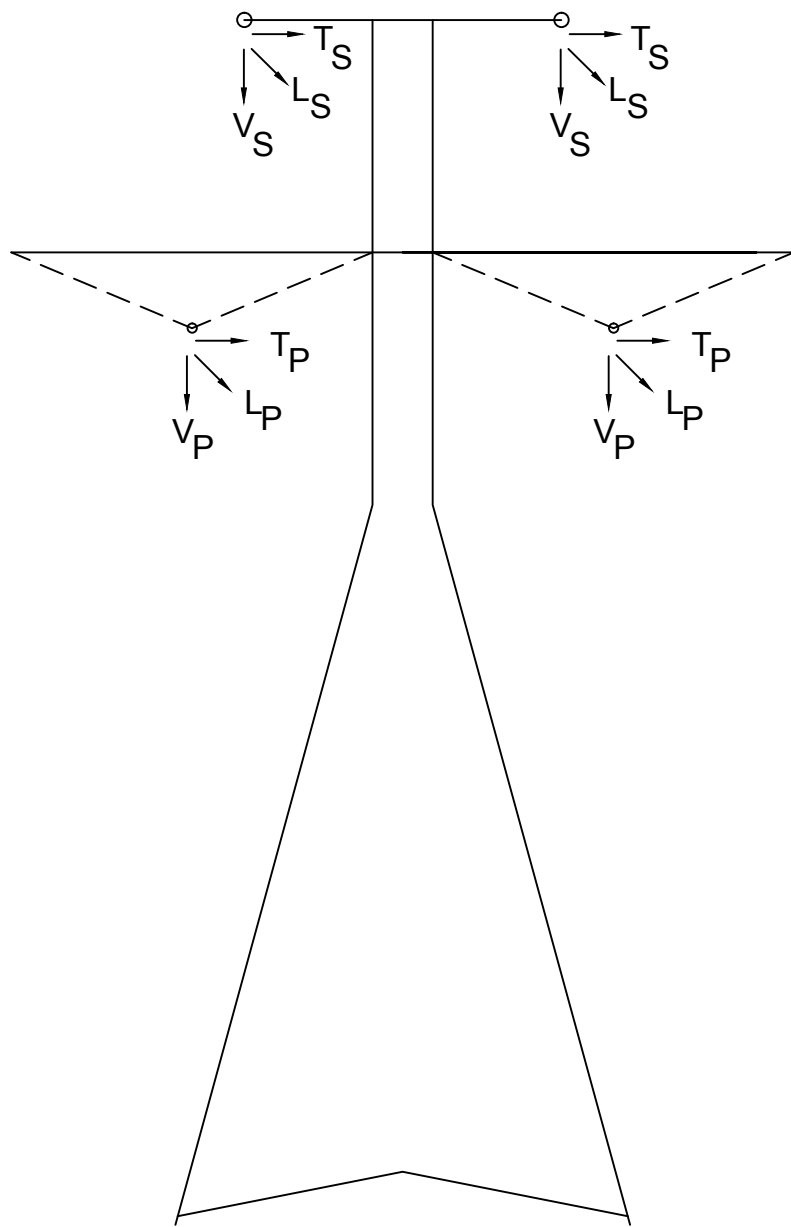
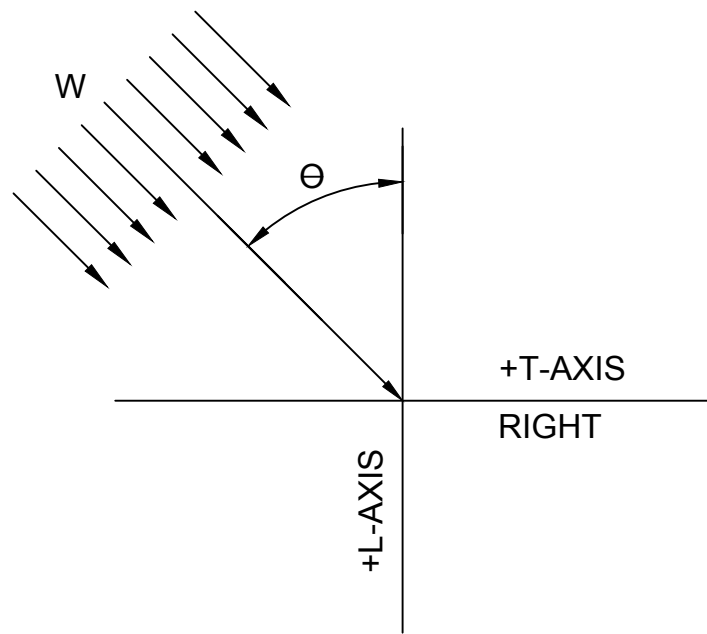
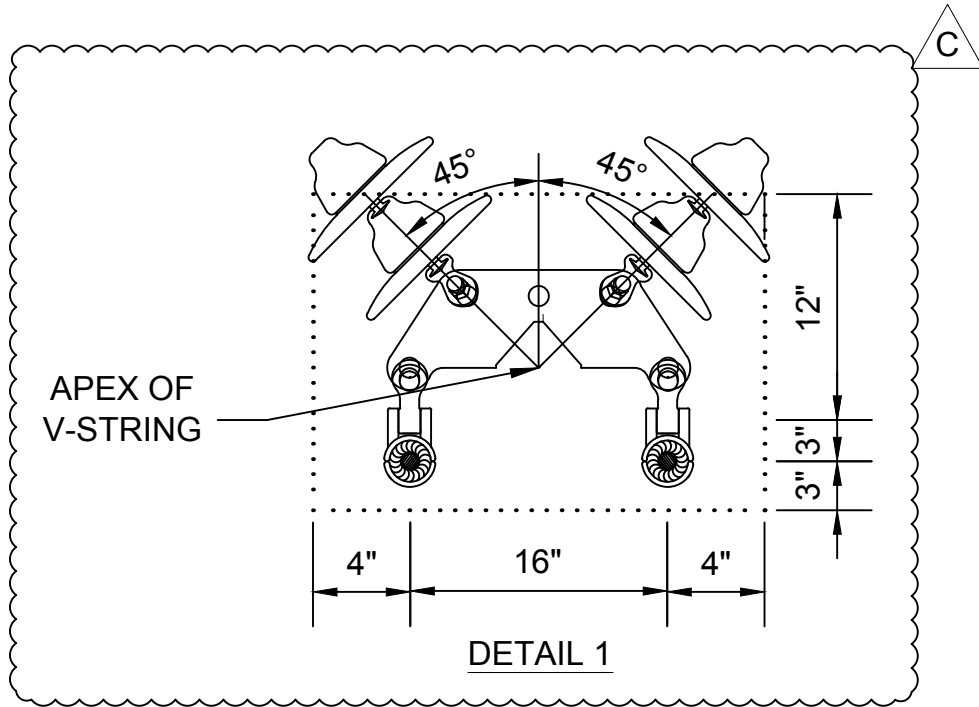
BMCD 58479





NOTES:

- 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
- 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.




LOADING TREE

STRUCTURE NAME: 32-SCHLT-LTG-002  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 550  
WEIGHT SPAN (FT): 850  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.45	1.03	0.00	13.54	5.30	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.43	0.75	0.00	5.61	5.98	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.03	0.74	0.00	12.70	3.28	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.62	1.06	0.00	17.43	4.15	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.96	0.48	0.00	9.02	2.65	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.96	0.47	0.00	9.02	2.49	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.96	0.37	5.50	9.02	1.51	24.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.58	0.27	0.27	23.61	2.17	2.27	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.66	0.21	0.00	13.01	1.66	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.43	0.46	0.00	5.61	3.67	0.00	29.00	45.00	1.00

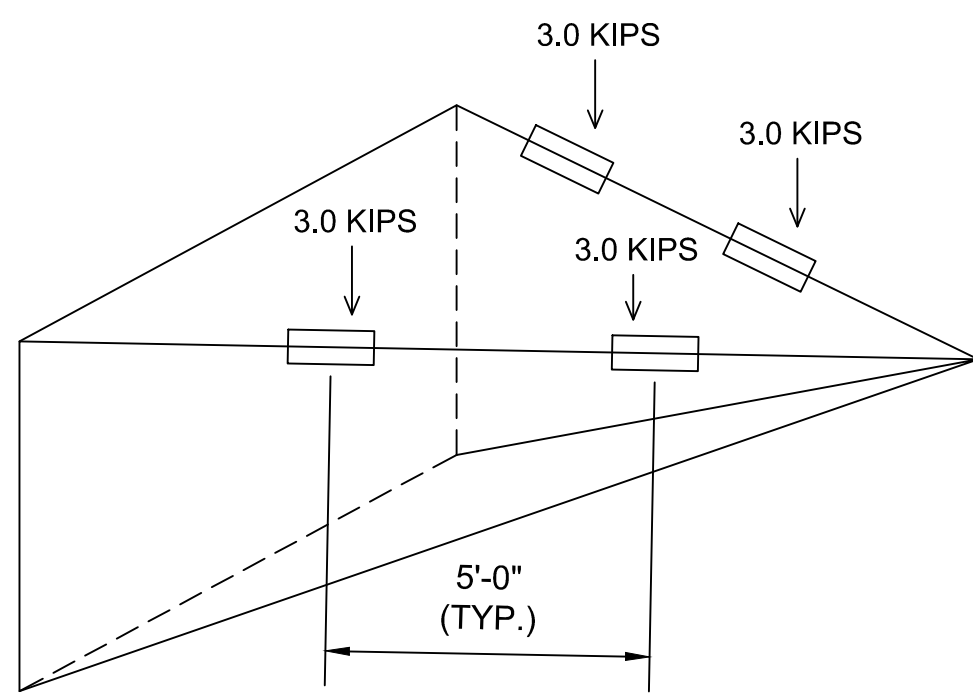
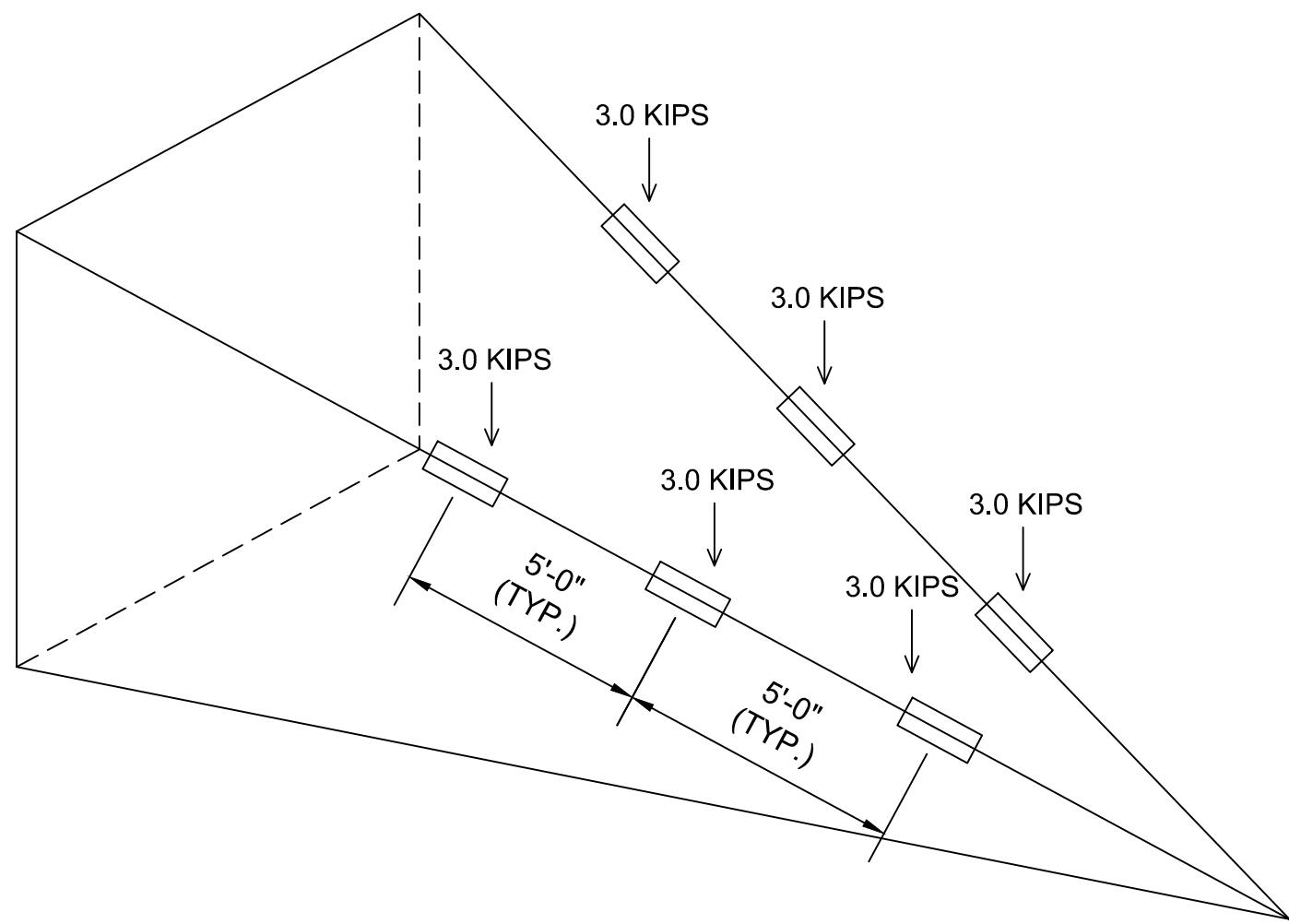
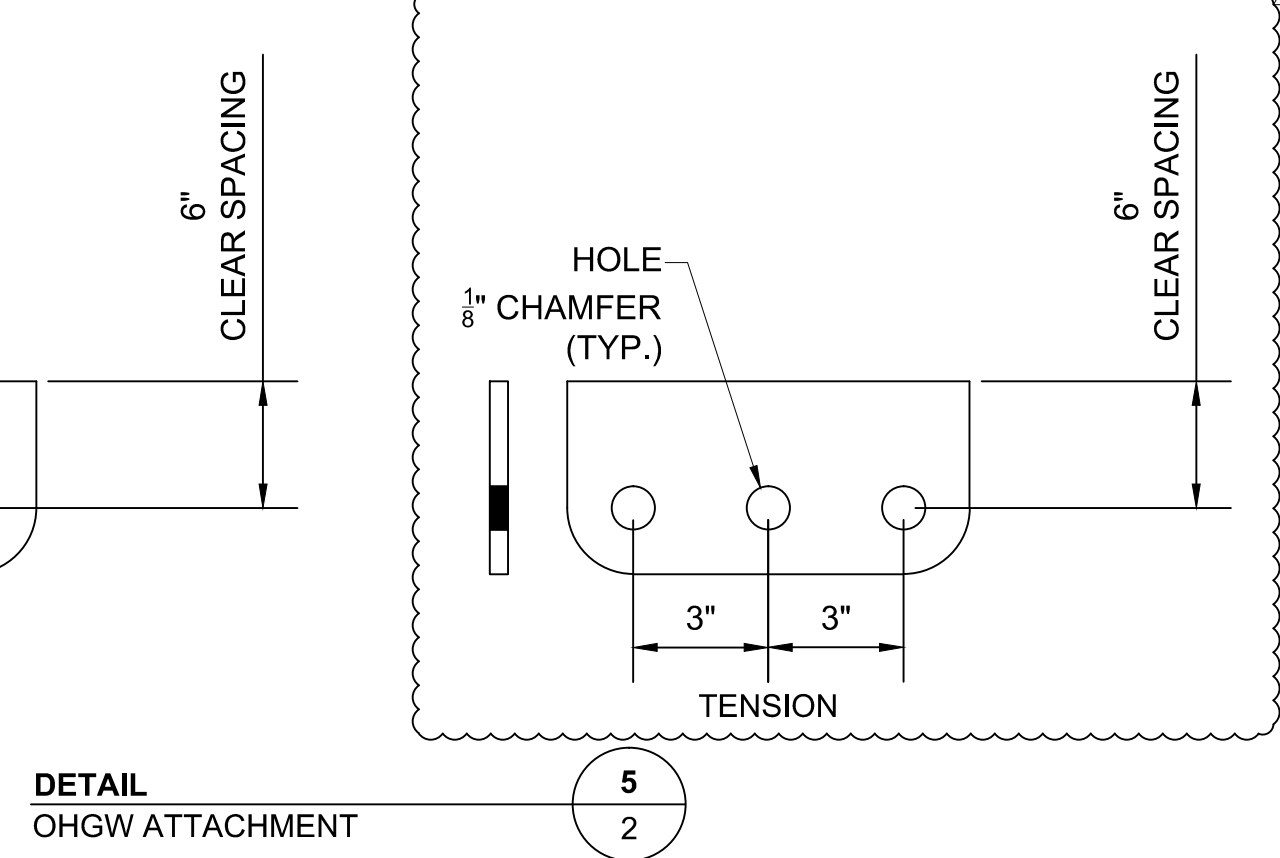
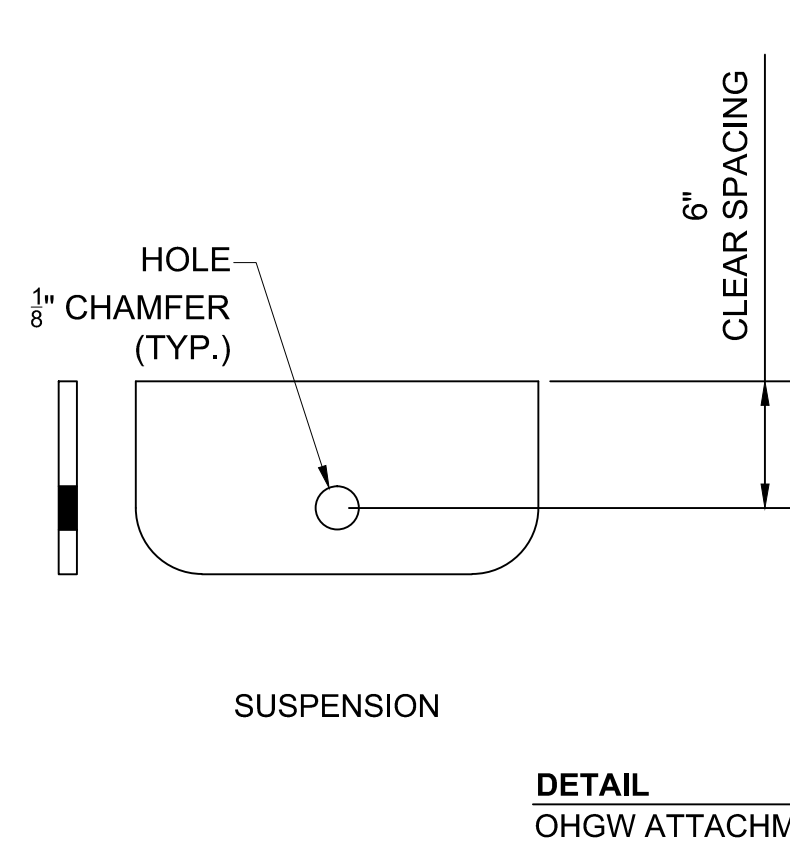
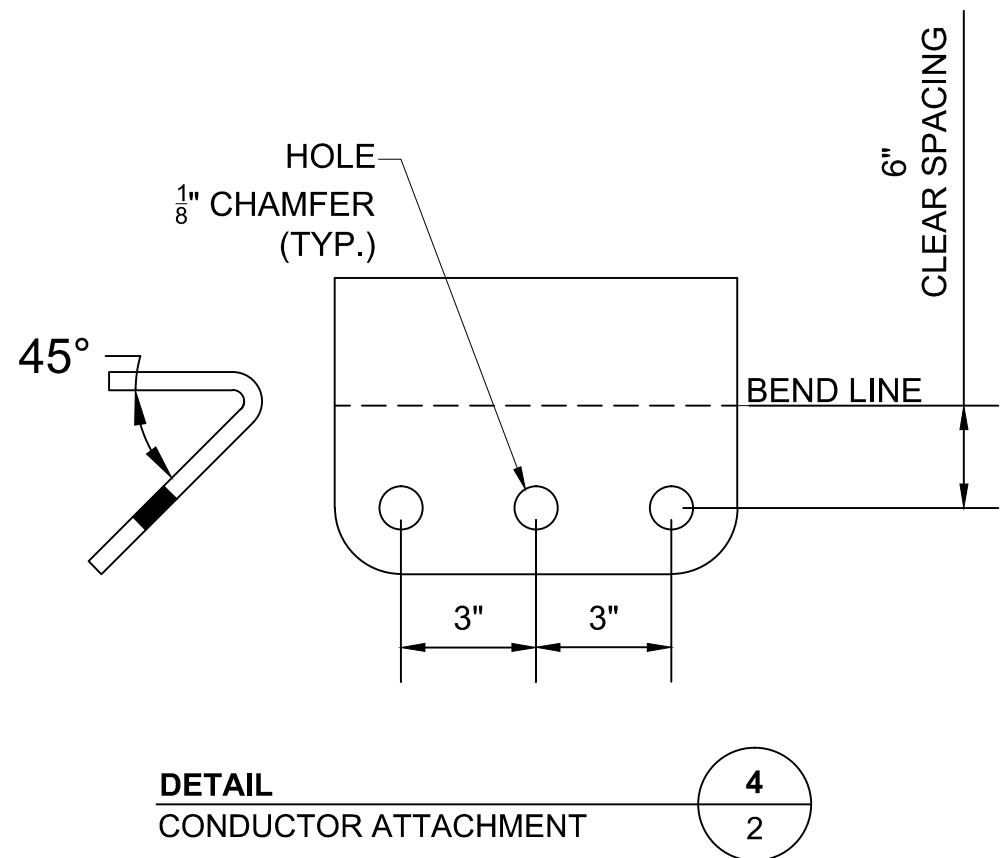
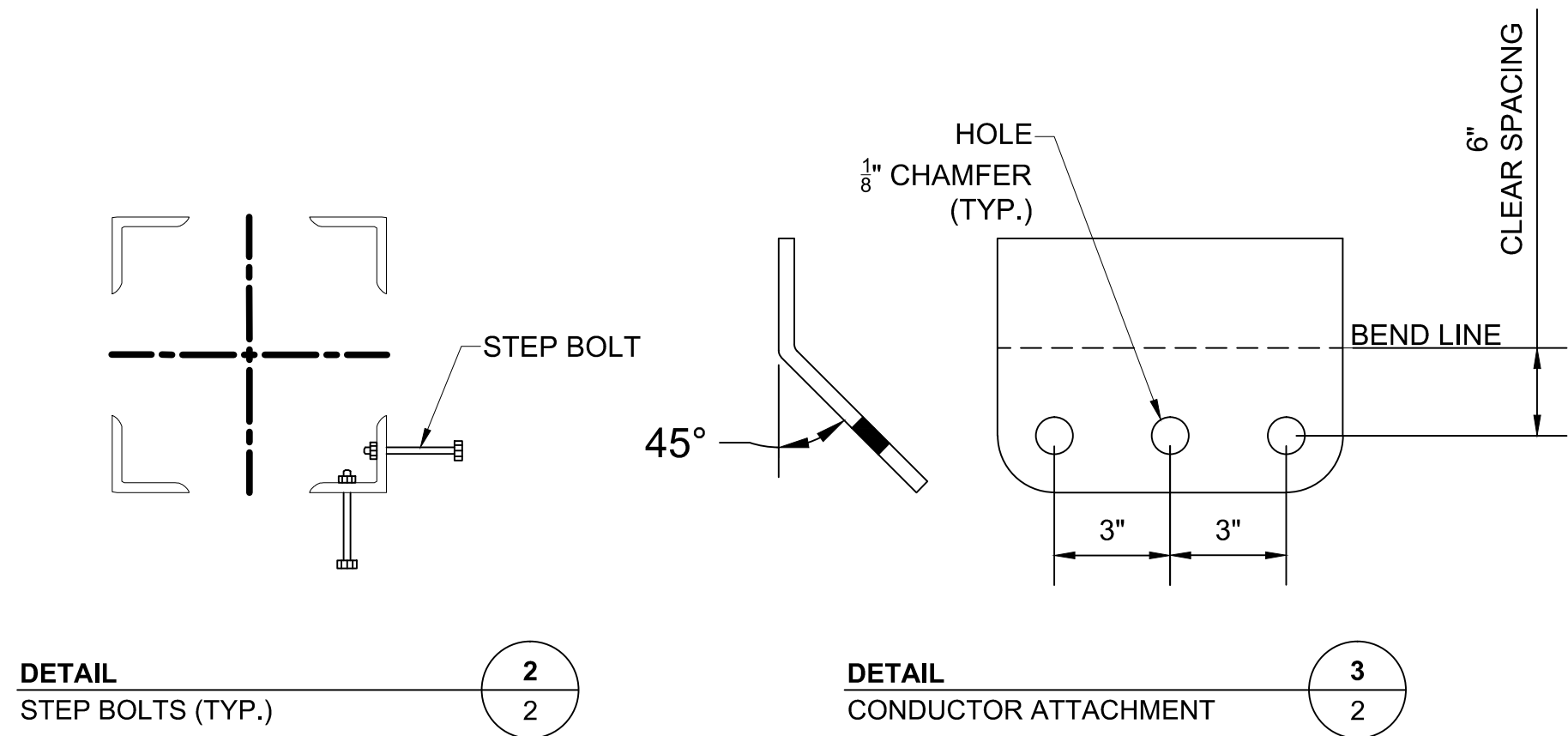
GENERAL NOTES:

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
- TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
- EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
- LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
- ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
- THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
- SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
- TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
- CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
- CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
- CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
- STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
C	MISC. REVISIONS		5/21/15	KAK			
B	UPDATED STRUCTURE HEIGHT RANGE		5/8/15	KAK			
A	RELEASED FOR RFP BID		5/1/15	KAK			
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	
 320kV DC LIGHT TANGENT 0°-2° 32-SCHLT-LTG-002 LOAD & DESIGN DRAWING							C
							DRAWN KAK
							ENGINEER AKO
							CHECKED TAB
							APPROVED
							DATE 5/1/15
SCALE NTS							FILE: LST-01-001.DWG IMAGE:
							DRAWING NO. LST-01-001

PRELIMINARY - NOT FOR CONSTRUCTION





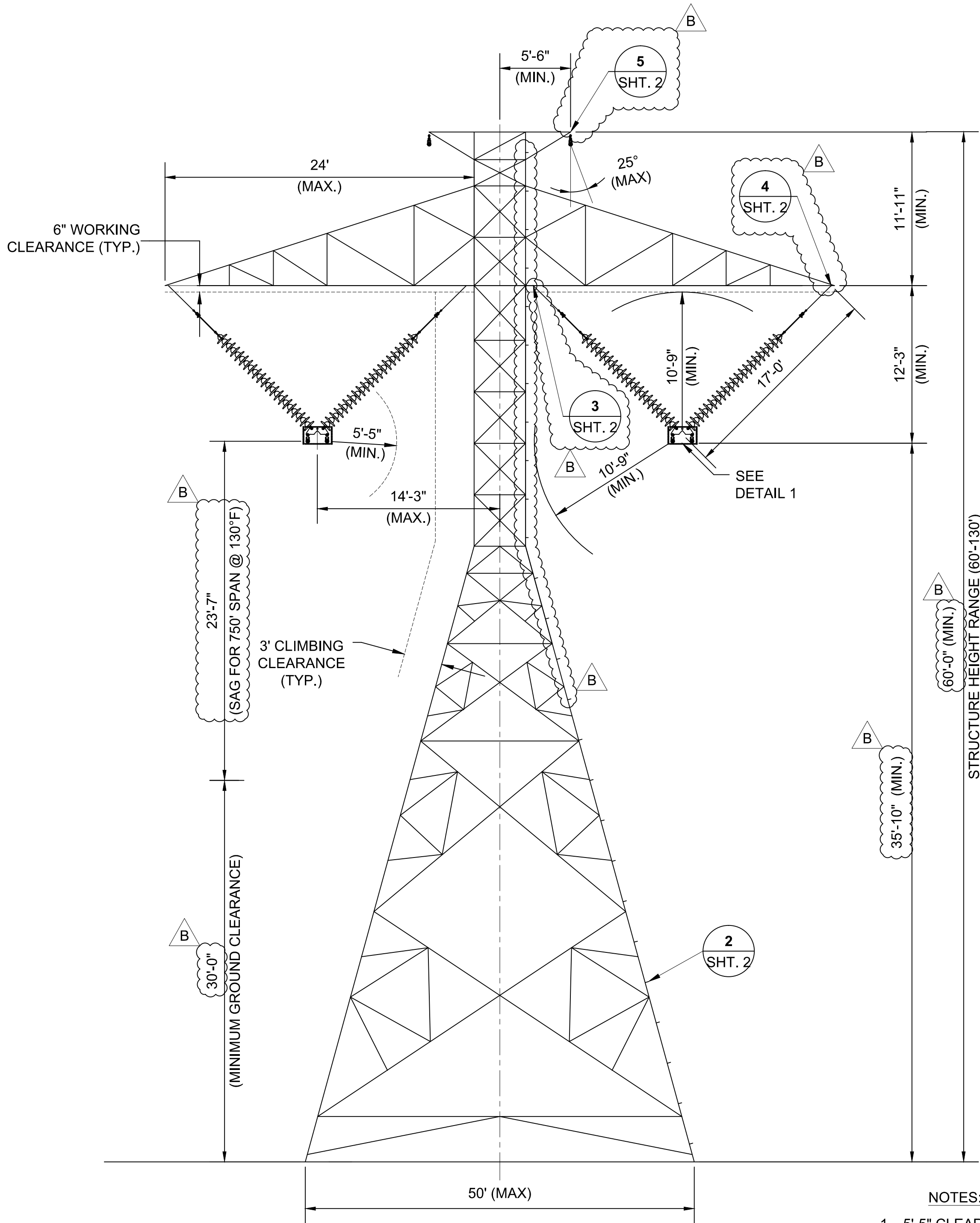
NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 5.
- FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

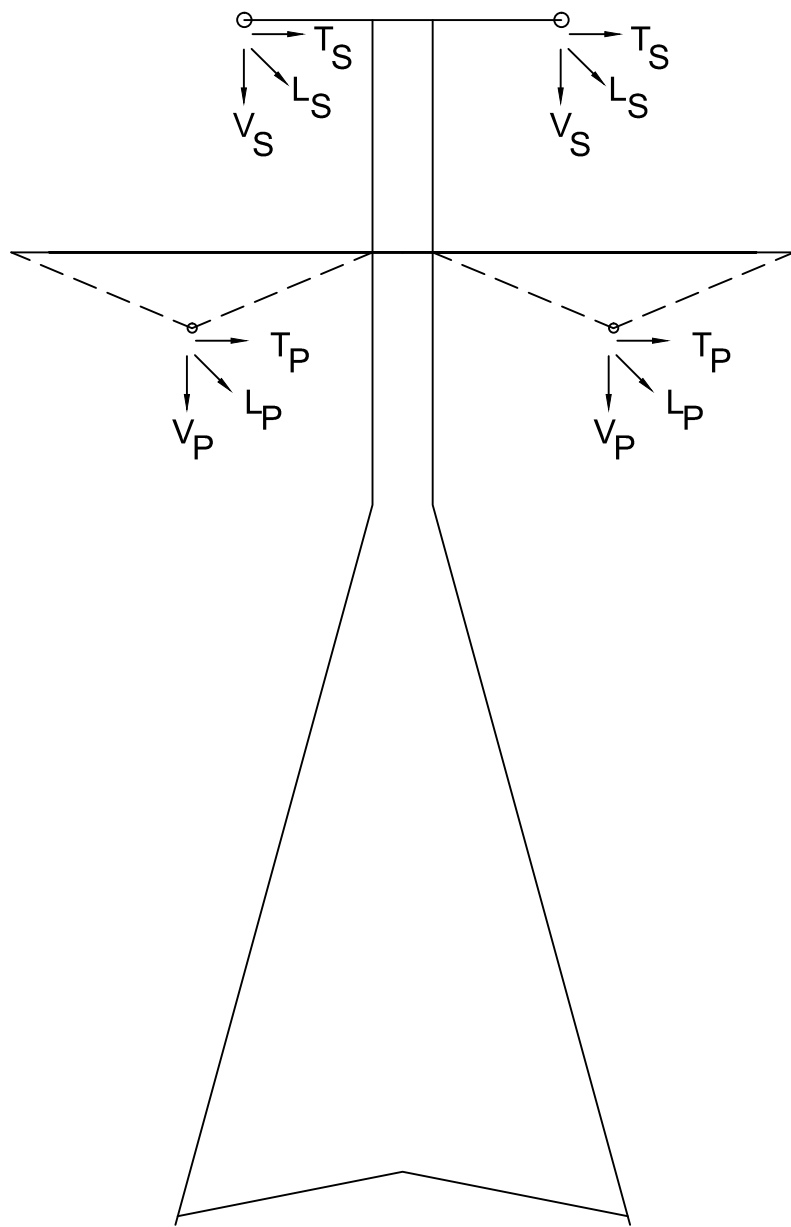
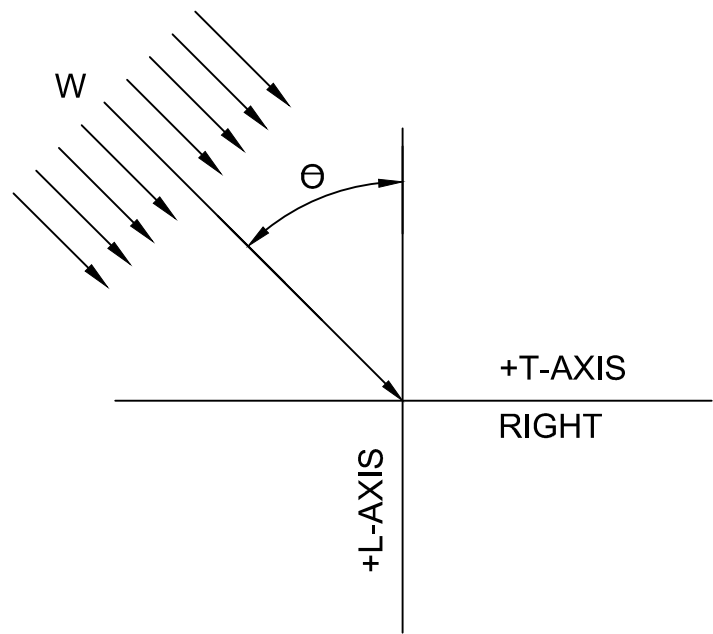
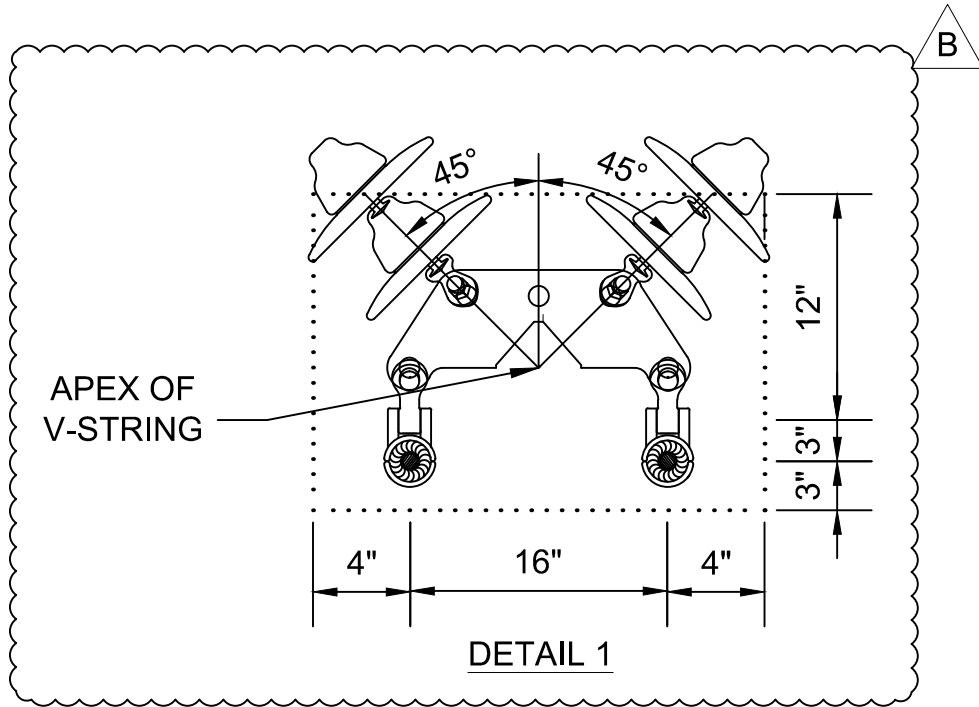
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3	NESC 250D	15.00	1.00	39.53	2.84	0.91	0.00	17.22	3.81	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	5.09	1.30	0.00	23.90	4.81	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.34	0.58	0.00	12.04	3.04	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.34	0.57	0.00	12.04	2.88	0.00	4.00	90.00	1.00
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8	CONSTRUCTION	30.00	0.00	29.97	3.82	0.30	0.27	26.51	2.40	2.27	3.45	90.00	1.50
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10	OBLIQUE WIND	60.00	0.00	100.00	0.59	0.56	0.00	7.55	4.51	0.00	29.00	45.00	1.00

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  - THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
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  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
  - CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
  - CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
  - STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
B MISC. REVISIONS 5/21/15 KAK							
A RELEASED FOR RFP BID 5/1/15 KAK							
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	

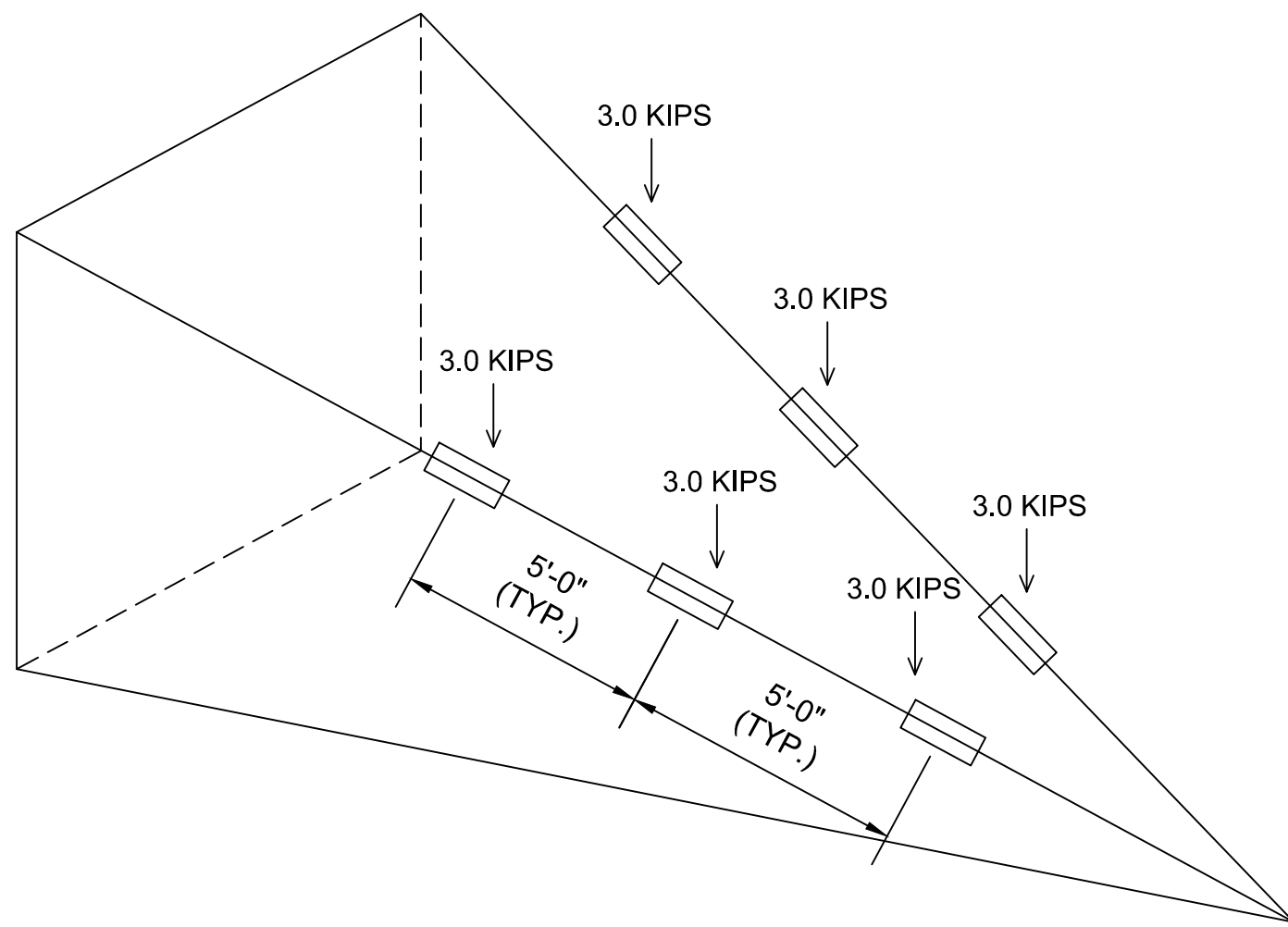
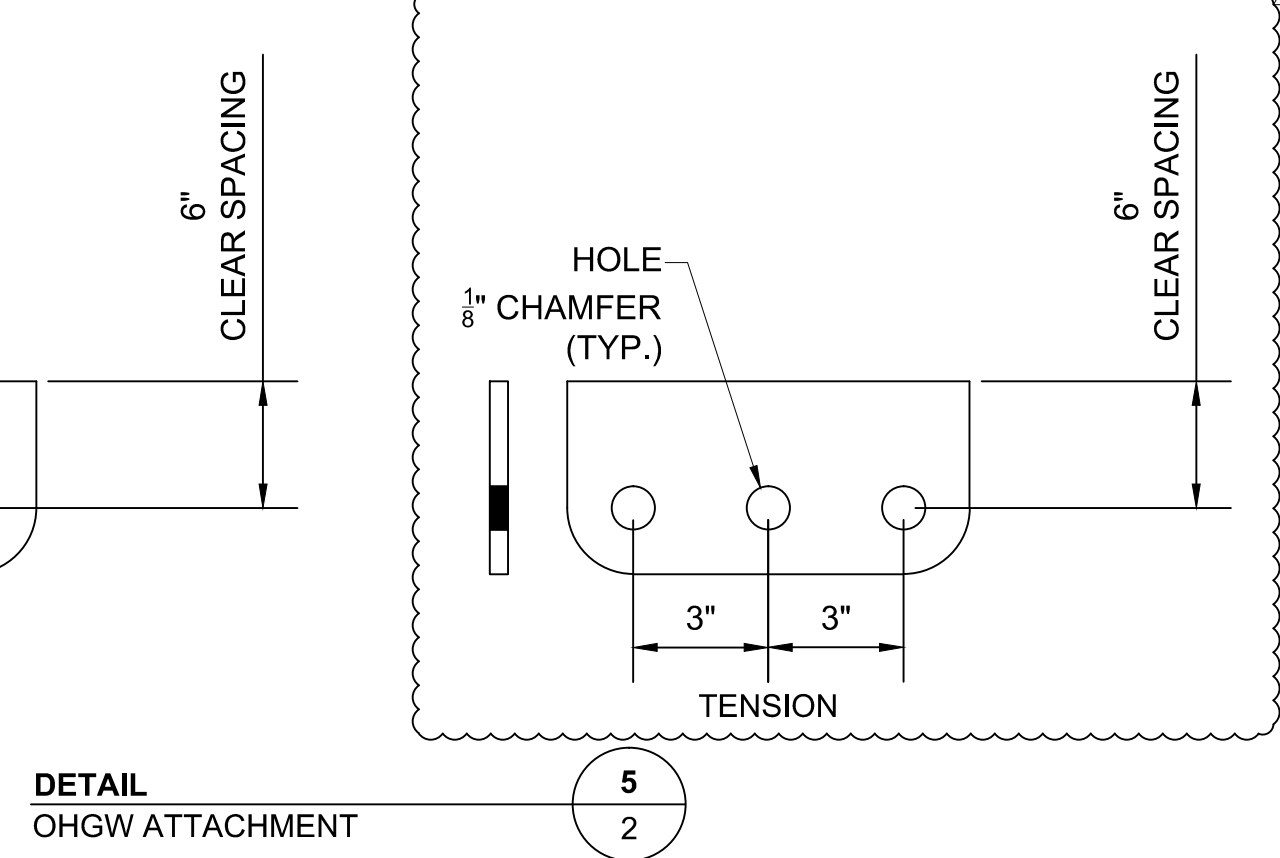
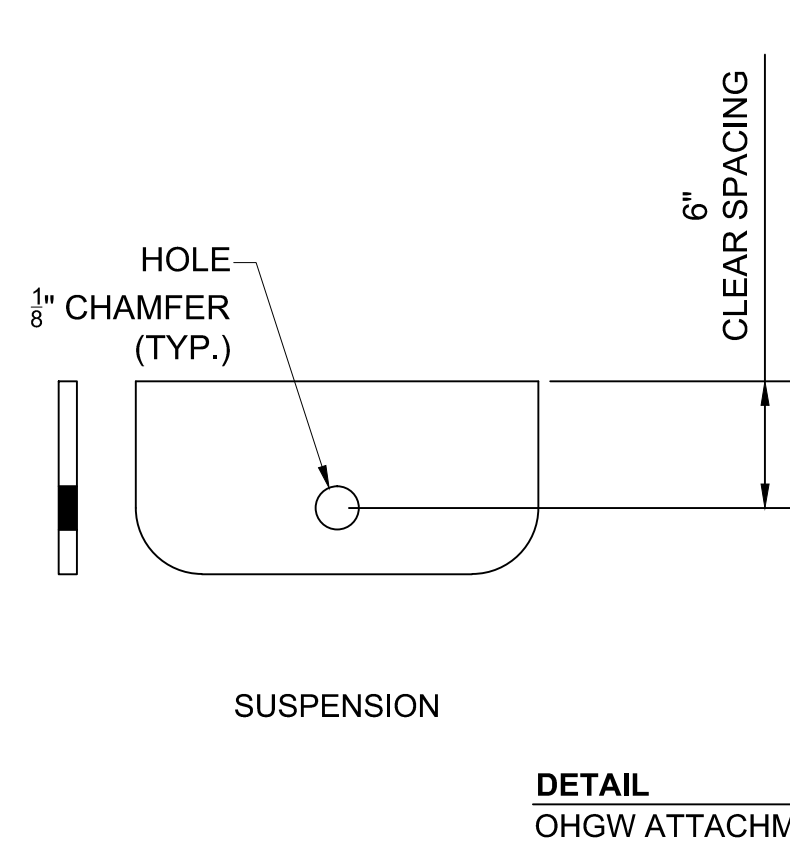
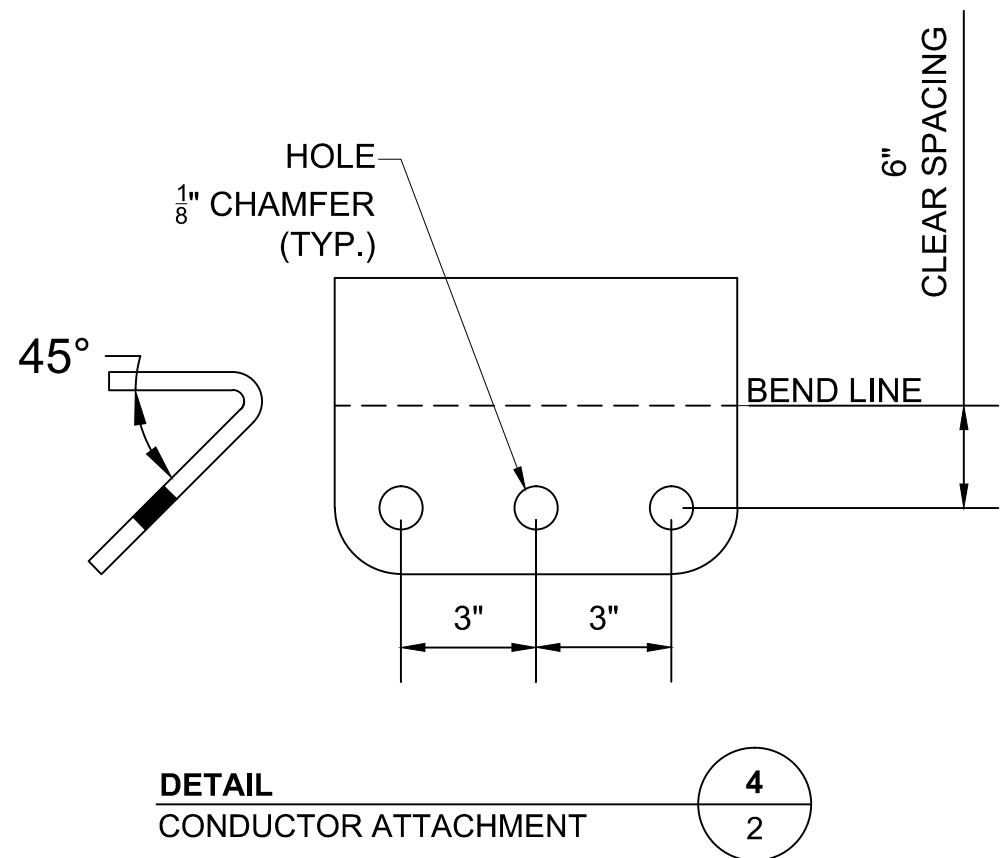
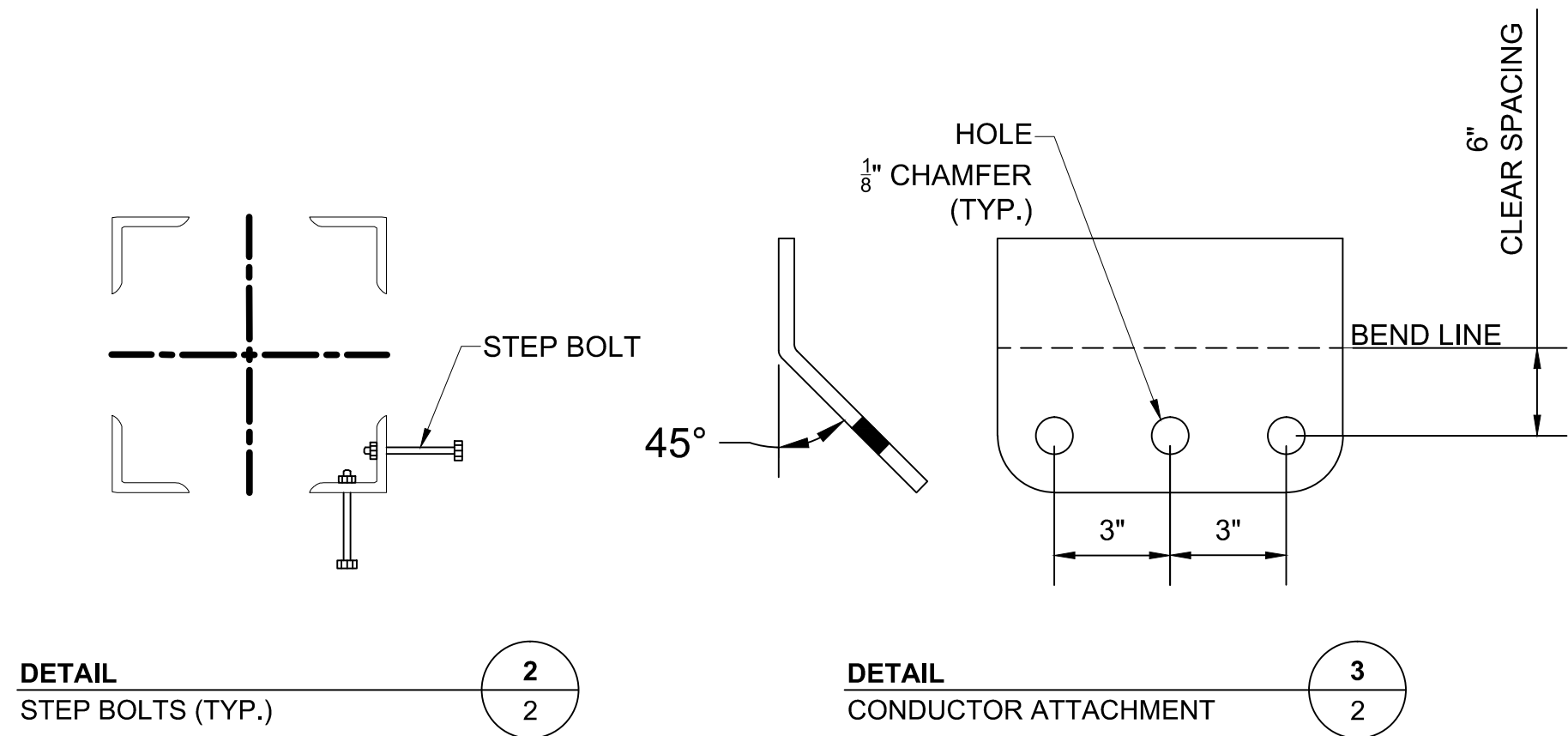
320kV DC MEDIUM TANGENT 0°-2°  
32-SCHLT-MTG-002  
LOAD & DESIGN DRAWING

SCALE NTS	FILE: LST-02-001.DWG IMAGE:	DRAWING NO. LST-02-001
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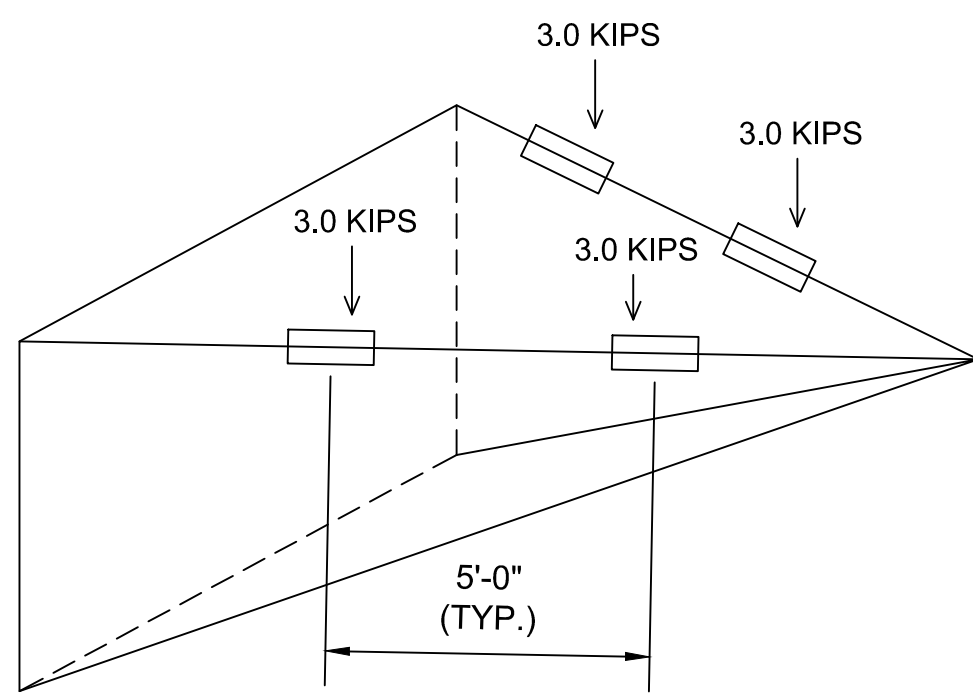
DRAWN KAK	DATE 5/1/15
ENGINEER AKO	
CHECKED TAB	
APPROVED	

PRELIMINARY - NOT  
FOR CONSTRUCTION





**DETAIL**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL  
CONDUCTOR CROSSARMS FRONT  
AND BACK, INCLUDING BOX ARMS.)



**DETAIL**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL OHSW  
CROSSARMS FRONT AND BACK,  
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NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 5.
- FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

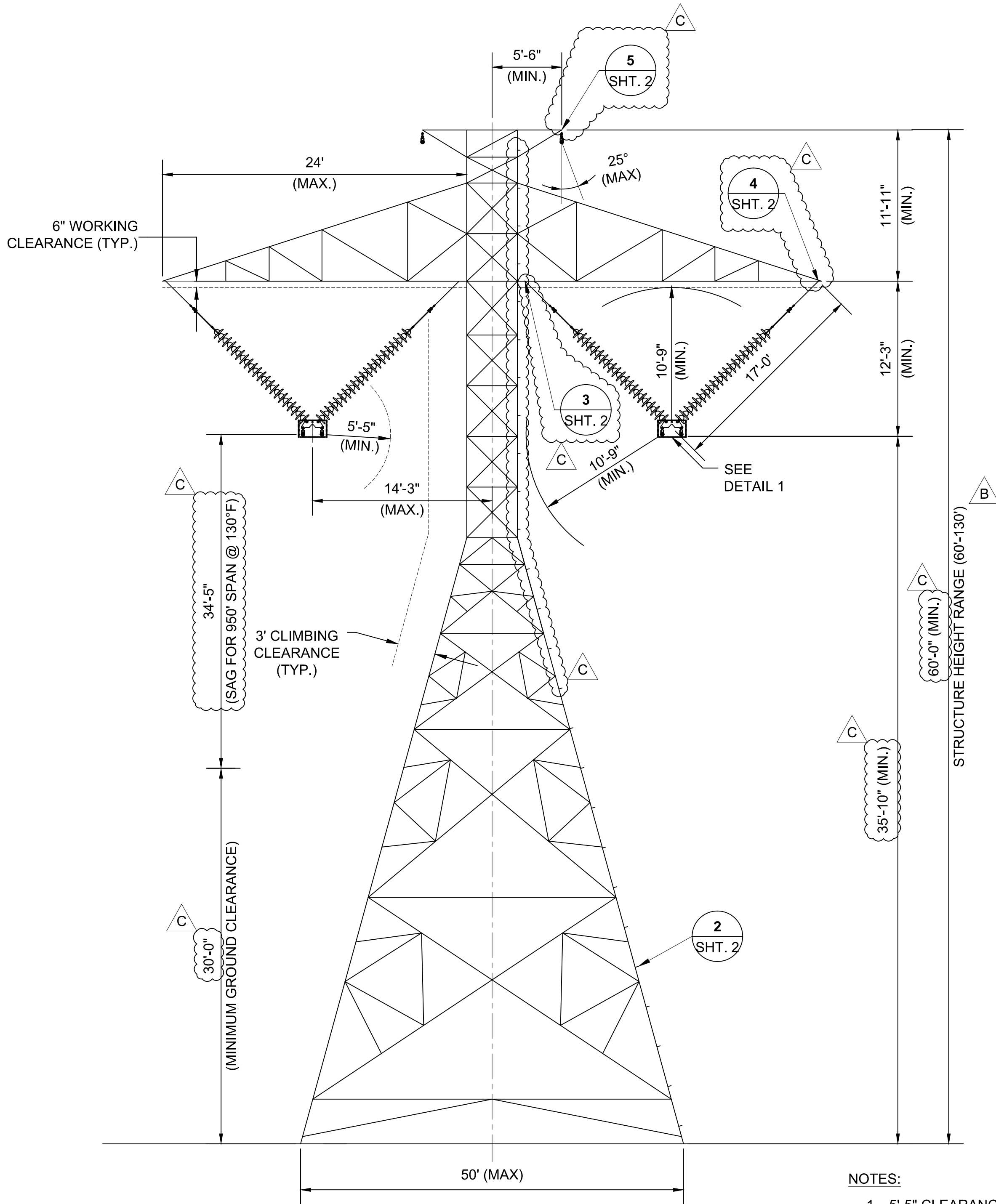
PRELIMINARY - NOT  
FOR CONSTRUCTION

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
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	A	RELEASED FOR RFP BID		5/1/15	KAK		
	DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR

 320kV DC MEDIUM TANGENT 0°-2° 32-SCHLT-MTG-002 LOAD & DESIGN DRAWING	DRAWN KAK
	ENGINEER AKO
	CHECKED TAB
	APPROVED
	DATE 5/1/15

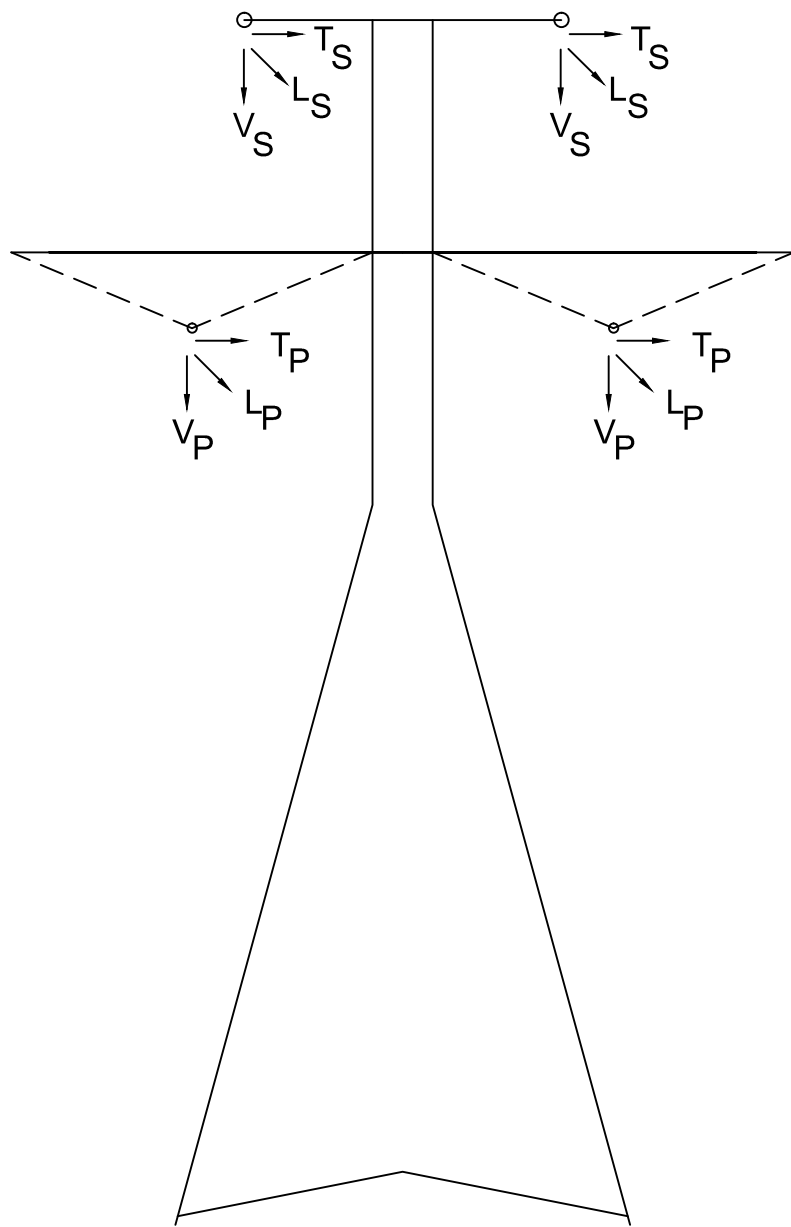
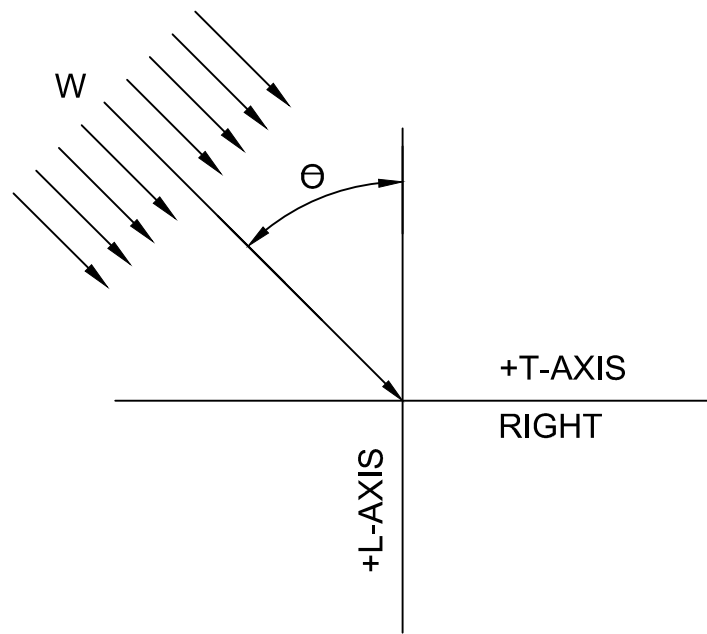
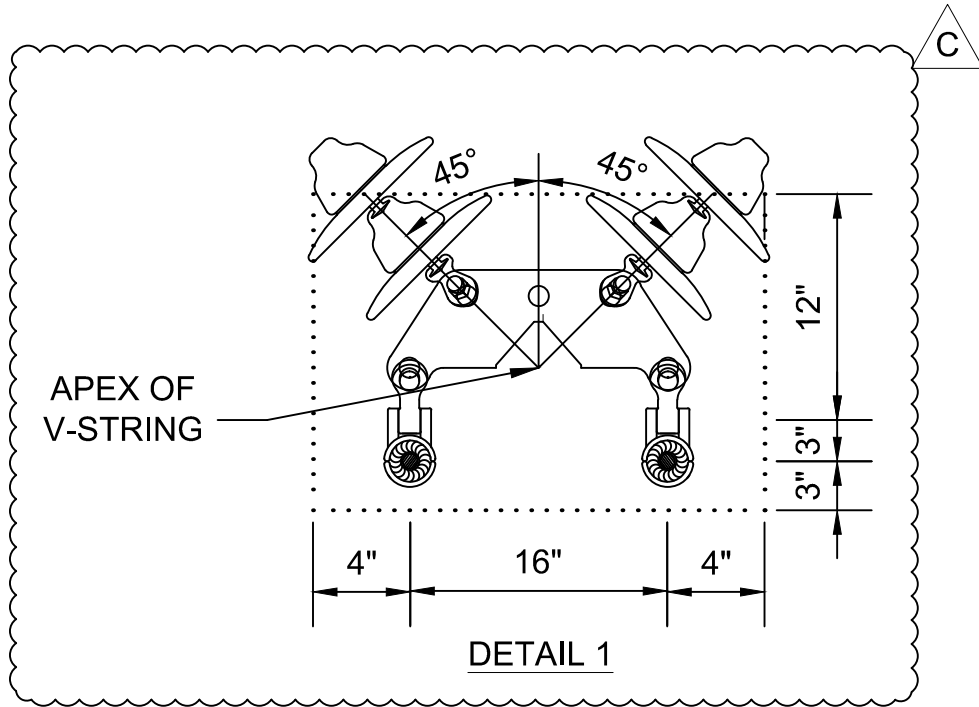
SCALE NTS	FILE: LST-02-002.DWG IMAGE:	DRAWING NO. LST-02-002
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NOTES:

- 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
- 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.



LOADING TREE

STRUCTURE NAME: 32-SCHLT-HTG-002  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 950  
WEIGHT SPAN (FT): 1850  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP ("F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	3.06	1.53	0.00	26.46	7.28	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.88	1.19	0.00	11.15	9.36	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	4.35	1.07	0.00	25.63	4.34	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	7.81	1.53	0.00	35.93	5.48	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	2.04	0.68	0.00	17.64	3.44	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	2.04	0.67	0.00	17.64	3.28	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	2.04	0.57	5.50	17.64	2.58	40.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.25	0.33	0.27	31.91	2.63	2.27	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	3.56	0.21	0.00	24.09	1.66	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.88	0.67	0.00	11.15	5.35	0.00	29.00	45.00	1.00

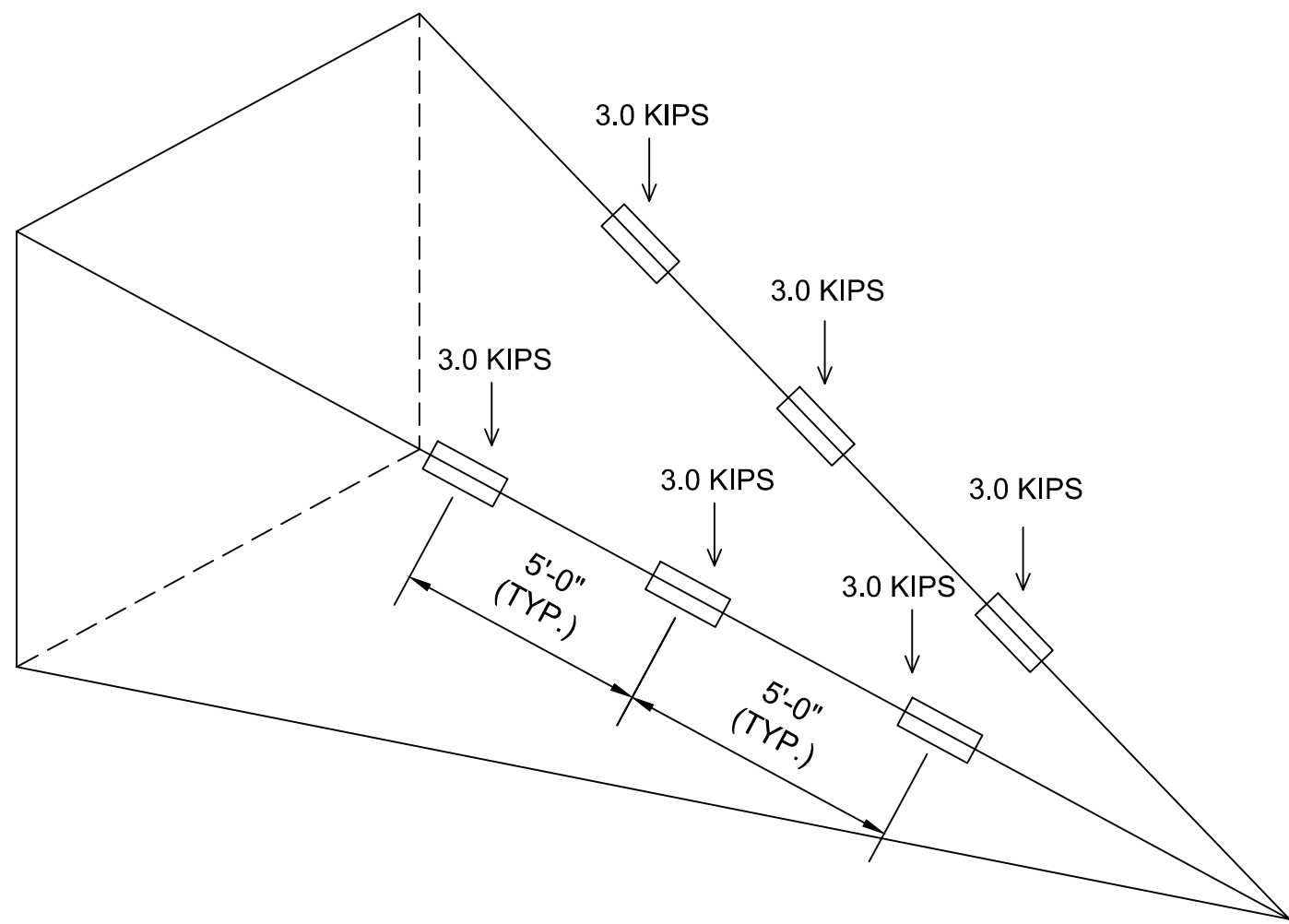
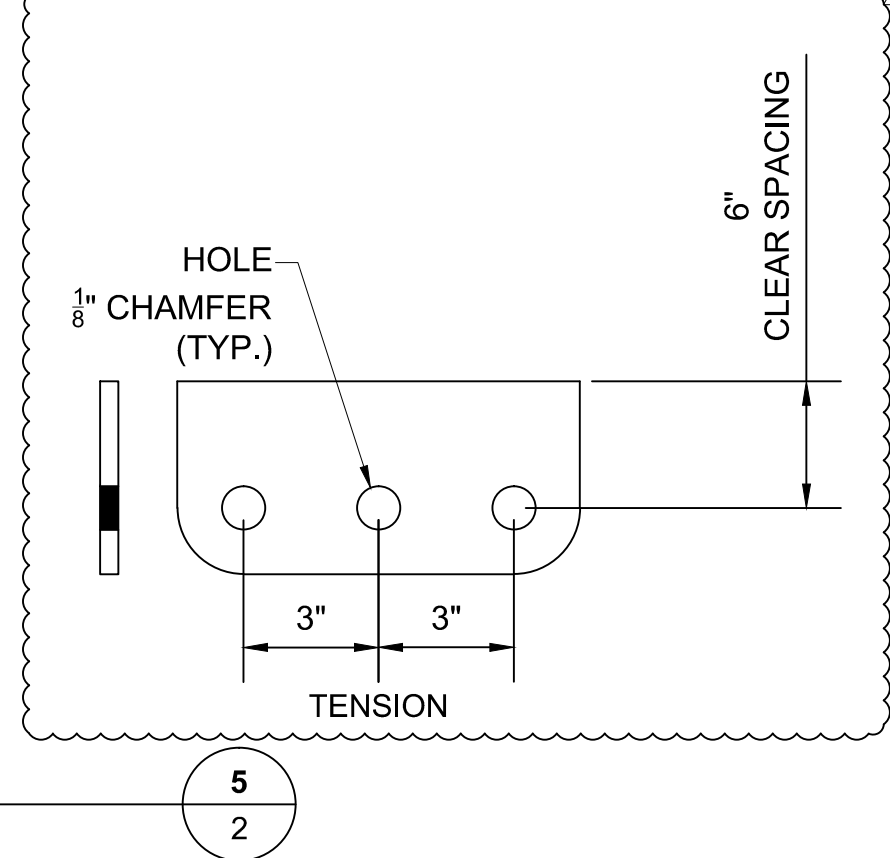
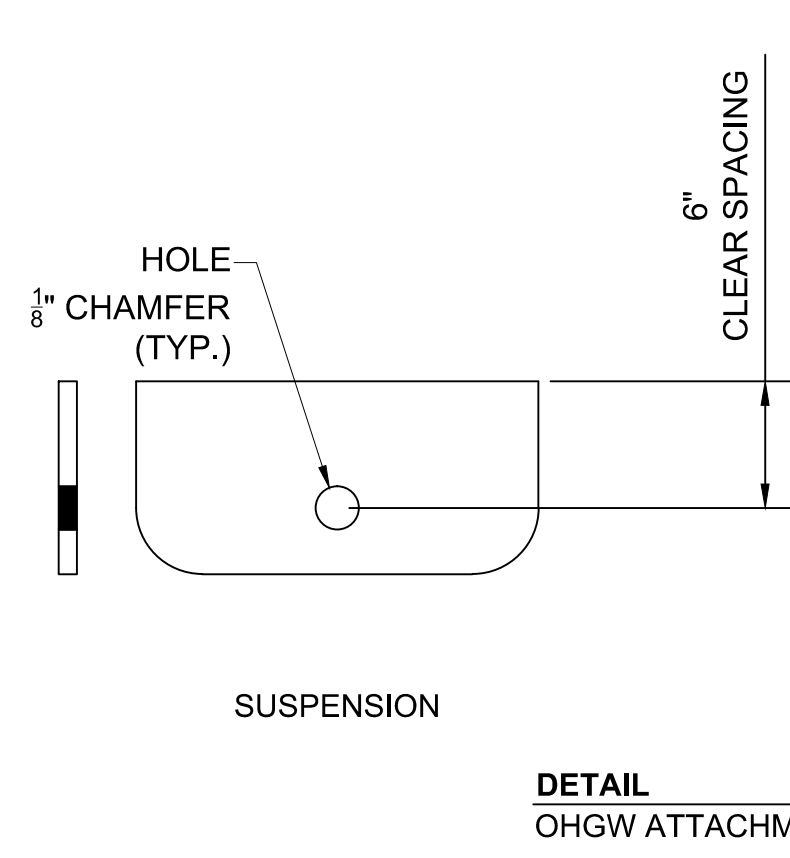
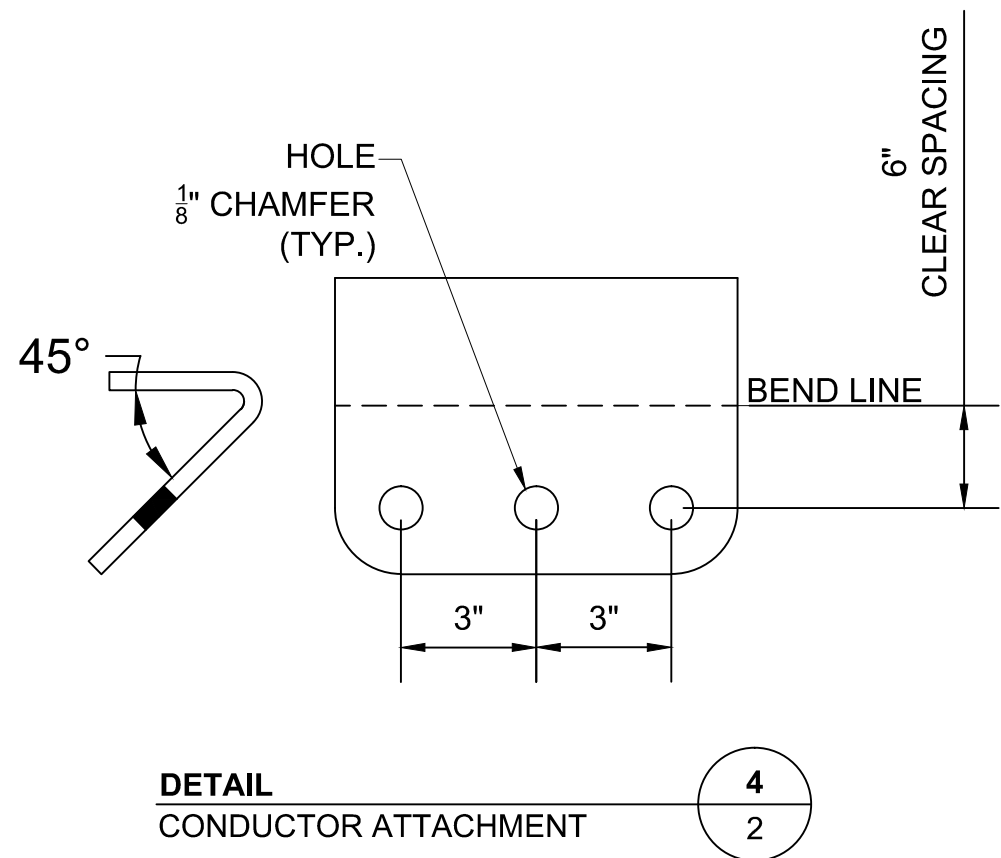
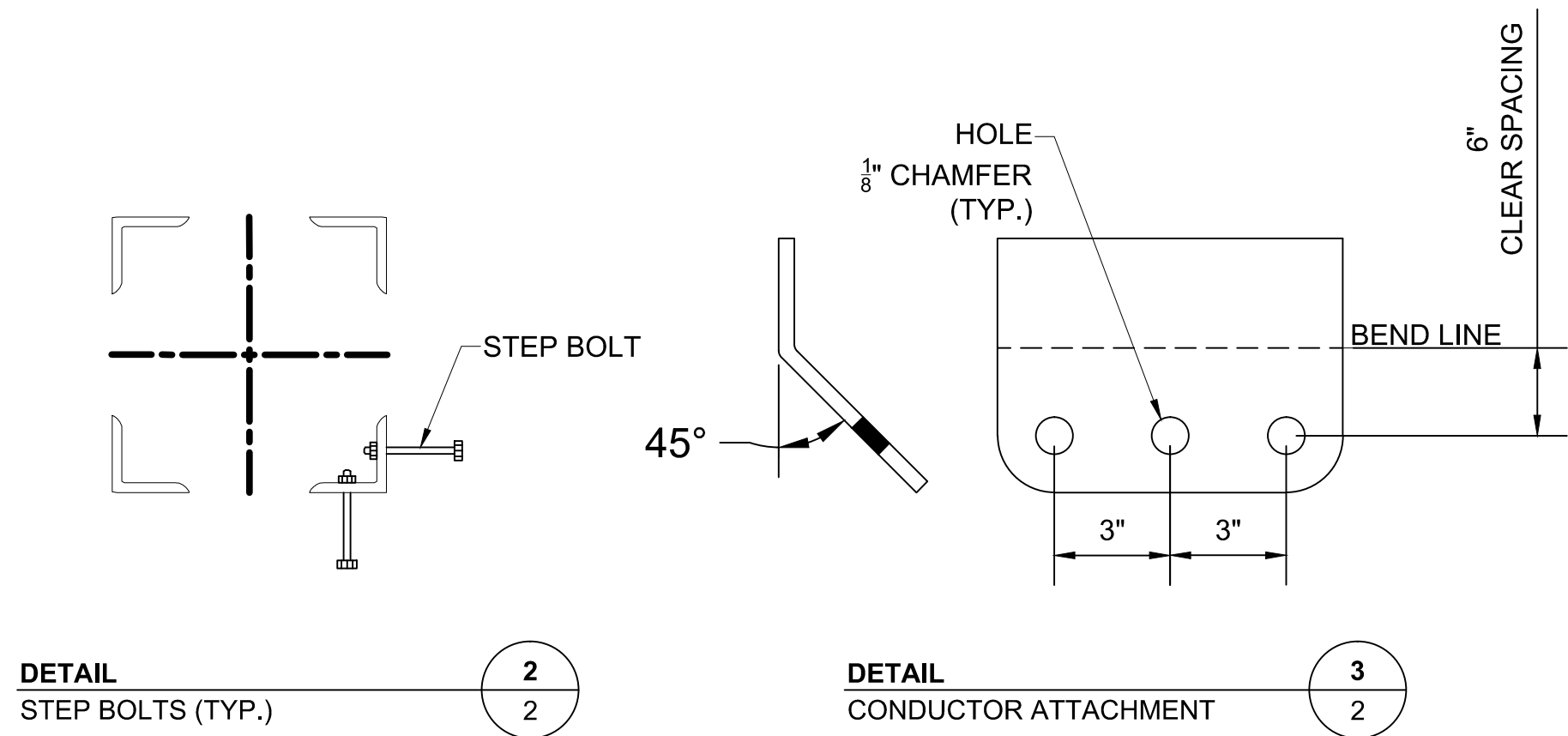
GENERAL NOTES:

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
- TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
- EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
- LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
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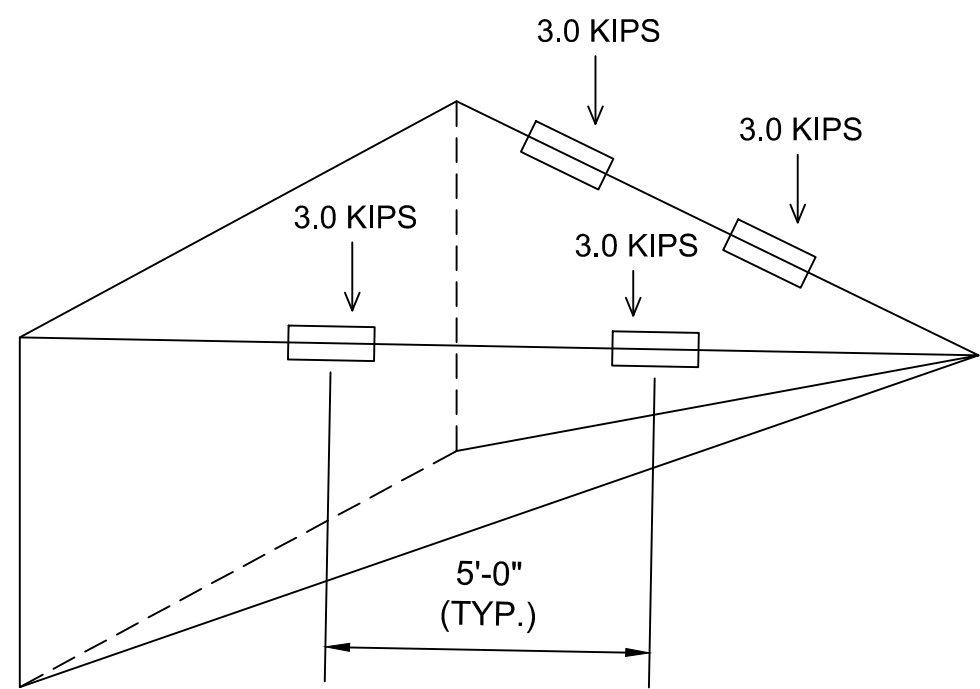
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PRELIMINARY - NOT  
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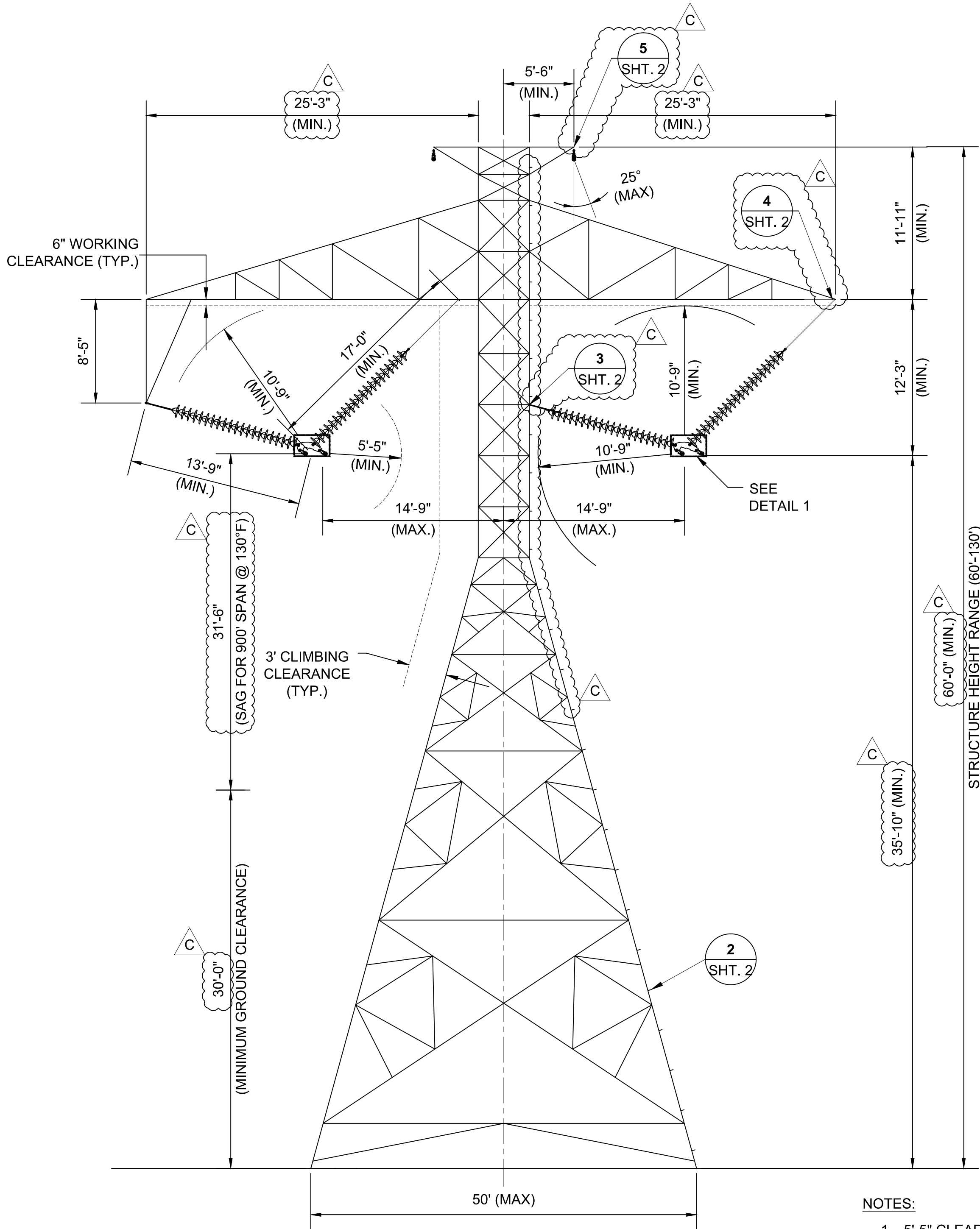
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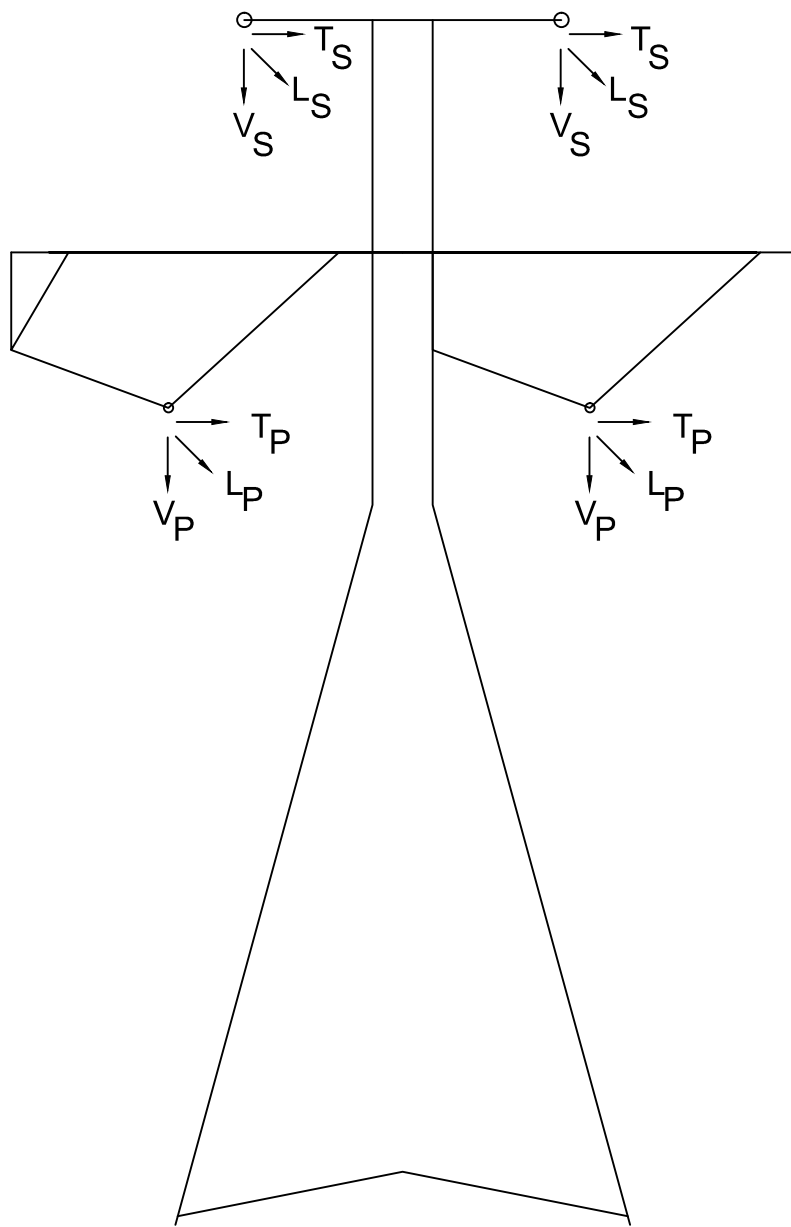
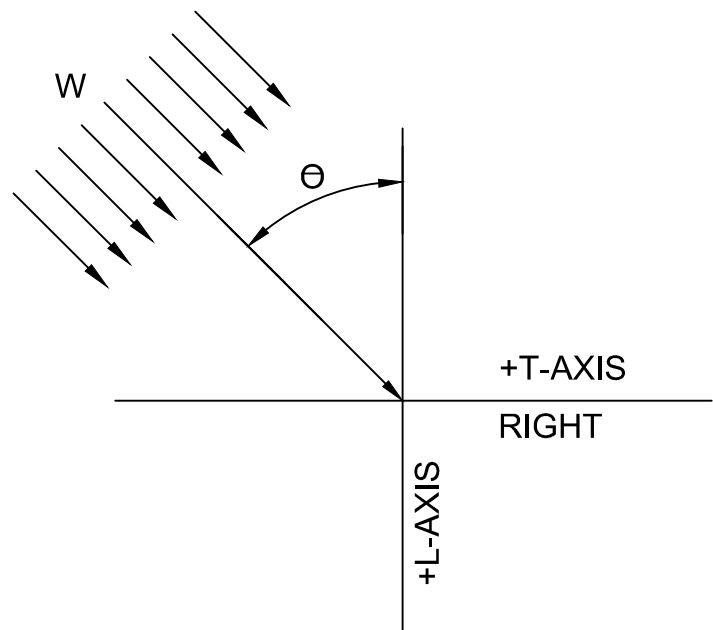
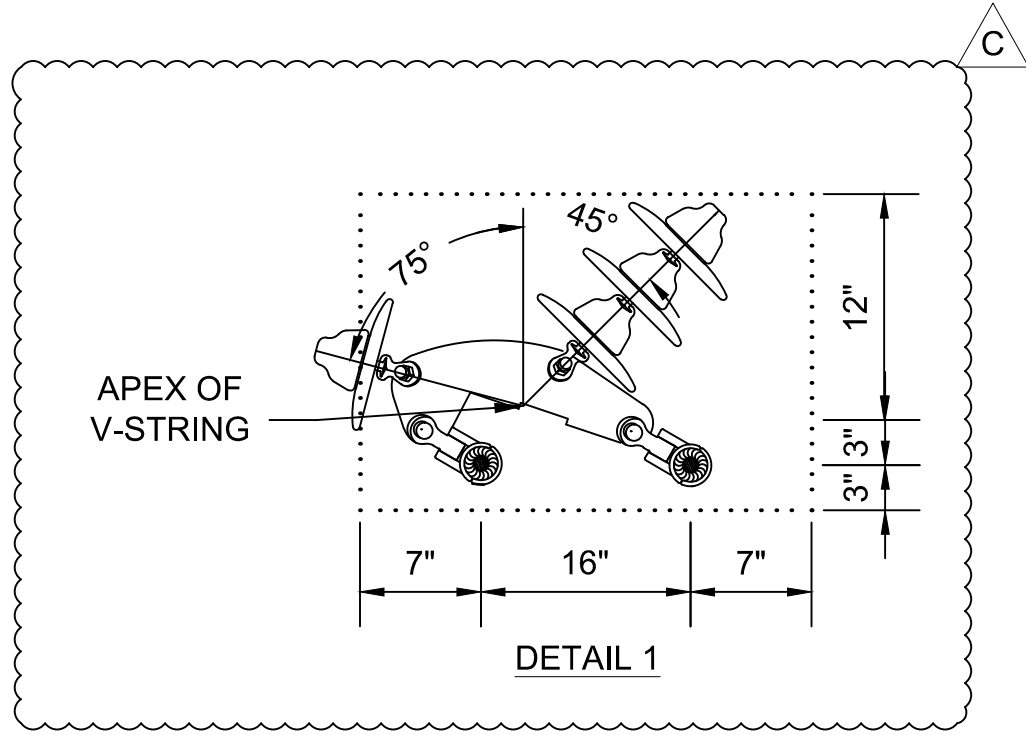
PRELIMINARY - NOT  
FOR CONSTRUCTION





NOTES:

- 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
- 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.



LOADING TREE


STRUCTURE NAME: 32-SCHLT-LAG-010  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 900  
WEIGHT SPAN (FT): 1250  
LINE ANGLE: 2 - 10 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	2.09	2.81	0.00	18.70	17.29	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.61	1.76	0.00	7.82	14.32	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.96	2.15	0.00	17.87	11.47	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	5.30	3.15	0.00	24.83	14.60	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.40	1.47	0.00	12.47	9.56	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.40	1.41	0.00	12.47	8.76	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.40	0.93	5.50	12.47	3.88	24.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.85	1.05	0.27	26.93	8.74	2.27	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	3.02	1.03	0.00	17.45	8.27	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.61	1.28	0.00	7.82	10.53	0.00	29.00	45.00	1.00

GENERAL NOTES:

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
- TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
- EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
- LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
- ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
- THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
- SNUB ANGLES SHALL BE LIMITED TO A 10 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
- TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
- CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
- CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
- CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
- STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

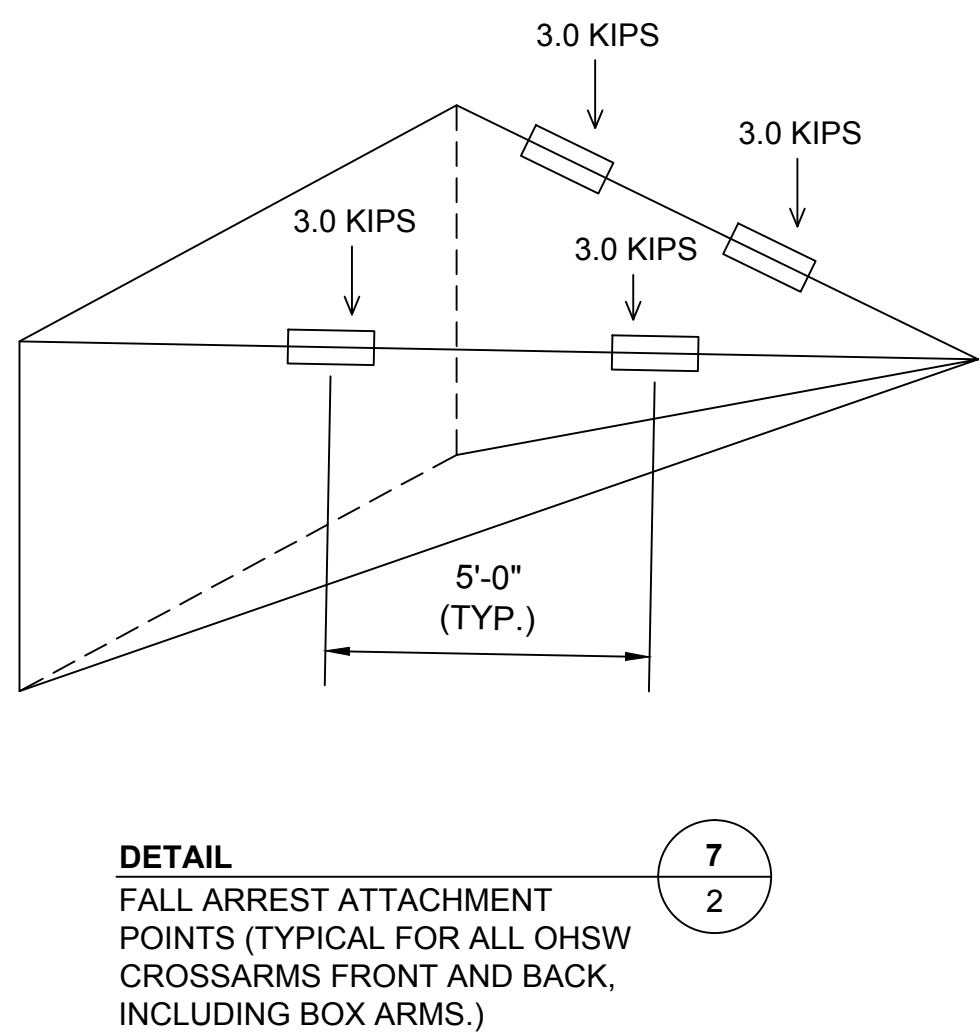
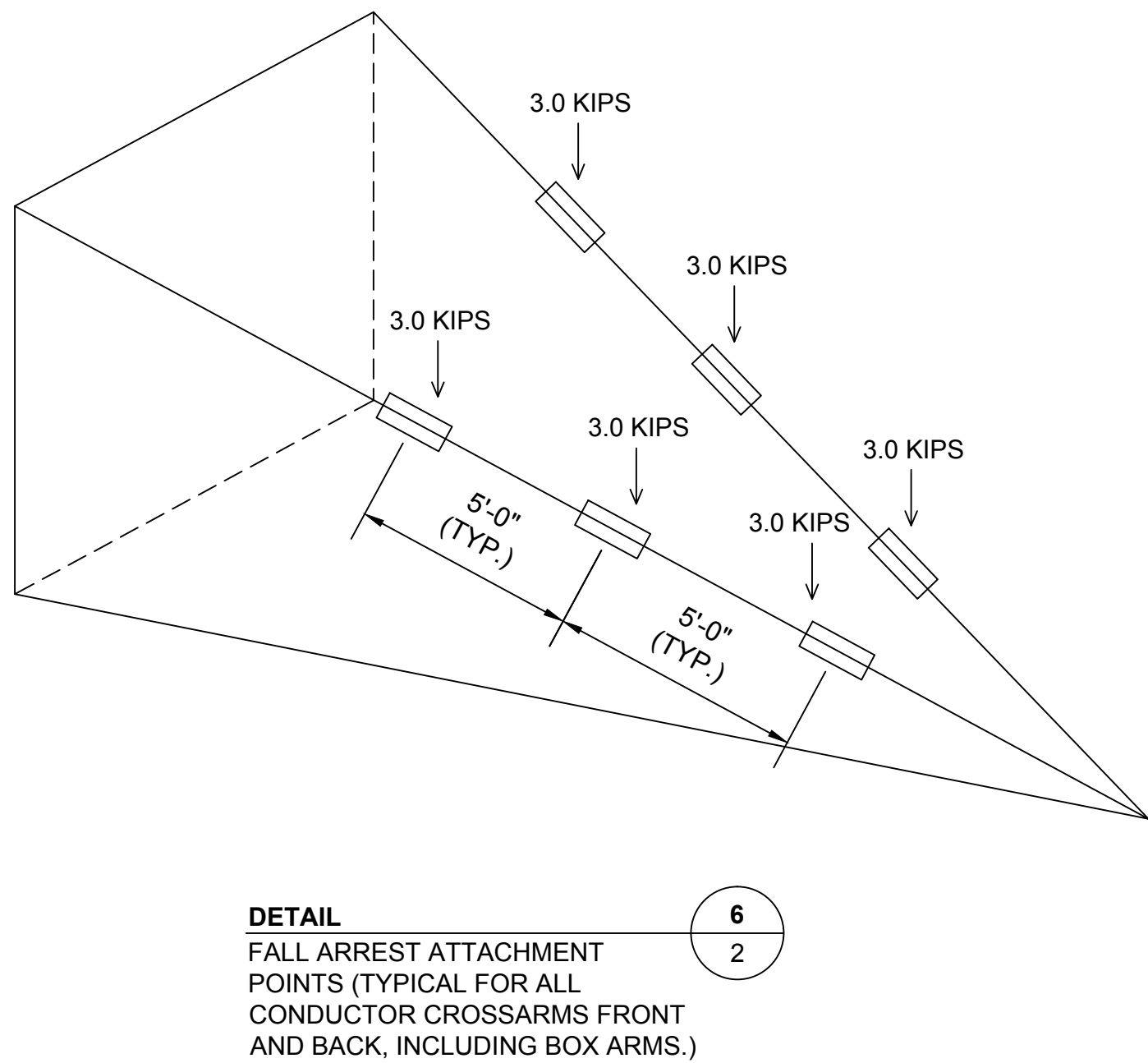
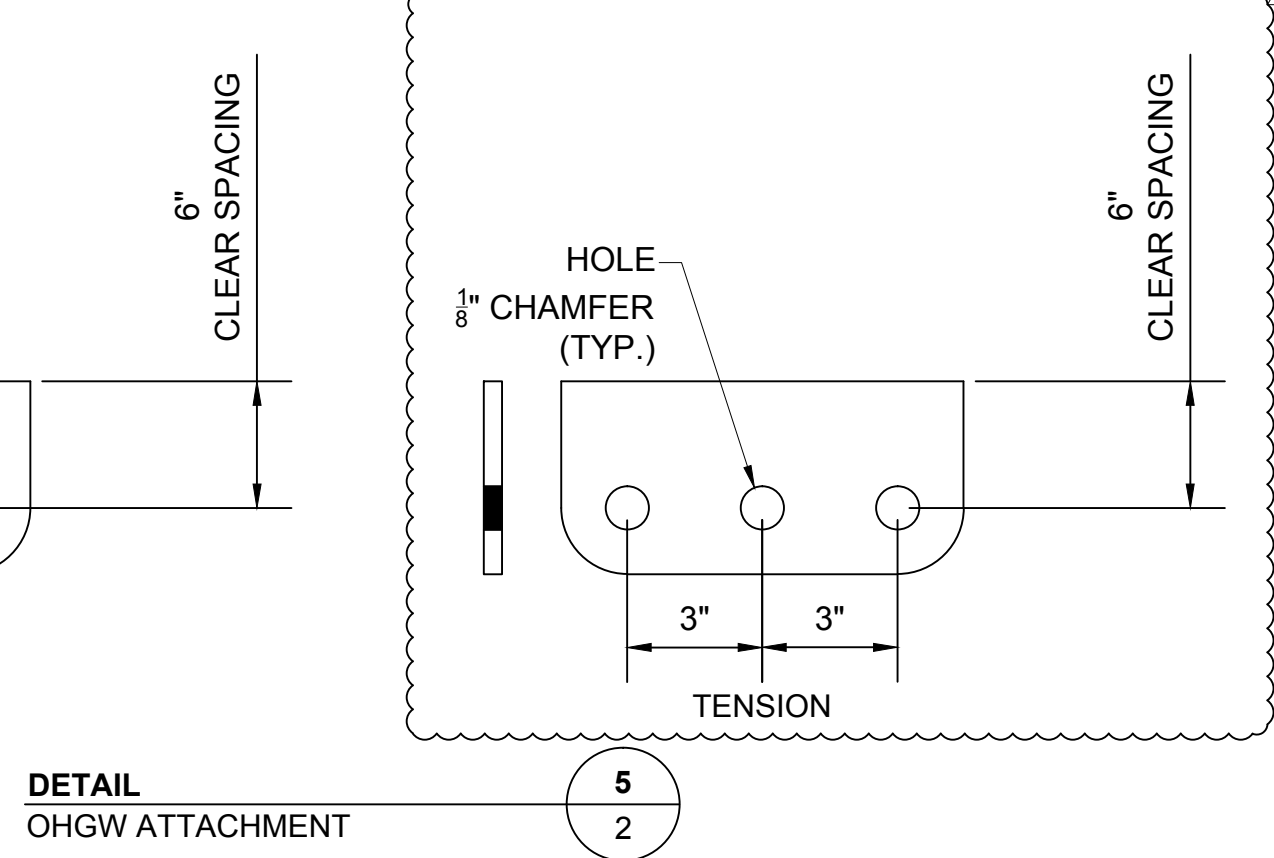
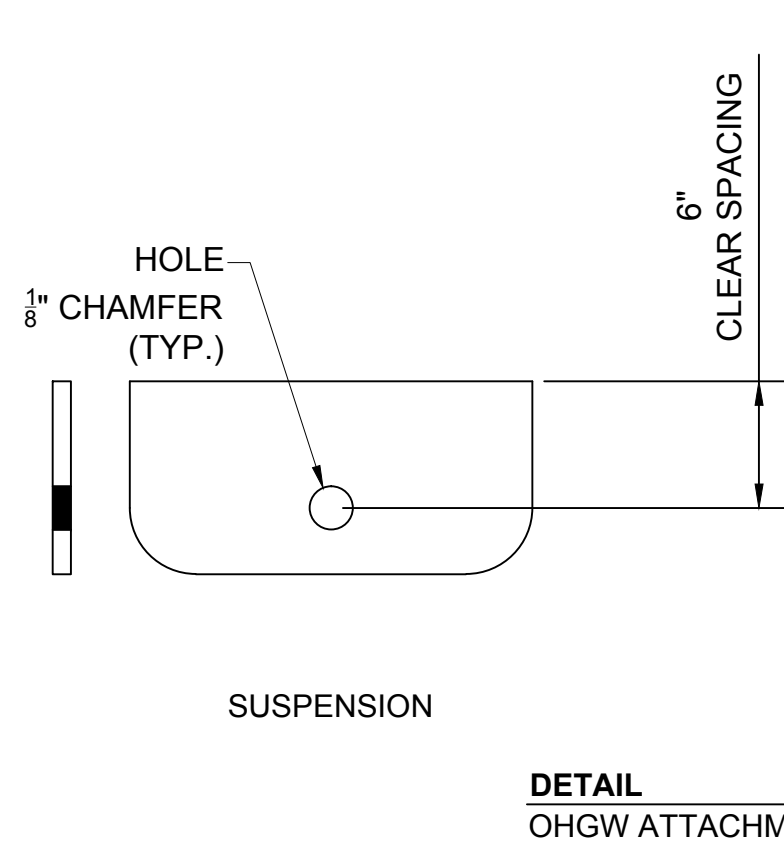
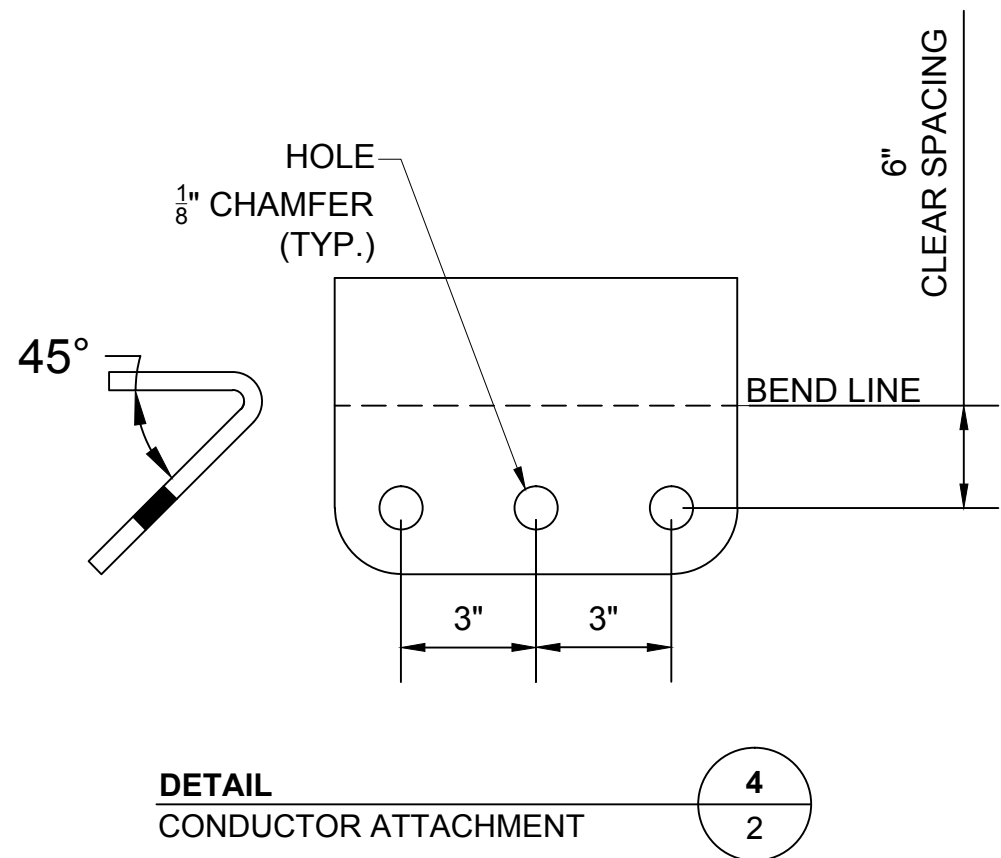
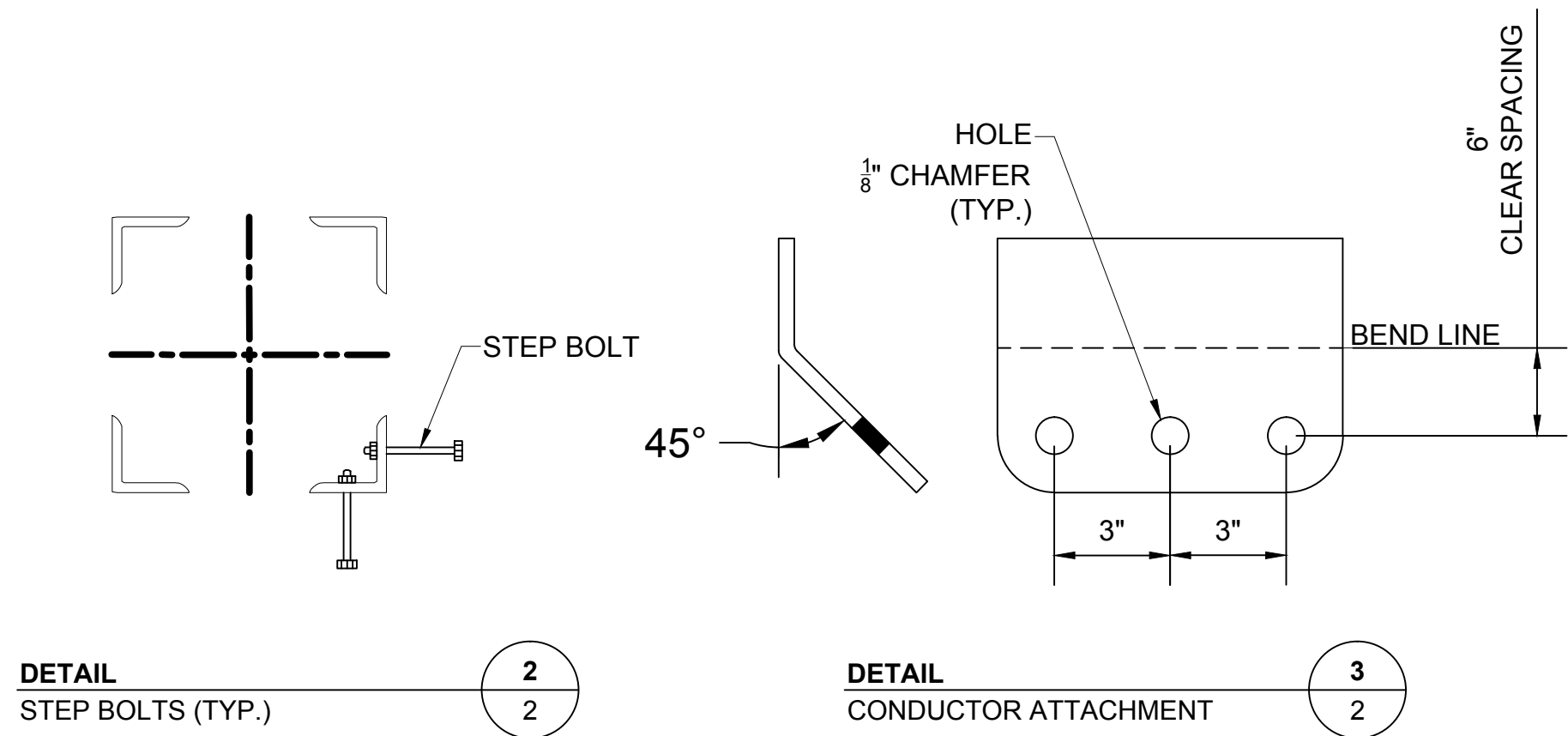
CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
	C	MISC. REVISIONS		5/21/15	KAK		
	B	UPDATED STRUCTURE HEIGHT RANGE		5/8/15	KAK		
	A	RELEASED FOR RFP BID		5/1/15	KAK		
	DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR

 THE NORTHERN PASS	DRAWN	KAK
	ENGINEER	AKO
	CHECKED	TAB
	APPROVED	
	DATE	5/1/15

320kV DC LIGHT RUNNING ANGLE 2°-10° 32-SCHLT-LAG-010 LOAD & DESIGN DRAWING	SCALE NTS	FILE: LST-04-001.DWG IMAGE:	DRAWING NO. LST-04-001
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PRELIMINARY - NOT  
FOR CONSTRUCTION





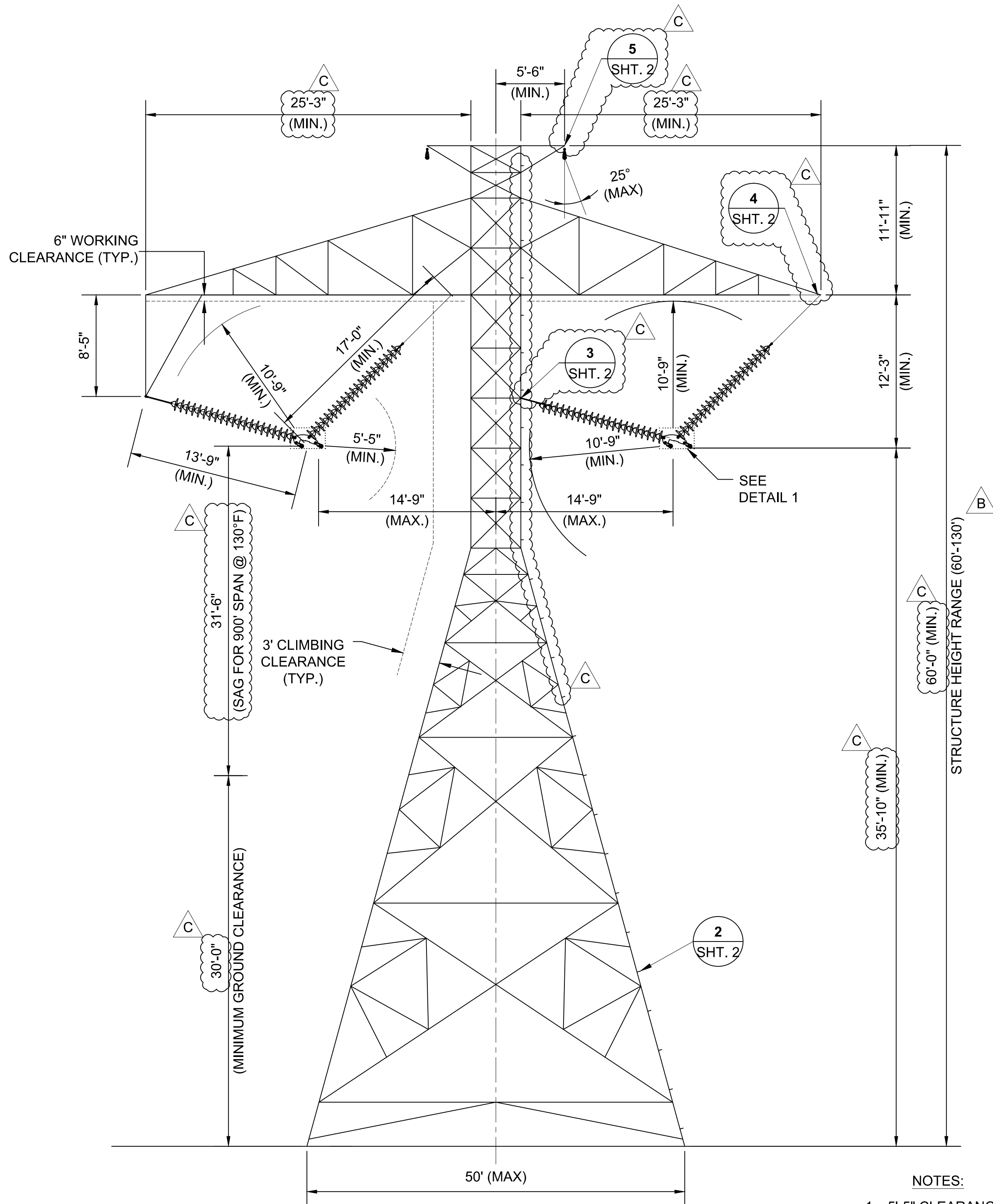
NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 5.
- FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

CONTRACT SERVICES								<div> THE NORTHERN PASS</div>		<div><div>B</div><div>DRAWN KAK</div><div>ENGINEER AKO</div><div>CHECKED TAB</div><div>APPROVED</div><div>DATE 5/1/15</div></div>		
								<div>320kV DC LIGHT RUNNNG ANGLE 2°-10° 32-SCHLT-LAG-010 LOAD &amp; DESIGN DRAWING</div>				
								SCALE NTS		FILE: LST-04-002.DWG		DRAWING NO.
							IMAGE:		LST-04-002			

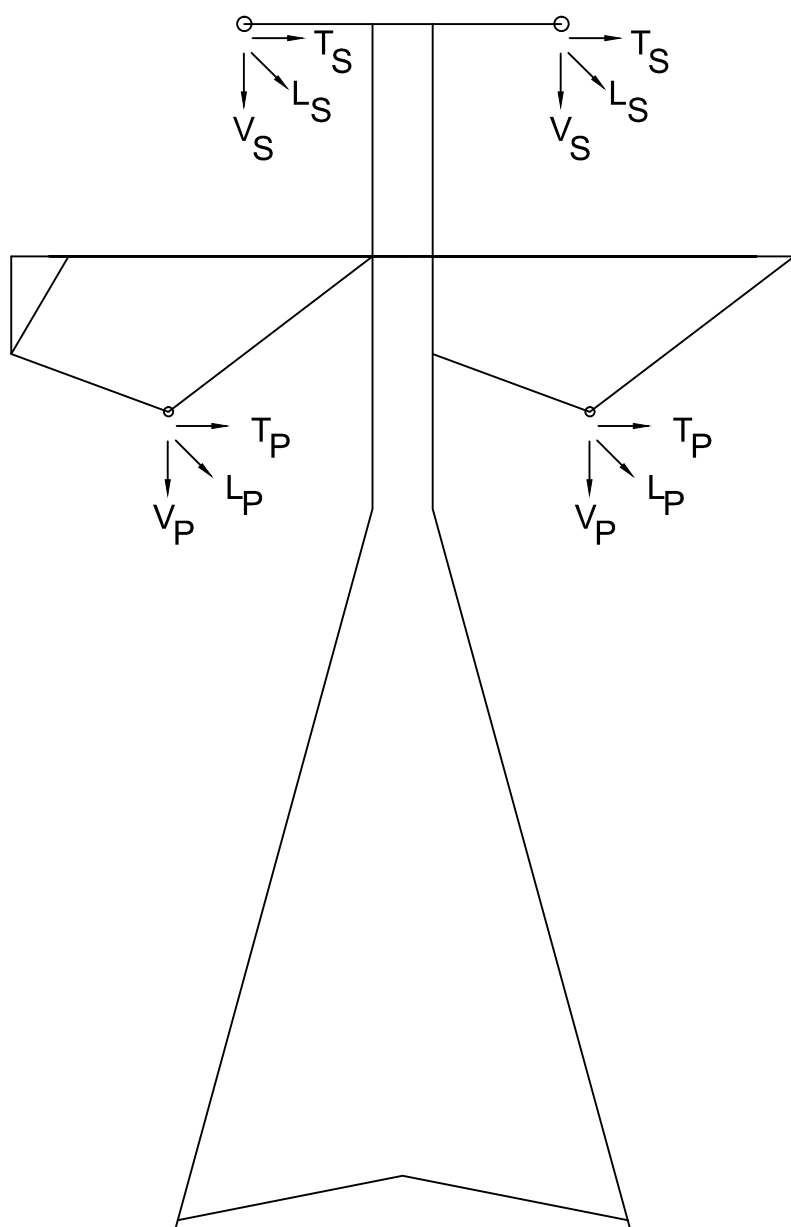
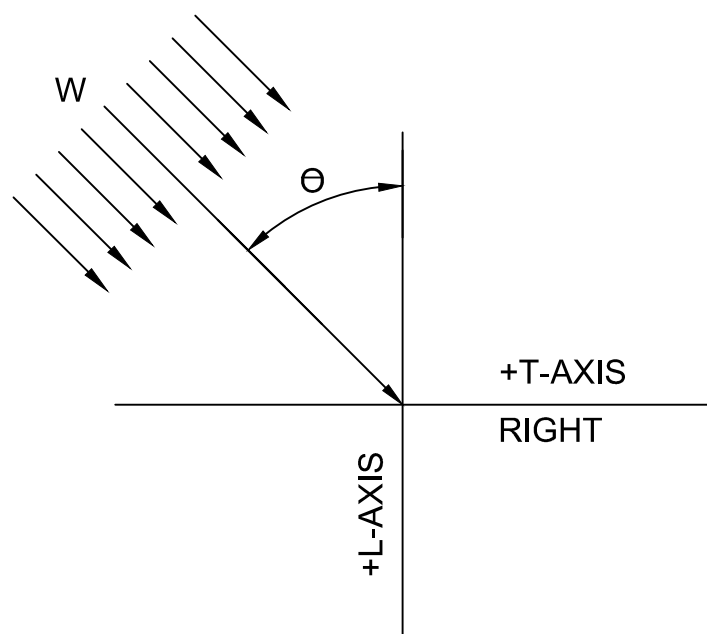
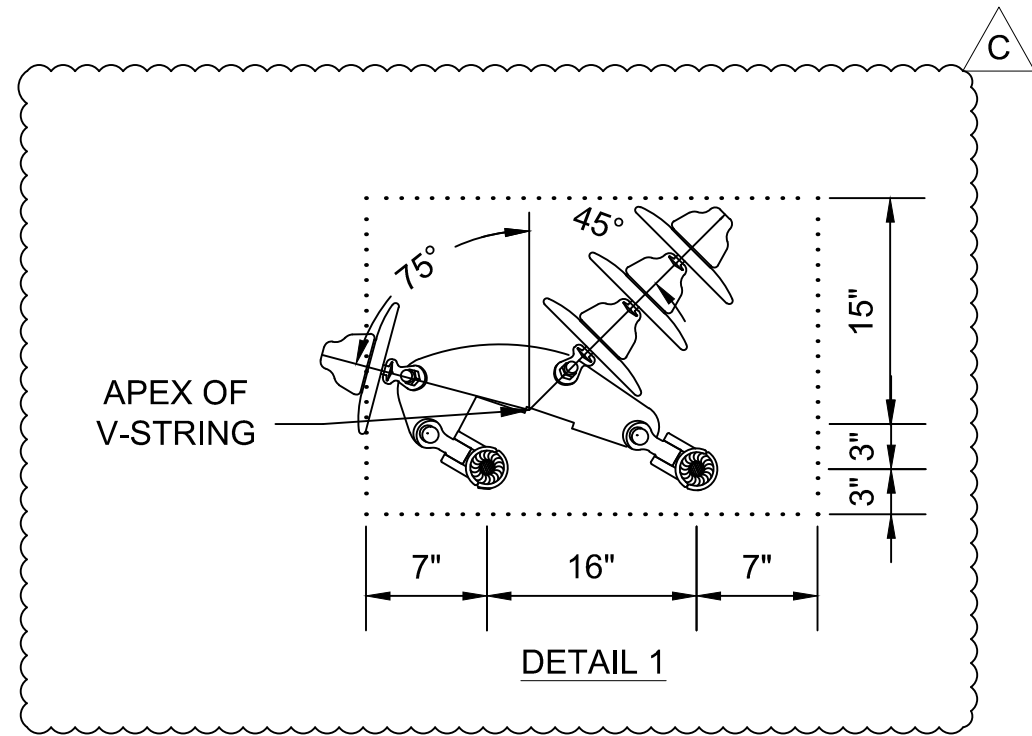
PRELIMINARY - NOT  
FOR CONSTRUCTION





## NOTES:

- 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
- 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.




LOADING TREE

STRUCTURE NAME: 32-SCHLT-HAG-025  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 900  
WEIGHT SPAN (FT): 1250  
LINE ANGLE: 10 - 25 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	2.09	5.30	0.00	18.70	36.32	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.61	2.93	0.00	7.82	24.32	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.96	4.22	0.00	17.87	24.95	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	5.30	6.27	0.00	24.83	31.83	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.40	2.98	0.00	12.47	21.09	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.40	2.83	0.00	12.47	19.10	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.40	1.64	5.48	12.47	10.44	39.85	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.85	2.40	0.27	26.93	20.18	2.27	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	3.02	2.56	0.00	17.45	20.54	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.61	2.44	0.00	7.82	20.53	0.00	29.00	45.00	1.00

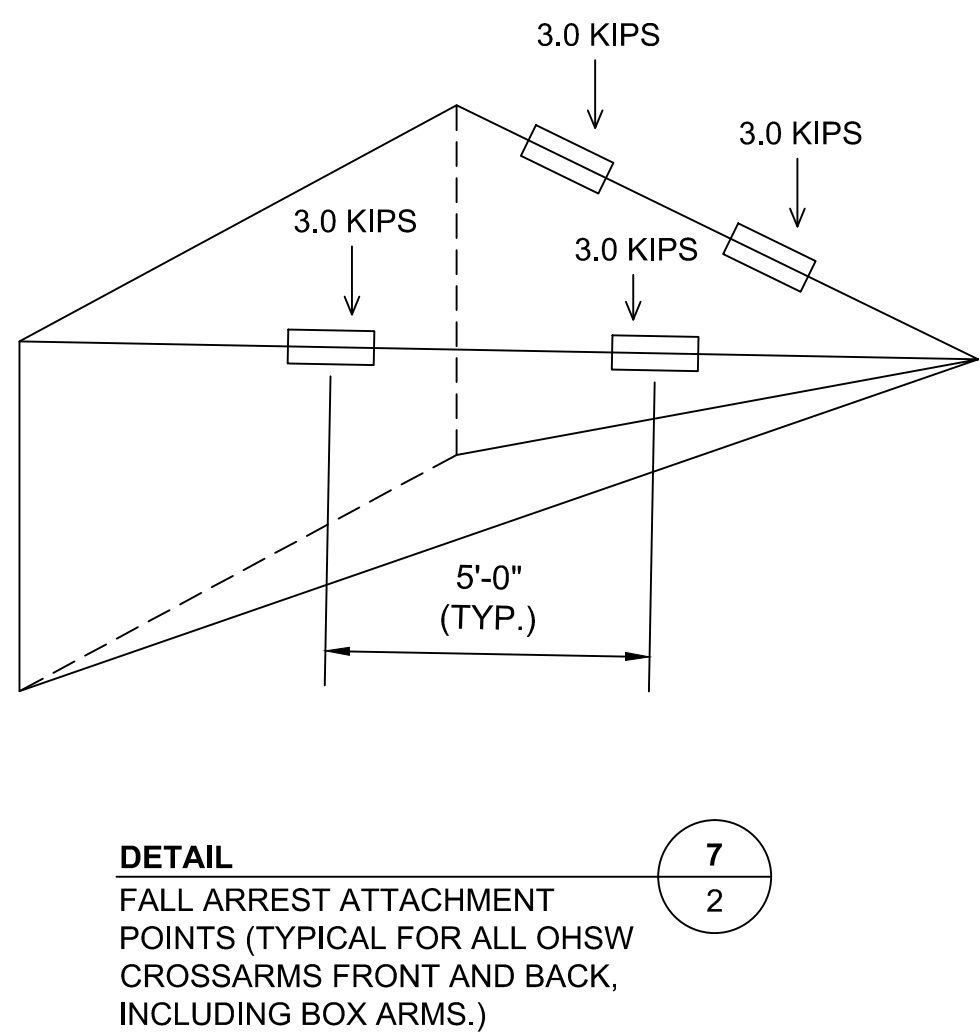
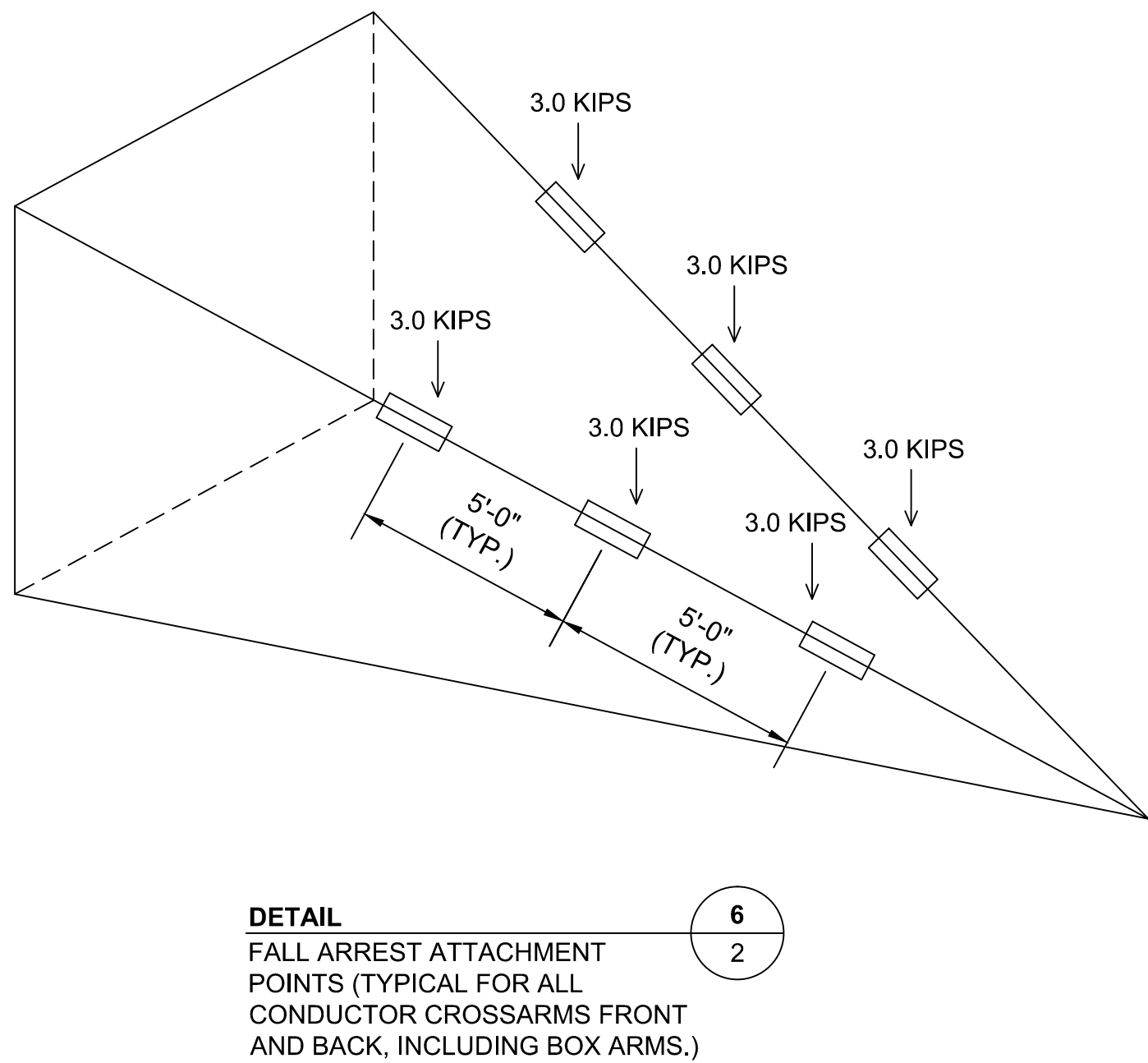
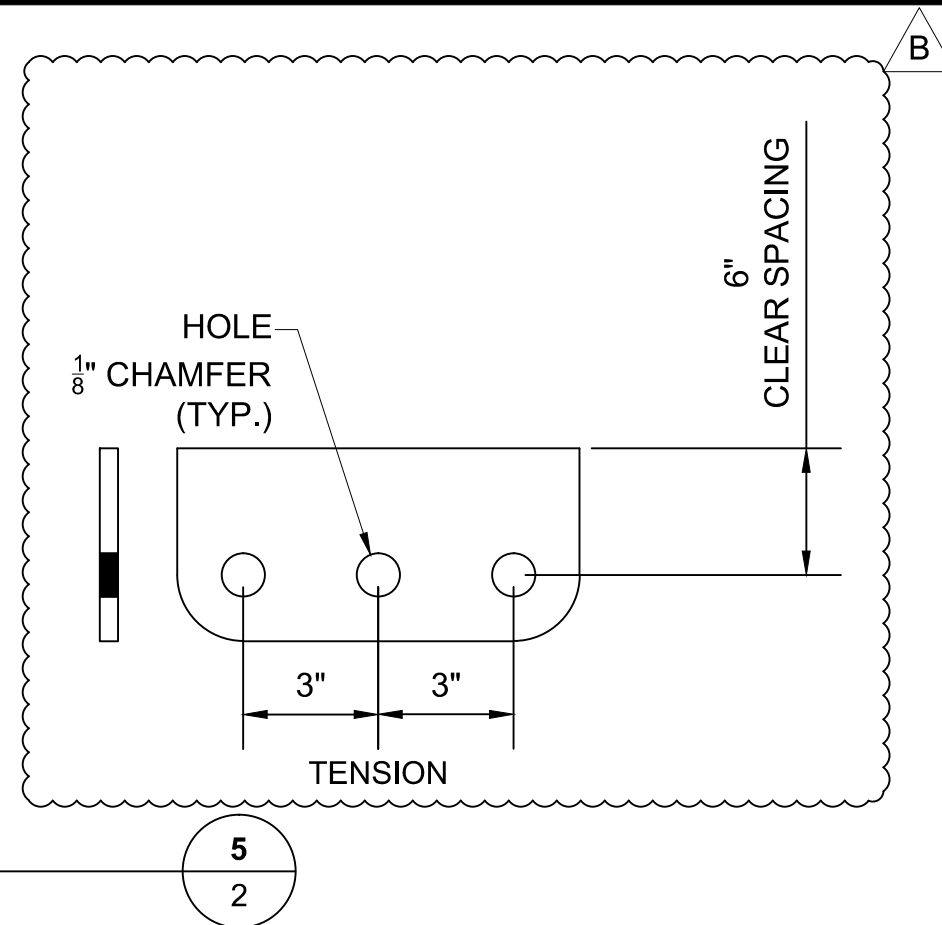
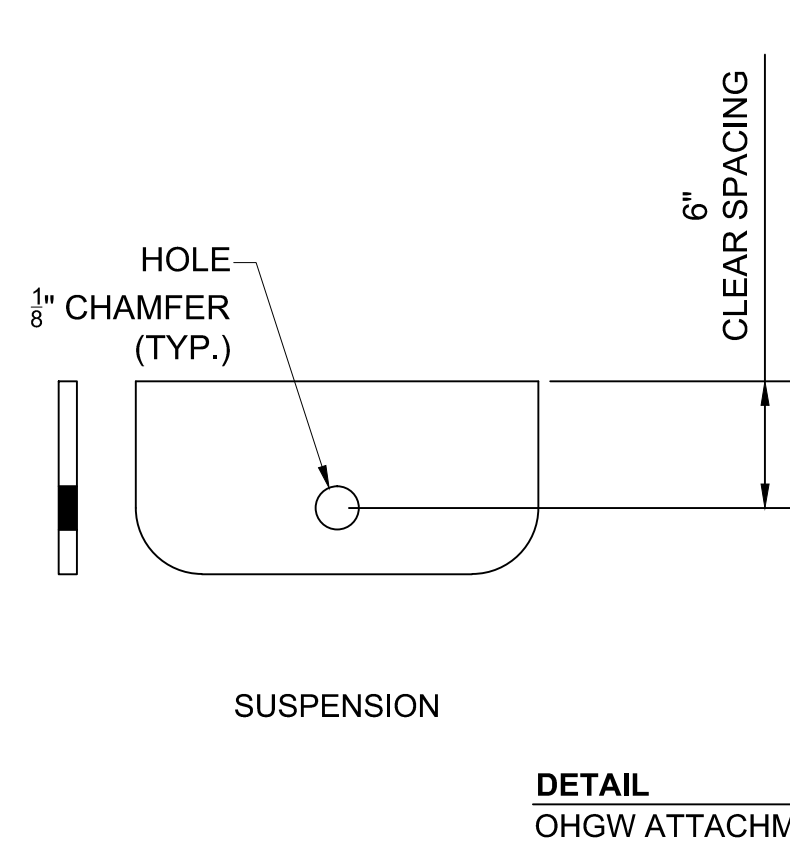
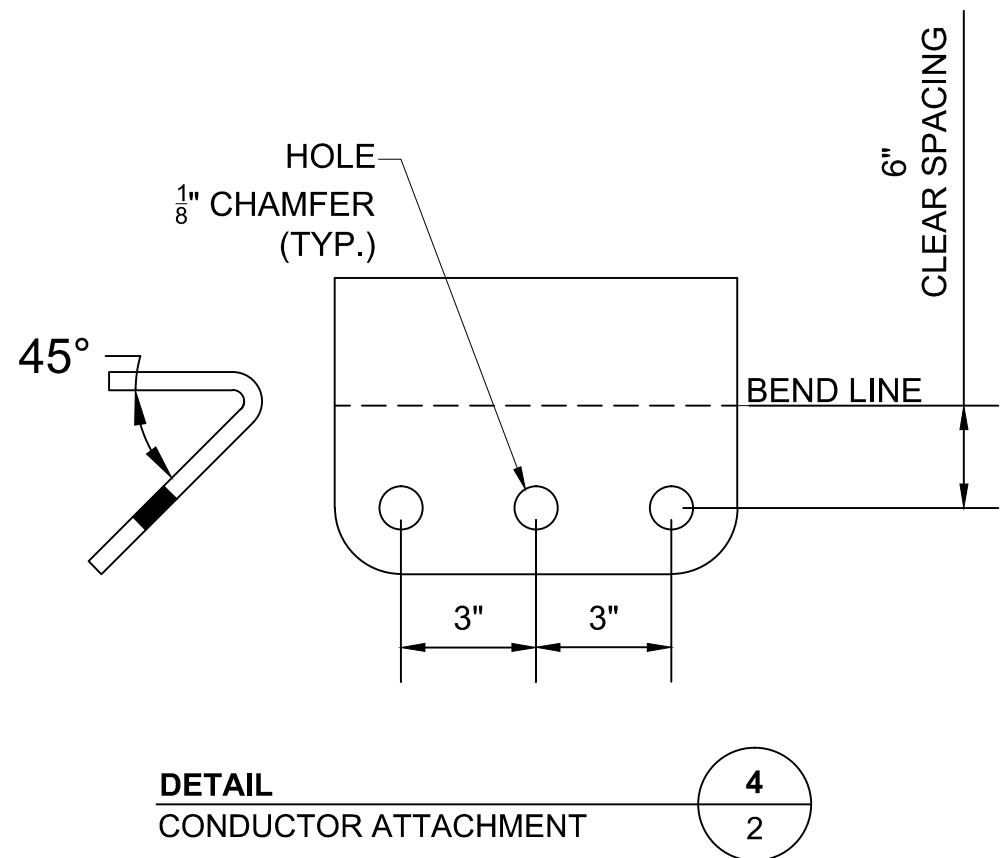
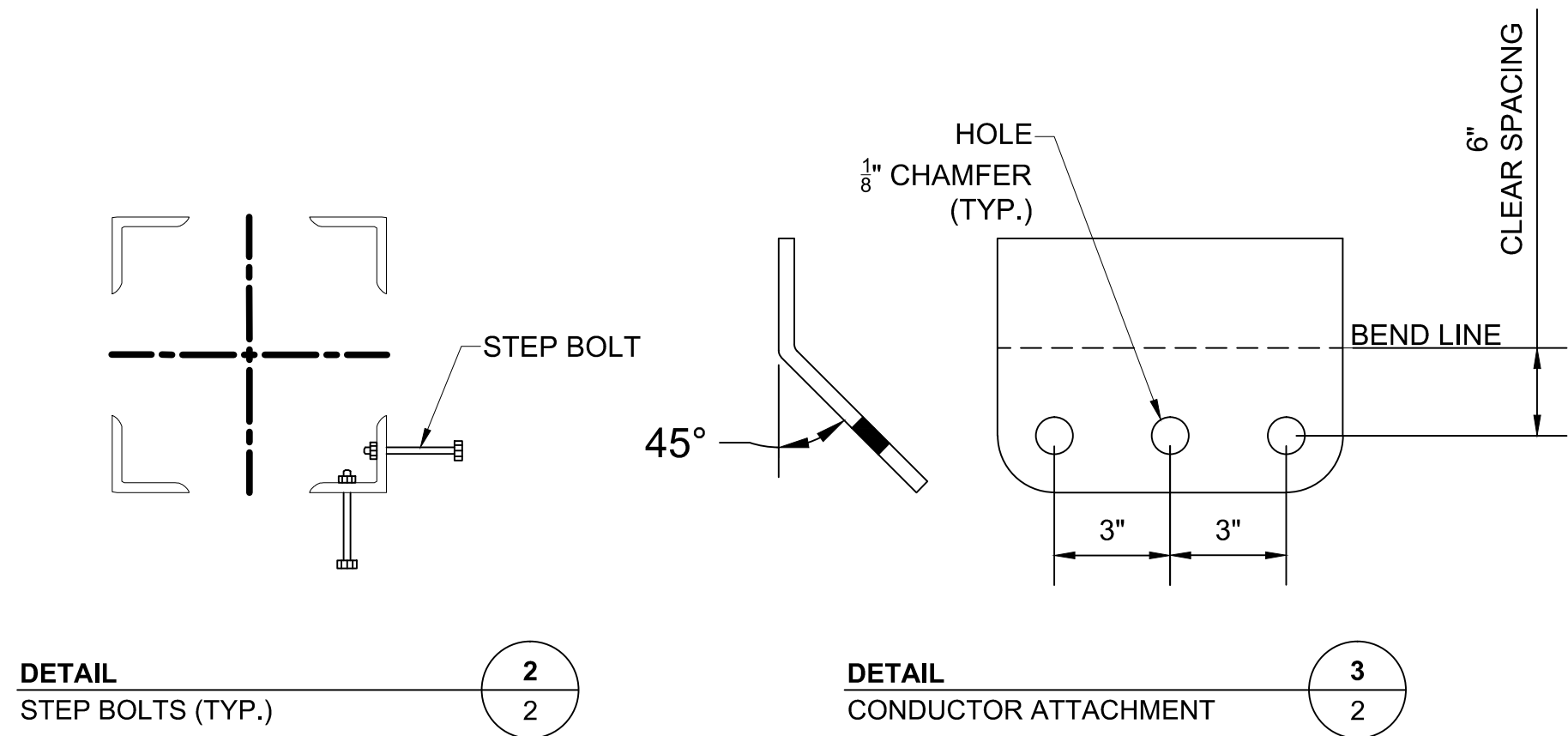
## GENERAL NOTES:

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
- TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
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- THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
- EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
- LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
- ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
- THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
- SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
- TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
- CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
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- CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
- STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	 320kV DC HEAVY RUNNING ANGLE 10°-25° 32-SCHLT-HAG-025 LOAD & DESIGN DRAWING		C	
										DRAWN KAK	
										ENGINEER AKO	
										CHECKED TAB	
								APPROVED		DATE 5/1/15	
								SCALE NTS		DRAWING NO. LST-05-001	
								FILE: LST-05-001.DWG		IMAGE:	
								DWG REV		EPM/DESCRIPTION	
										CONT/PE#	
										DATE	
										DRN	
										CHKD	
										APPR	

PRELIMINARY - NOT  
FOR CONSTRUCTION





NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 5.
- FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

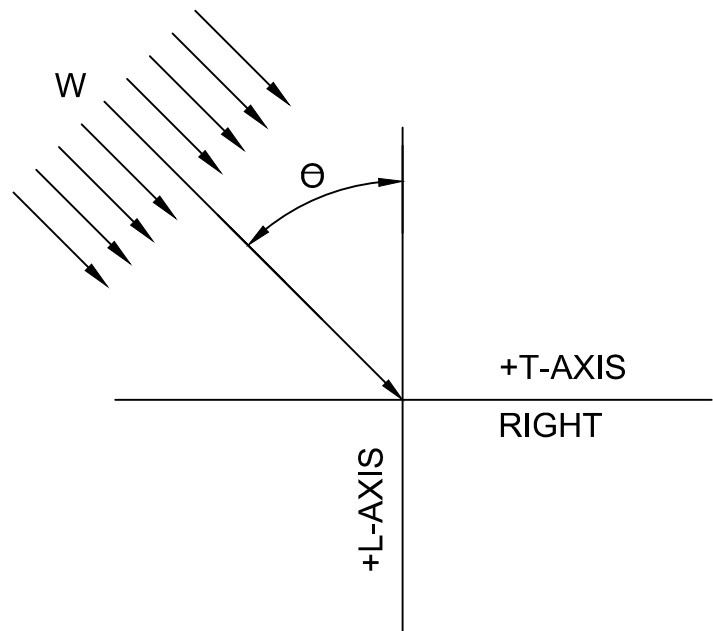
CONTRACT SERVICES																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					</
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PRELIMINARY - NOT  
FOR CONSTRUCTION





1. 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
2. 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.

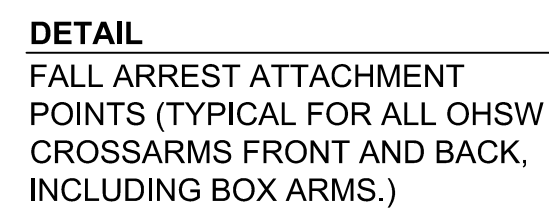
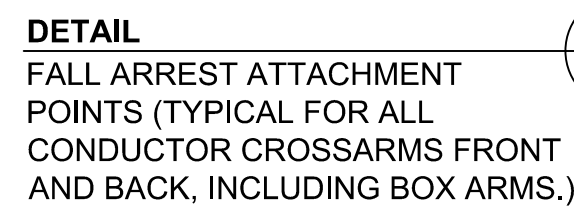


LOADING CASE					DESIGN LOADS															
NO.	DESCRIPTION	TEMP ("F)	ICE (in)	WIND (mph)	VSA (k)	TSa (k)	LSa (k)	VSb (k)	TSb (k)	LSb (k)	VPA (k)	TPA (k)	LPA (k)	VPb (k)	TPb (k)	LPb (k)	W (psf)	Ø	K	
1	NESC 250B	0.00	0.50	39.53	1.41	4.37	9.62	1.41	4.37	-9.62	13.36	30.89	73.59	13.36	30.89	-73.59	10.00	90.00	1.50	
2	NESC 250C	60.00	0.00	100.00	0.42	2.32	4.51	0.42	2.32	-4.51	5.52	19.43	38.67	5.52	19.43	-38.67	29.00	90.00	1.00	
3	NESC 250D	15.00	1.00	39.53	1.97	3.53	8.01	1.97	3.53	-8.01	12.47	21.41	52.13	12.47	21.41	-52.13	4.00	90.00	1.00	
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	5.25	12.04	3.51	5.25	-12.04	16.96	27.33	66.65	16.96	27.33	-66.65	4.00	90.00	1.00	
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	2.51	5.83	0.94	2.51	-5.83	8.91	18.16	44.60	8.91	18.16	-44.60	4.00	90.00	1.00	
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	2.38	-5.50	8.91	16.40	40.00	8.91	16.40	-40.00	4.00	90.00	1.00	
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	2.38	0.00	8.91	16.40	40.00	8.91	1.00	0.00	4.00	90.00	1.00	
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.52	0.27	1.98	2.08	-5.23	30.33	12.71	2.27	9.63	17.56	-44.25	3.45	90.00	1.50	
9	MAINTENANCE	60.00	0.00	0.00	2.64	2.26	5.92	2.64	2.26	-5.92	12.84	18.16	47.44	12.84	18.16	-47.44	0.00	90.00	2.00	
10	OBLIQUE WIND	60.00	0.00	100.00	0.42	2.03	4.51	0.42	2.03	-4.51	5.52	17.12	38.67	5.52	17.12	-38.67	29.00	45.00	1.00	
11	UPLIFT	-20.00	0.00	0.00	0.42	1.70	4.43	0.42	1.70	-4.43	5.52	16.59	43.34	5.52	16.59	-43.34	0.00	90.00	1.00	


3. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
4. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
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20. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
21. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).
22. STRUCTURES SHALL ALSO BE DESIGNED WITH UPLIFT LOADING. UPLIFT SHALL BE CONSIDERED UNDER LOAD CASE 1, LOAD CASE 2, & LOAD CASE 11. FOR LOAD CASE 1 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -1 KIPS. FOR LOAD CASE 2 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.1 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -1.6 KIPS. FOR LOAD CASE 13 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -2.3 KIPS.

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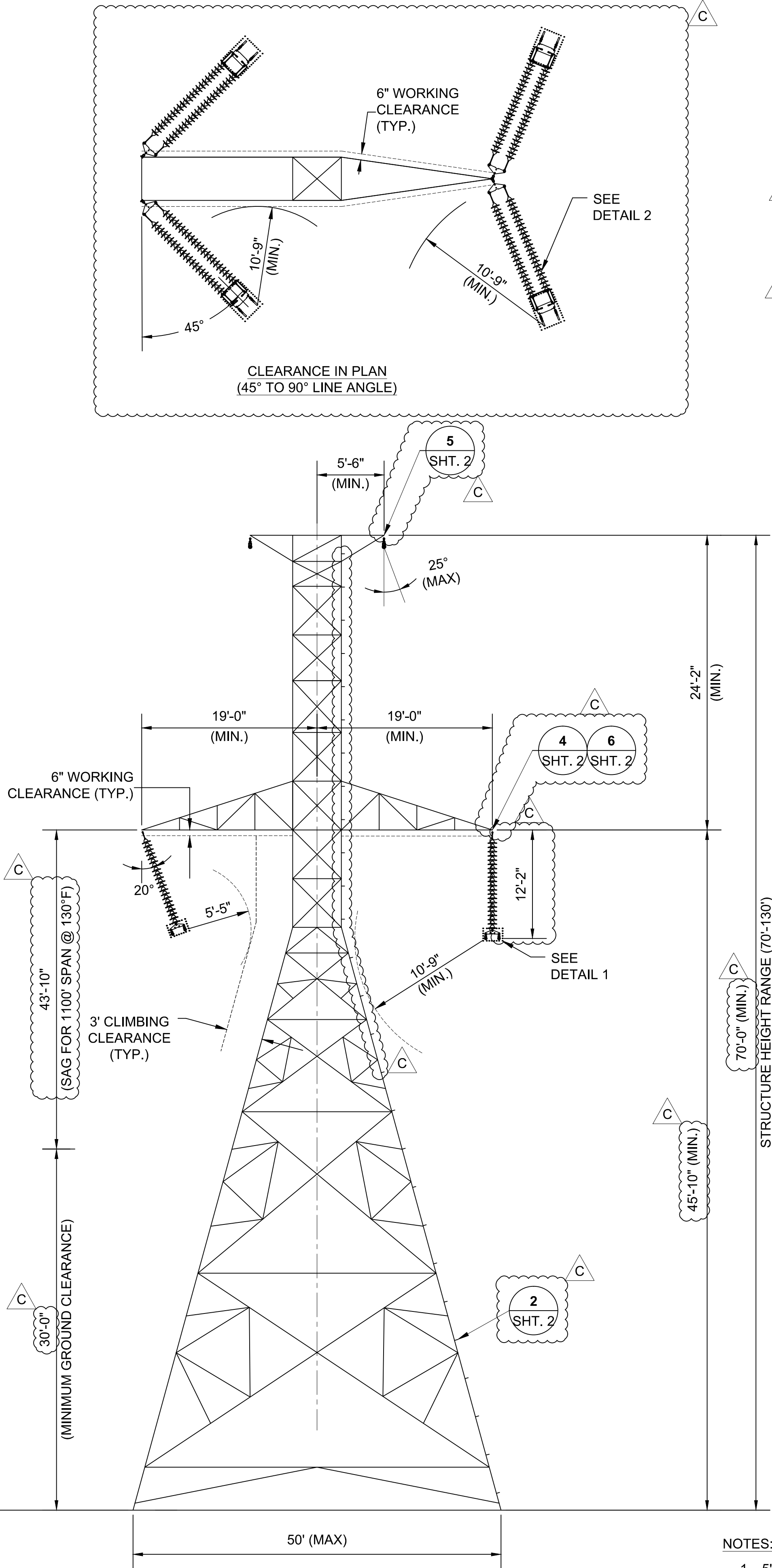




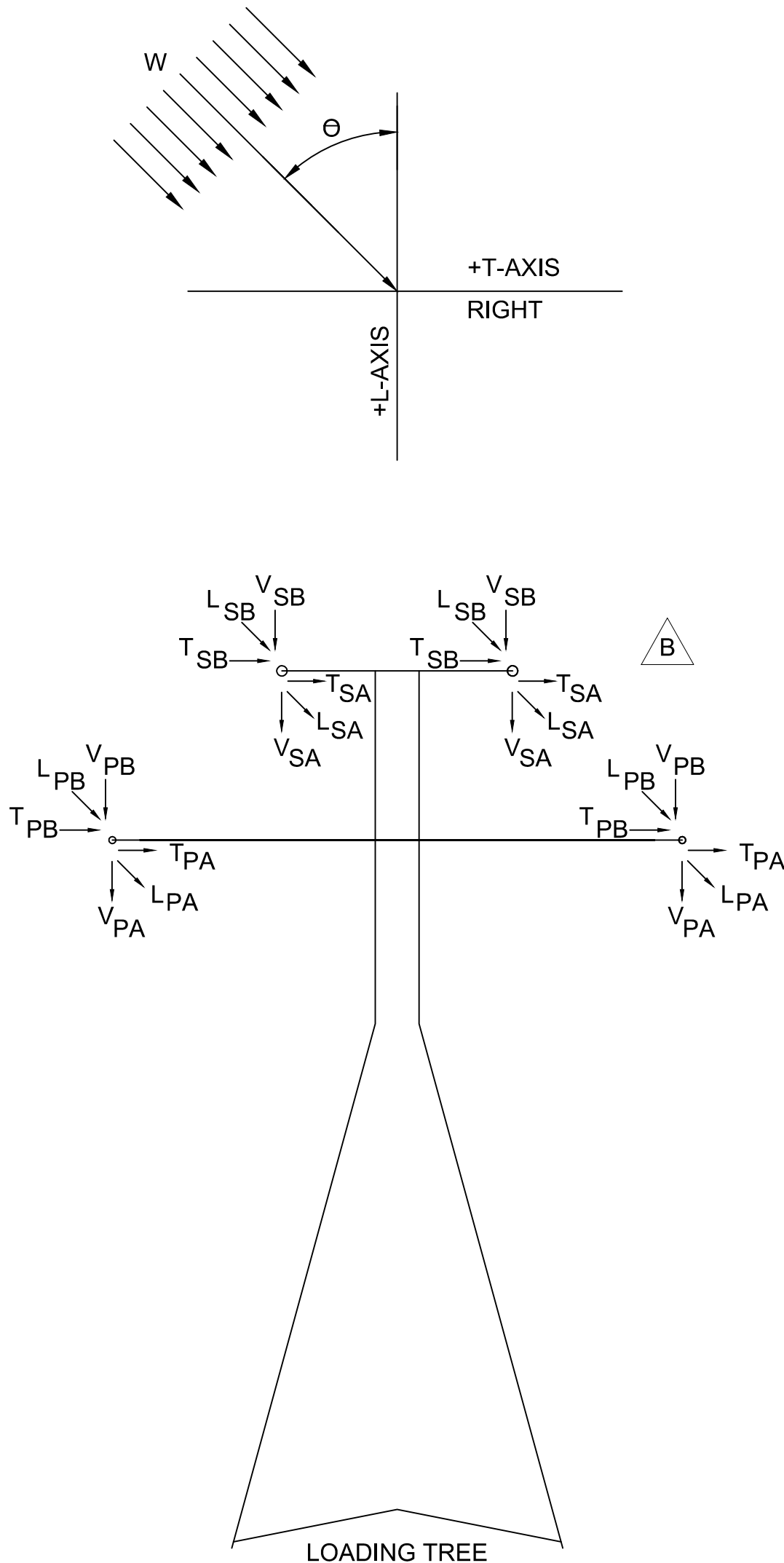
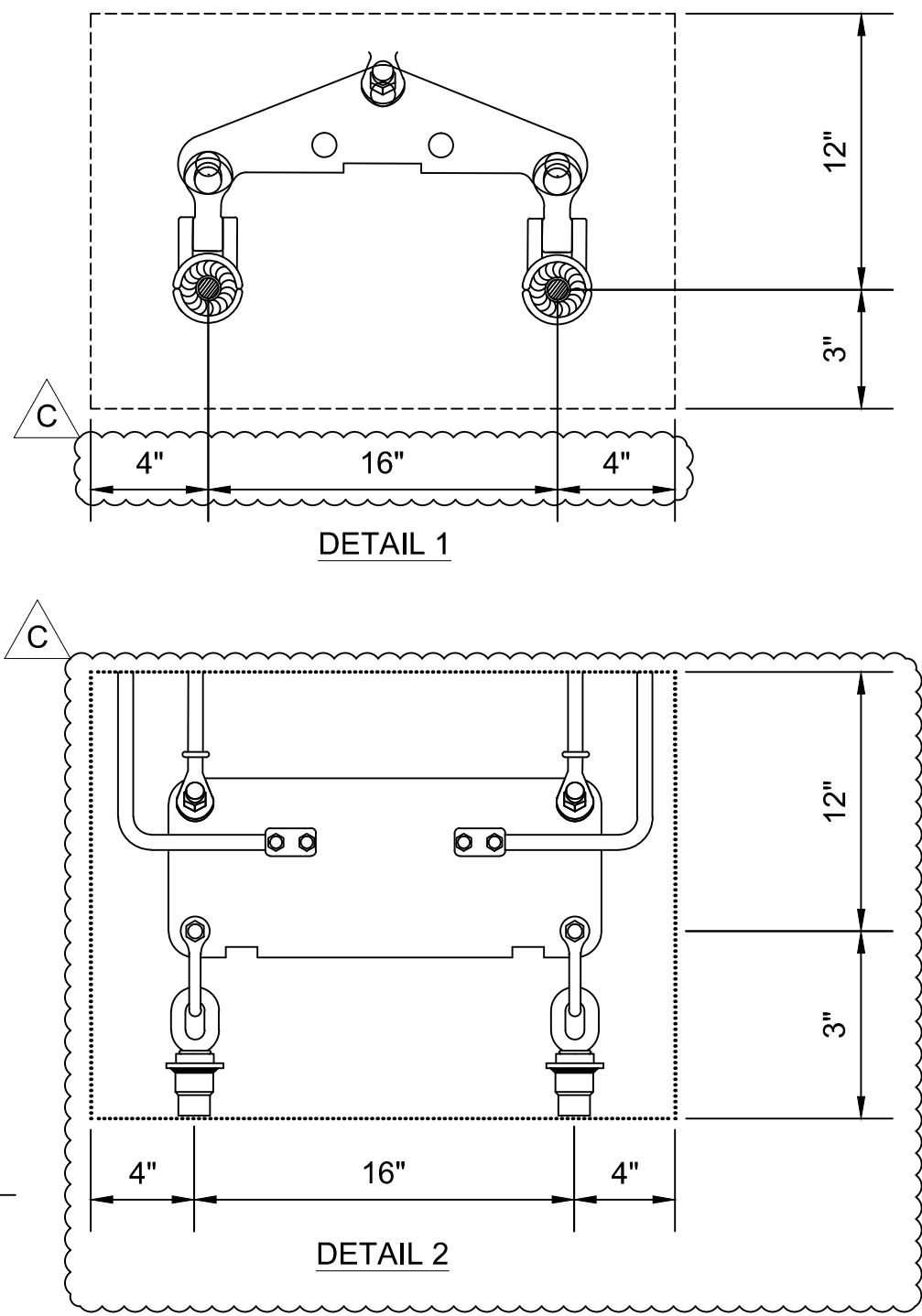
1. HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
2. STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
3. BOX ARMS SHALL HAVE PLATE ATTACHMENT HOLE AT EACH CORNER AND AT MIDPOINT.
4. FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

CONTRACT SERIES										 THE NORTHERN PASS			B
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REV	DESCRIPTION	ENG./PE#	DATE	DRN	CHKD	APPR				320kV DC LIGHT DEADEND 0°-45° 32-SCHLT-LDG-045 LOAD & DESIGN DRAWING			
B	MISC. REVISIONS		5/21/15	KAK									
A	RELEASED FOR RFP BID		5/1/15	KAK									
DWG REV	EPN/DESCRIPTION	CONT./PE#	DATE	DRN	CHKD	APPR				SCALE NTS	FILE: LST-06-002.DWG IMAGE:	DRAWING NO. LST-06-002	





- NOTES:
- 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.



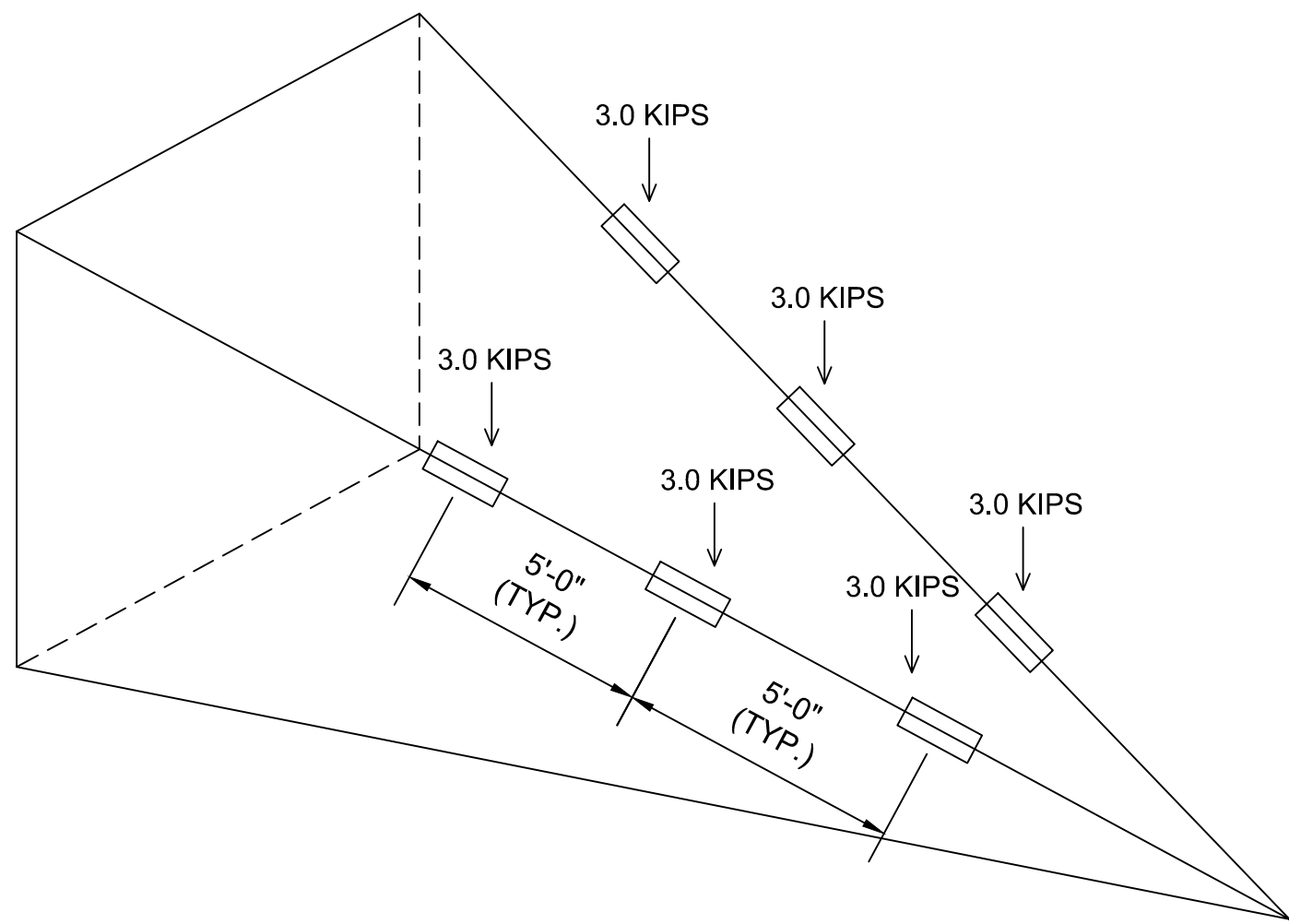
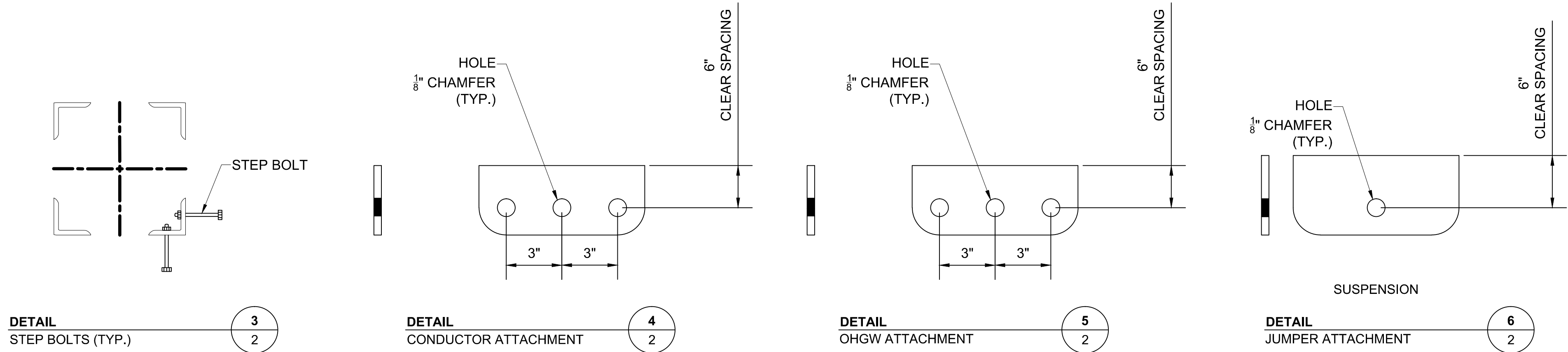
STRUCTURE NAME: 32-SCHLT-HDG-090																			
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)																			
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)																			
WIND SPAN AHEAD (FT): 550 WIND SPAN BACK (FT): 550																			
WEIGHT SPAN AHEAD (FT): 825 WEIGHT SPAN BACK (FT): 825																			
LINE ANGLE: 45 - 90 DEGREES																			
LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	w (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.41	7.50	8.89	1.41	7.50	-8.89	13.36	54.76	67.99	13.36	54.76	-67.99	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.42	3.79	4.17	0.42	3.79	-4.17	5.52	31.98	35.73	5.52	31.98	-35.73	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.97	6.12	7.40	1.97	6.12	-7.40	12.47	38.32	48.17	12.47	38.32	-48.17	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	9.16	11.13	3.51	9.16	-11.13	16.96	48.95	61.57	16.96	48.95	-61.57	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	4.40	5.39	0.94	4.40	-5.39	8.91	32.63	41.21	8.91	32.63	-41.21	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	4.17	-5.08	8.91	29.38	36.96	8.91	29.38	-36.96	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	0.28	0.00	8.91	29.38	36.96	8.91	1.09	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.38	0.25	1.98	3.78	-4.83	30.33	11.55	2.10	9.63	31.91	-40.88	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.64	4.18	5.47	2.64	4.18	-5.47	12.84	33.55	43.83	12.84	33.55	-43.83	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.42	3.49	4.17	0.42	3.49	-4.17	5.52	29.66	35.73	5.52	29.66	-35.73	29.00	45.00	1.00
11	UPLIFT	-20.00	0.00	0.00	0.42	3.13	4.09	0.42	3.13	-4.09	5.52	30.65	40.04	5.52	30.65	-40.04	0.00	90.00	1.00

- GENERAL NOTES:
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
  - TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
  - EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
  - LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
  - ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
  - THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
  - SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
  - CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
  - CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
  - STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).
  - STRUCTURES SHALL ALSO BE DESIGNED WITH UPLIFT LOADING. UPLIFT SHALL BE CONSIDERED UNDER LOAD CASE 1, LOAD CASE 2, & LOAD CASE 11. FOR LOAD CASE 1 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.3 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -1.9 KIPS. FOR LOAD CASE 2 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -2.1 KIPS. FOR LOAD CASE 13 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -3 KIPS.

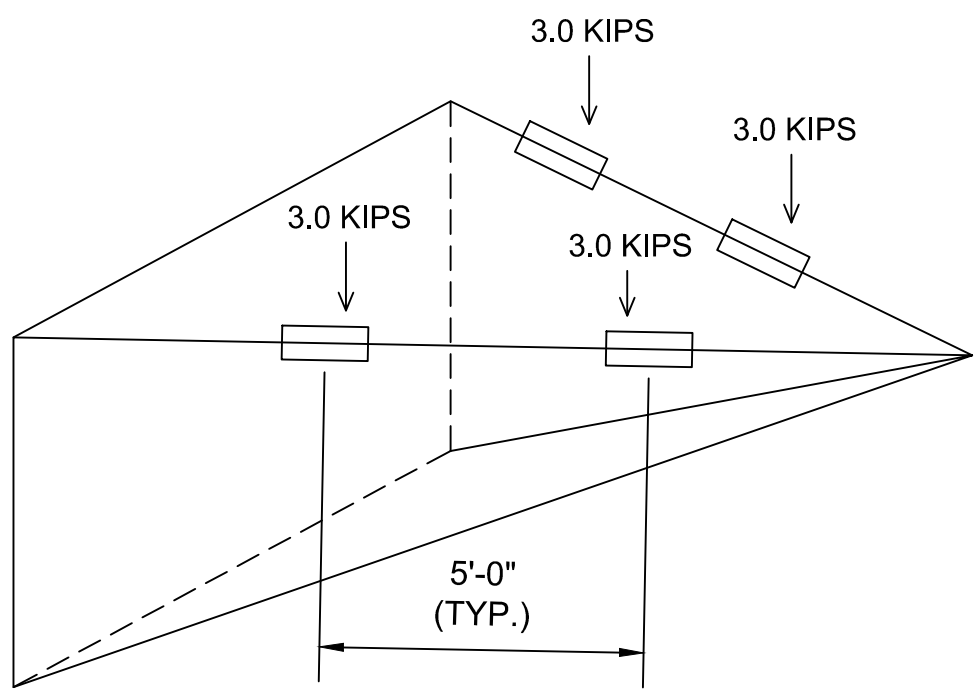
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PRELIMINARY - NOT FOR CONSTRUCTION





DETAIL FALL ARREST ATTACHMENT POINTS (TYPICAL FOR ALL CONDUCTOR CROSSARMS FRONT AND BACK, INCLUDING BOX ARMS.) 7/2



DETAIL FALL ARREST ATTACHMENT POINTS (TYPICAL FOR ALL OHSW CROSSARMS FRONT AND BACK, INCLUDING BOX ARMS.) 8/2

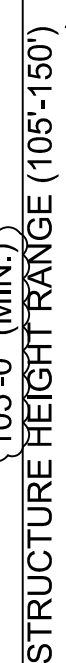
NOTES:


1. HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
2. STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
3. BOX ARMS SHALL HAVE PLATE ATTACHMENT HOLE AT EACH CORNER AND AT MIDPOINT.
4. FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

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PRELIMINARY - NOT FOR CONSTRUCTION





CONDITION	$\phi$	C	REMARKS
NU SWING $C_W$	0°	8'-6"	CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS
NU SWING $C_L$	25°	8'-1"	
NU SWING $C_S$	43°	6'-2"	
NU SWING $C_R$	54°	2'-6"	
NU SWING $C_W$	0°	<div style="border: 1px solid black; border-radius: 50%; padding: 10px; display: inline-block;"> 8'-6" </div> <div style="text-align: center;">  </div>	CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WALKOUT CLEARANCE



PRELIMINARY - NOT  
FOR CONSTRUCTION

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.45	1.40	0.00	8.94	4.99	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.43	1.08	0.00	3.49	6.26	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.03	0.99	0.00	9.14	3.09	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.76	1.20	0.00	11.12	3.56	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.96	0.63	0.00	5.96	2.29	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.96	0.62	0.00	5.96	2.21	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.96	0.52	5.50	5.96	1.66	13.68	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.58	0.31	0.27	13.87	1.56	1.21	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.66	0.21	0.00	8.79	0.93	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.43	0.62	0.00	3.49	3.53	0.00	29.00	45.00	1.00

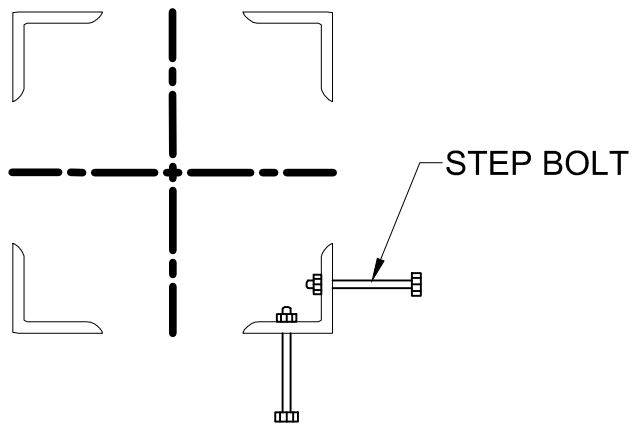
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
2. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
3. TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
4. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
6. THETA ( $\Theta$ ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
7. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
8. EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
9. LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
10. ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF NEAREST MEMBER.
11. THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 15 DEGREES.
12. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
13. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
14. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
15. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
16. CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
17. CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
18. PHI ( $\phi$ ) IS THE SWING ANGLE OF THE ASSEMBLY AND "C" IS THE REQUIRED ELECTRICAL CLEARANCE. THE STRUCTURE DESIGN SHALL PROVIDE CLEARANCE AS INDICATED IN TABLE 1.
19. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW. (FOR WALKOUT CLEARANCES, ASSUME A WORKER HEIGHT OF 6'-6").
20. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

[illegible]



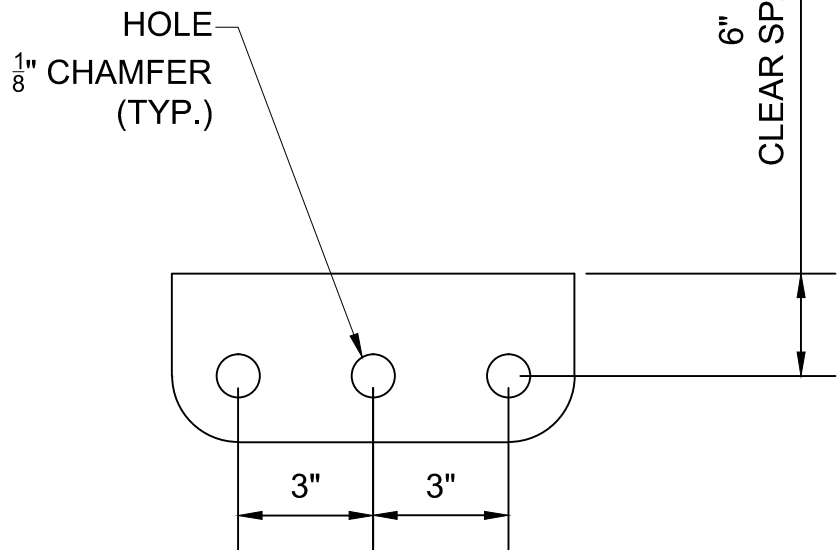
DETAIL  
STEP BOLTS (TYP.)

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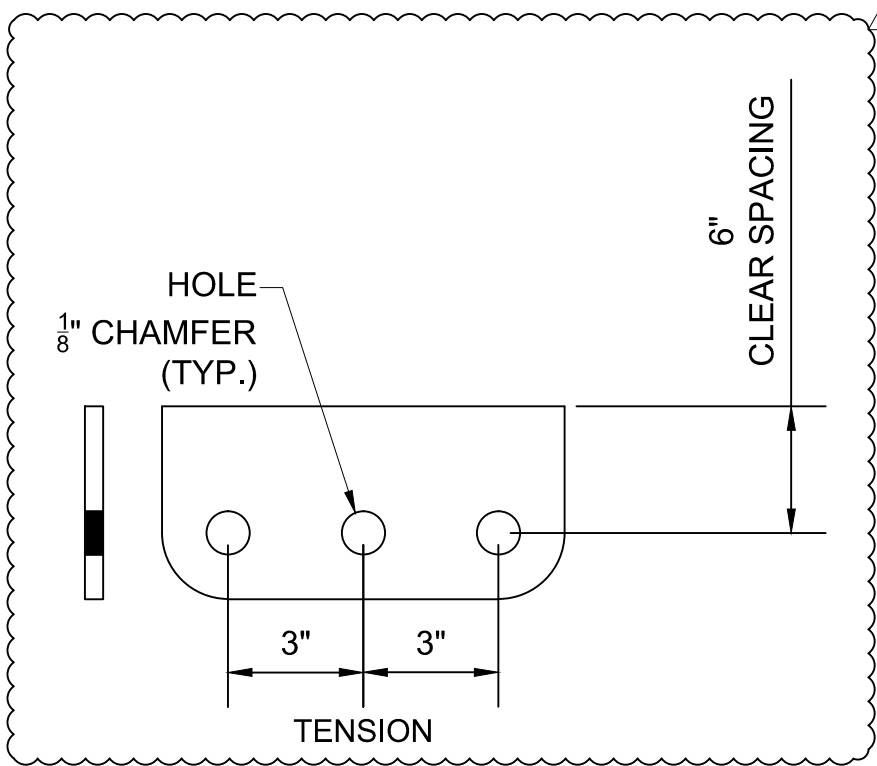
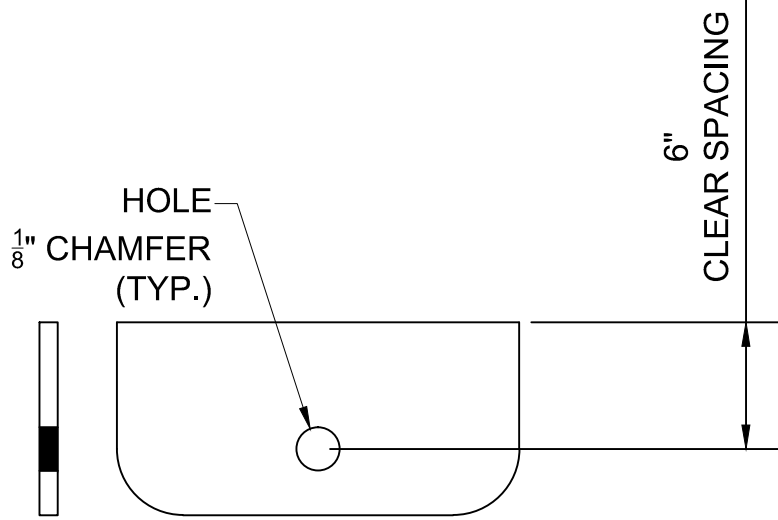
DETAIL  
CONDUCTOR ATTACHMENT

3  
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DETAIL  
OHGW ATTACHMENT

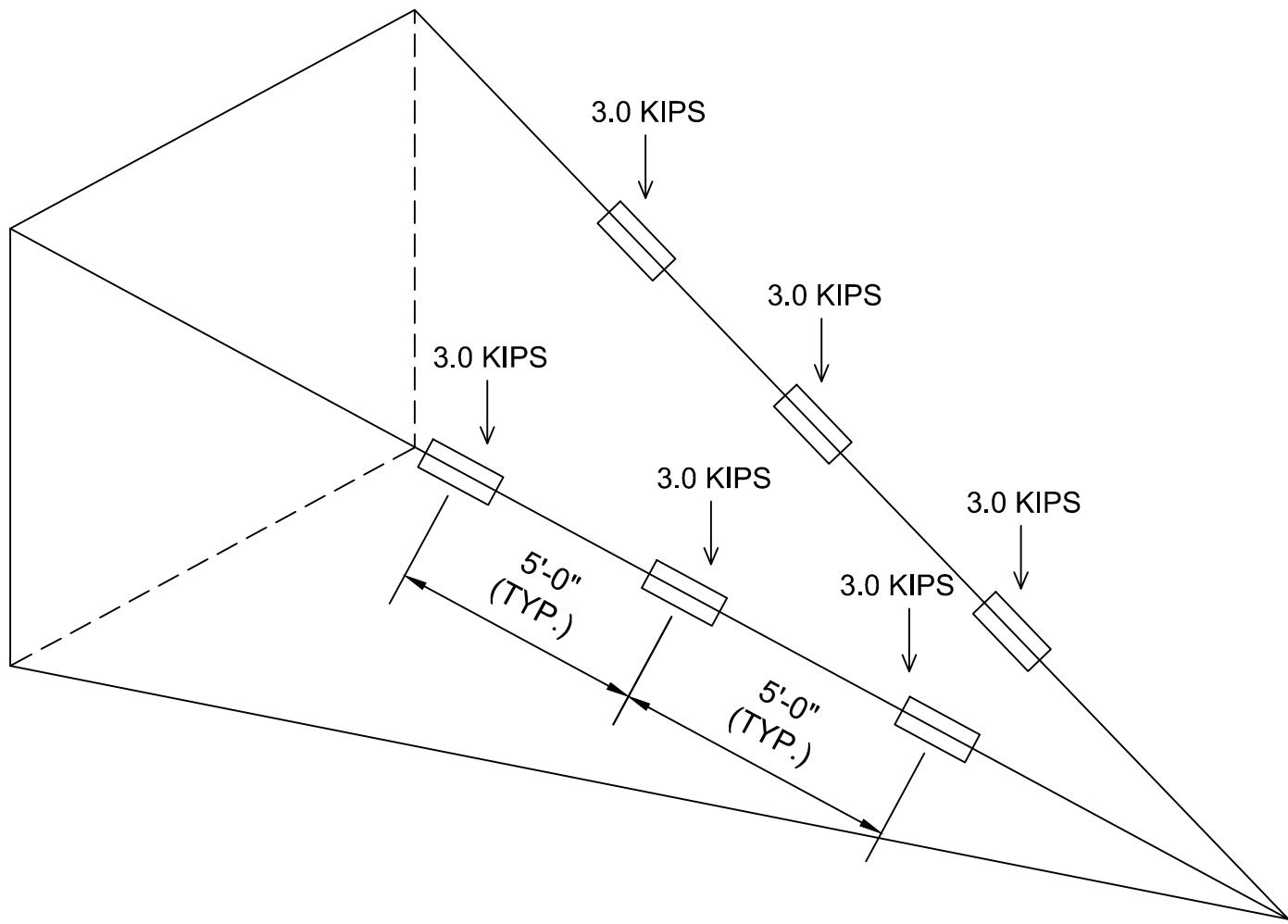
4  
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DETAIL

FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL  
CONDUCTOR CROSSARMS FRONT  
AND BACK, INCLUDING BOX ARMS.)

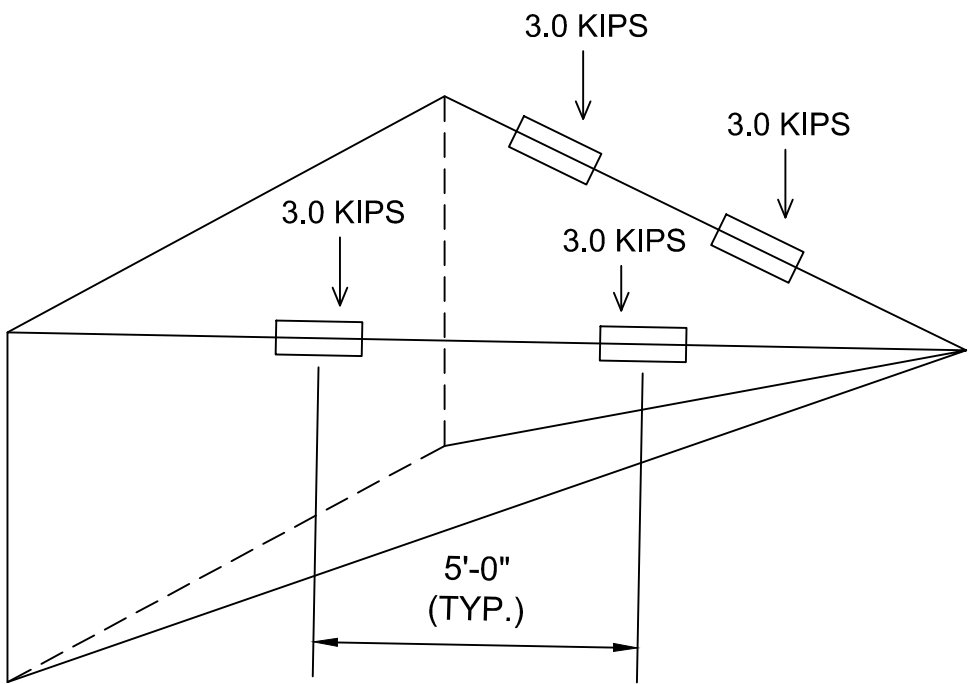
5  
2



DETAIL

FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL OHSW  
CROSSARMS FRONT AND BACK,  
INCLUDING BOX ARMS.)

6  
2



NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 4.
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PRELIMINARY - NOT  
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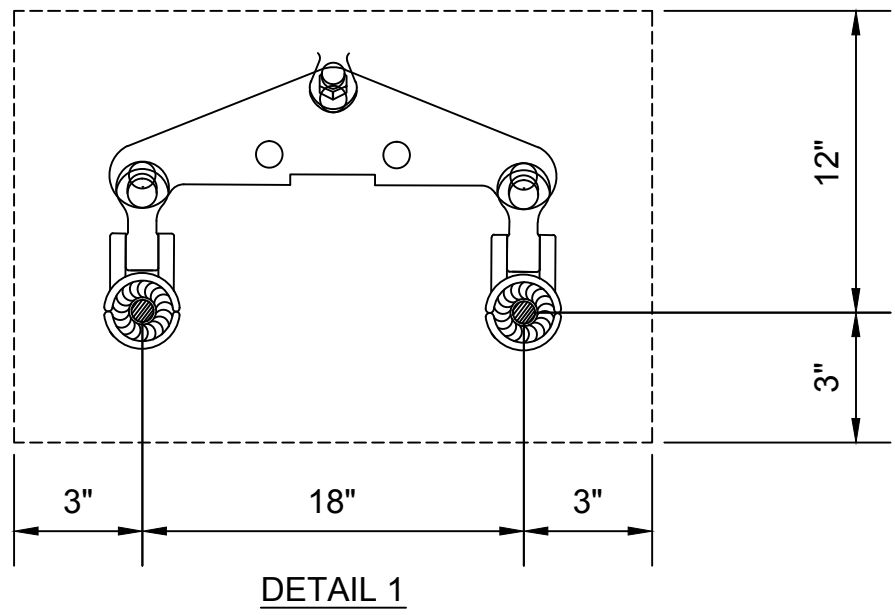


TABLE 1. INSULATOR SWING AND CLEARANCE

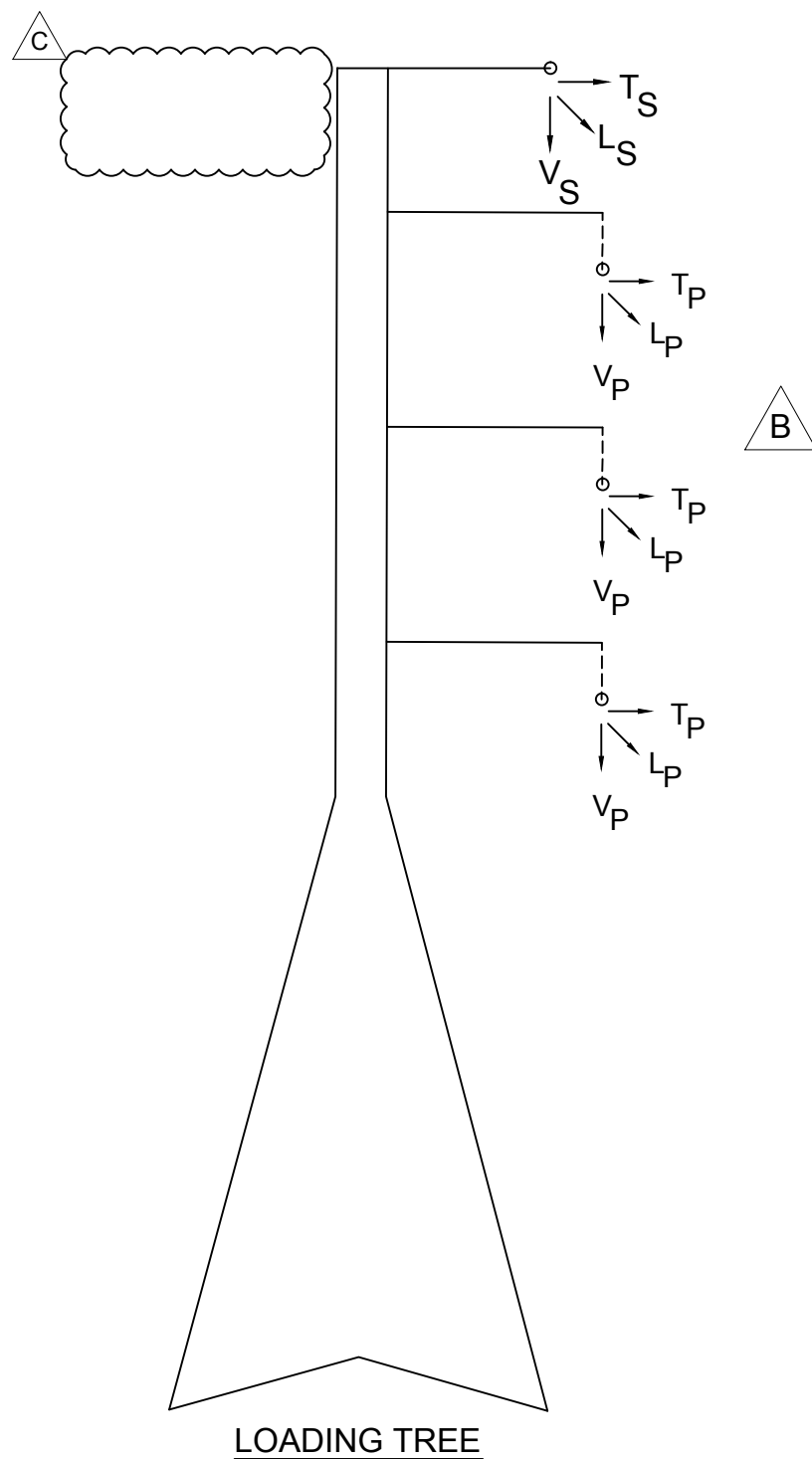
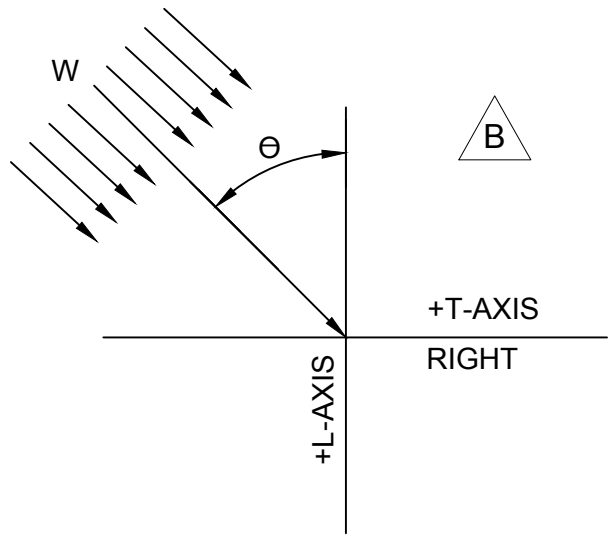
CONDITION	$\phi$	C	REMARKS
NU SWING $C_W$	0°	8'-6"	CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS
NU SWING $C_L$	25°	8'-1"	
NU SWING $C_S$	43°	6'-2"	
NU SWING $C_R$	54°	2'-6"	
NU SWING $C_W$	0°	8'-6"	CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WALKOUT CLEARANCE

STRUCTURE NAME: 30-SCVLT-HTG-002  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 850  
WEIGHT SPAN (FT): 1550  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	2.58	1.40	0.00	15.32	4.99	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.75	1.08	0.00	6.00	6.26	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	3.65	0.99	0.00	16.00	3.09	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	4.98	1.20	0.00	19.62	3.56	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.72	0.63	0.00	10.21	2.29	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.72	0.62	0.00	10.21	2.21	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.72	0.52	5.50	10.21	1.82	22.80	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.05	0.31	0.27	17.63	1.56	1.21	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	3.29	0.21	0.00	13.80	0.93	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.75	0.62	0.00	6.00	3.53	0.00	29.00	45.00	1.00


GENERAL NOTES:

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
- TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THETA ( $\theta$ ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
- EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
- LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
- ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF NEAREST MEMBER.
- THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 15 DEGREES.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
- SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
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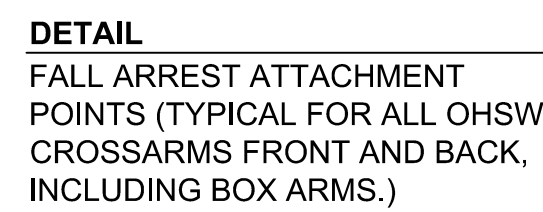
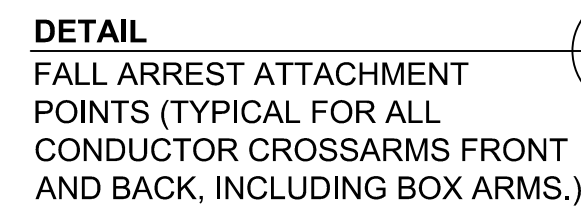
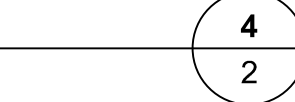
PRELIMINARY - NOT FOR CONSTRUCTION

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
C	MISC. REVISIONS		5/21/15	MSP			
B	UPDATED STRUCTURE HEIGHT RANGE		5/8/15	KAK			
A	RELEASED FOR RFP BID		5/1/15	KAK			
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	

 THE NORTHERN PASS	C
	DRAWN KAK
	ENGINEER AKO
	CHECKED TAB
	APPROVED
345kv AC HEAVY TANGENT 0°-2° 30-SCVLT-HTG-002 LOAD & DESIGN DRAWING	
SCALE NTS	DATE 5/1/15

FILE: LST-09-001.DWG	DRAWING NO. LST-09-001
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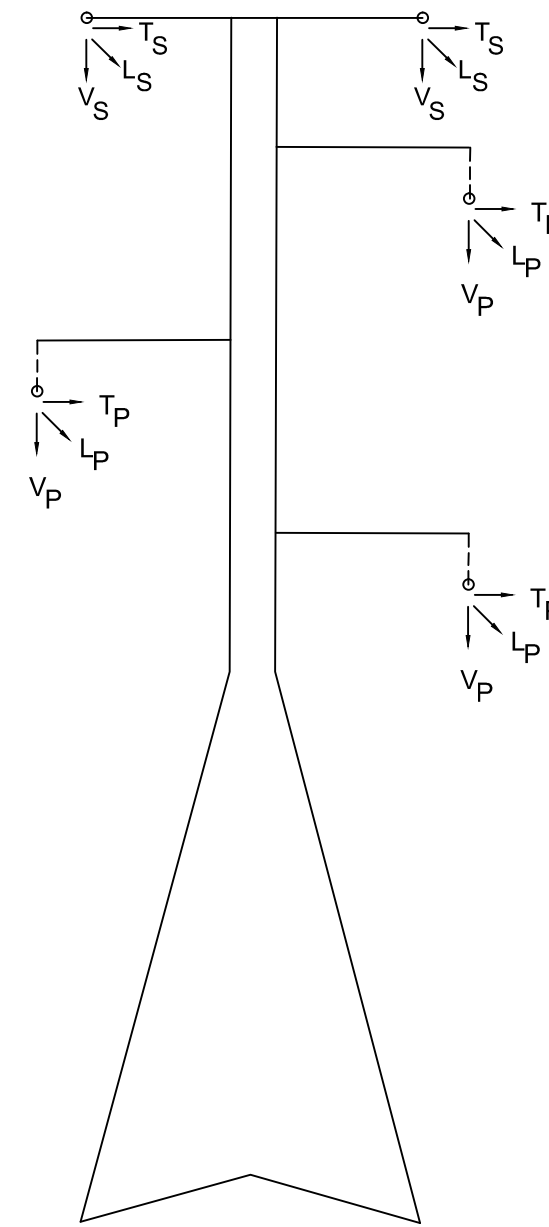
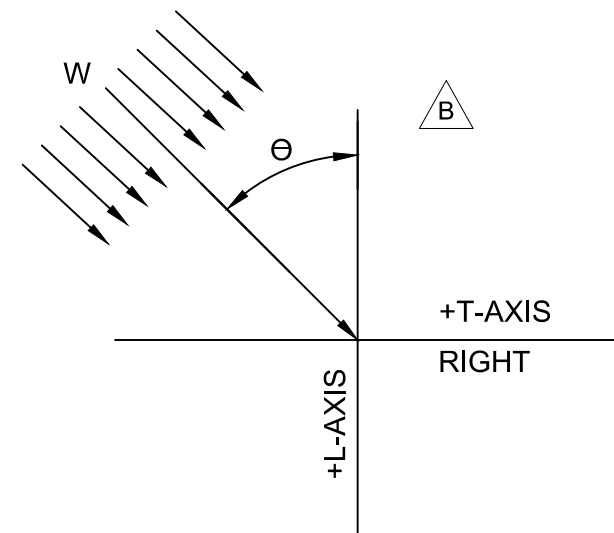




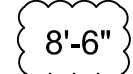

1. HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
2. STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
3. STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 4.
4. FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

<b>CONTRACT SERVICES</b>										 <b>THE NORTHERN PASS</b>	B
	-	-	-	-	-	-	-	-	-		DRAWN KAK
	REV	DESCRIPTION	ENG./PE#	DATE	DRN	CHKD	APPR				ENGINEER AKO
											CHECKED TAB
											APPROVED
											DATE 5/1/15
B	MISC. REVISIONS	-	5/21/15	KAK	-	-			SCALE NTS	FILE: LST-09-002.DWG IMAGE:	DRAWING NO. <b>LST-09-002</b>
A	RELEASED FOR RFP BID	-	5/1/15	KAK	-	-					
DWG REV	EPN/DESCRIPTION	CONT./PE#	DATE	DRN	CHKD	APPR					





## LOADING TREE

CONDITION	$\phi$	C	REMARKS
NU SWING C <sub>W</sub>	0°	8'-6"	CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS
NU SWING C <sub>L</sub>	25°	8'-1"	
NU SWING C <sub>S</sub>	43°	6'-2"	
NU SWING C <sub>R</sub>	54°	2'-6"	
NU SWING C <sub>W</sub>	0°	 	CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WALKOUT CLEARANCE

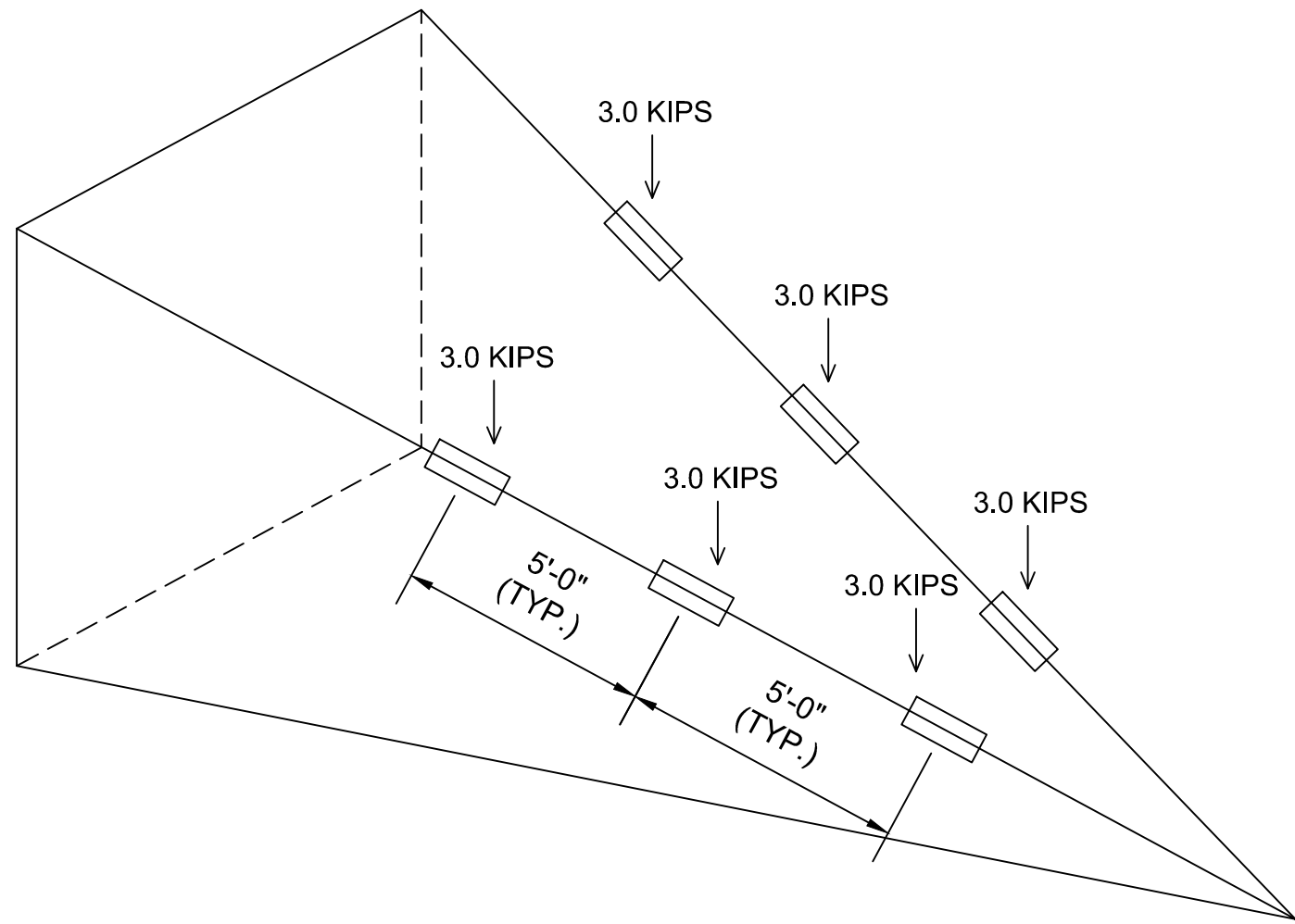
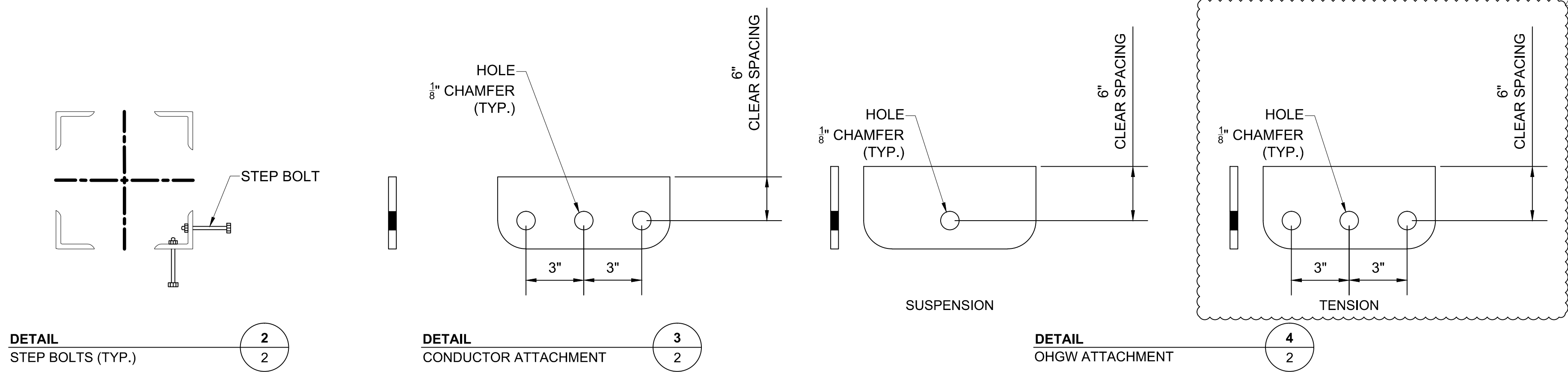
STRUCTURE NAME: 30-SCDLT-LTG-002  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 550  
WEIGHT SPAN (FT): 850  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	Ø	K
1	NESC 250B	0.00	0.50	39.53	1.45	1.03	0.00	8.94	3.73	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.43	0.75	0.00	3.49	4.34	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.03	0.74	0.00	9.14	2.39	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.76	0.90	0.00	11.12	2.76	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.96	0.48	0.00	5.96	1.79	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.96	0.47	0.00	5.96	1.71	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.96	0.37	5.50	5.96	1.16	13.68	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.58	0.27	0.27	13.87	1.30	1.21	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.66	0.21	0.00	8.79	0.93	0.00	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.43	0.46	0.00	3.49	2.57	0.00	29.00	45.00	1.00

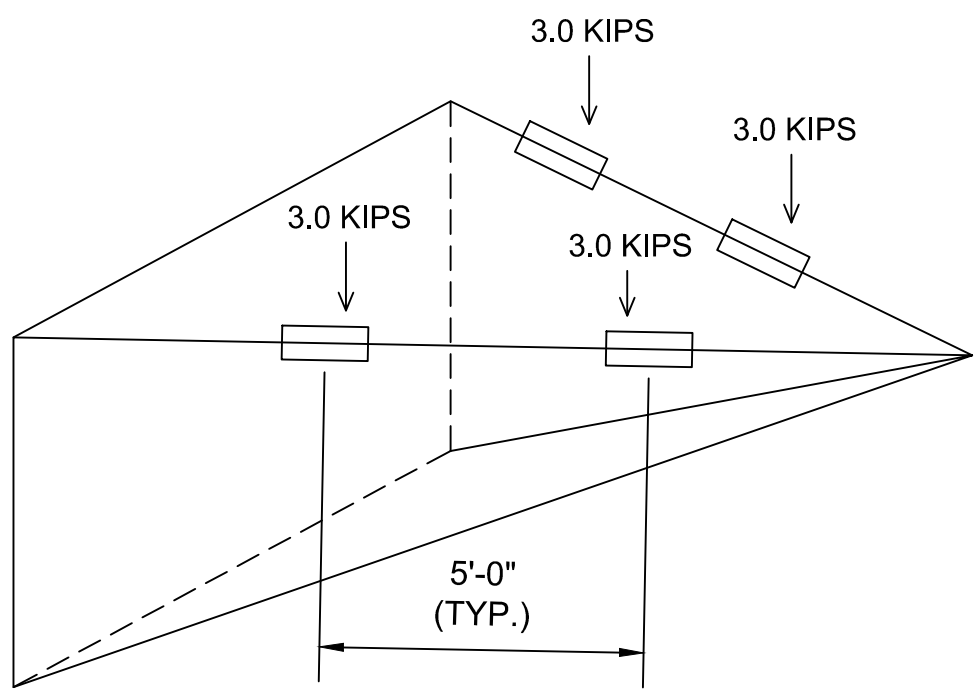
3. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
2. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
3. TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
4. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
6. THETA (Θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
7. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
8. EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
9. LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
10. ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF NEAREST MEMBER.
11. THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 15 DEGREES.
12. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0 - 20°. CLEARANCES MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
13. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
14. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
15. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
16. CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
17. CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
18. PHI (φ) IS THE SWING ANGLE OF THE ASSEMBLY AND "C" IS THE REQUIRED ELECTRICAL CLEARANCE. THE STRUCTURE DESIGN SHALL PROVIDE CLEARANCE AS INDICATED IN TABLE 1.
19. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW. (FOR WALKING CLEARANCES, ASSUME A WORKER HEIGHT OF 6'-6").
20. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

CONTRACT SERVICES																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
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**DETAIL**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL  
CONDUCTOR CROSSARMS FRONT  
AND BACK, INCLUDING BOX ARMS.) 5/2



**DETAIL**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL OHSW  
CROSSARMS FRONT AND BACK,  
INCLUDING BOX ARMS.) 6/2

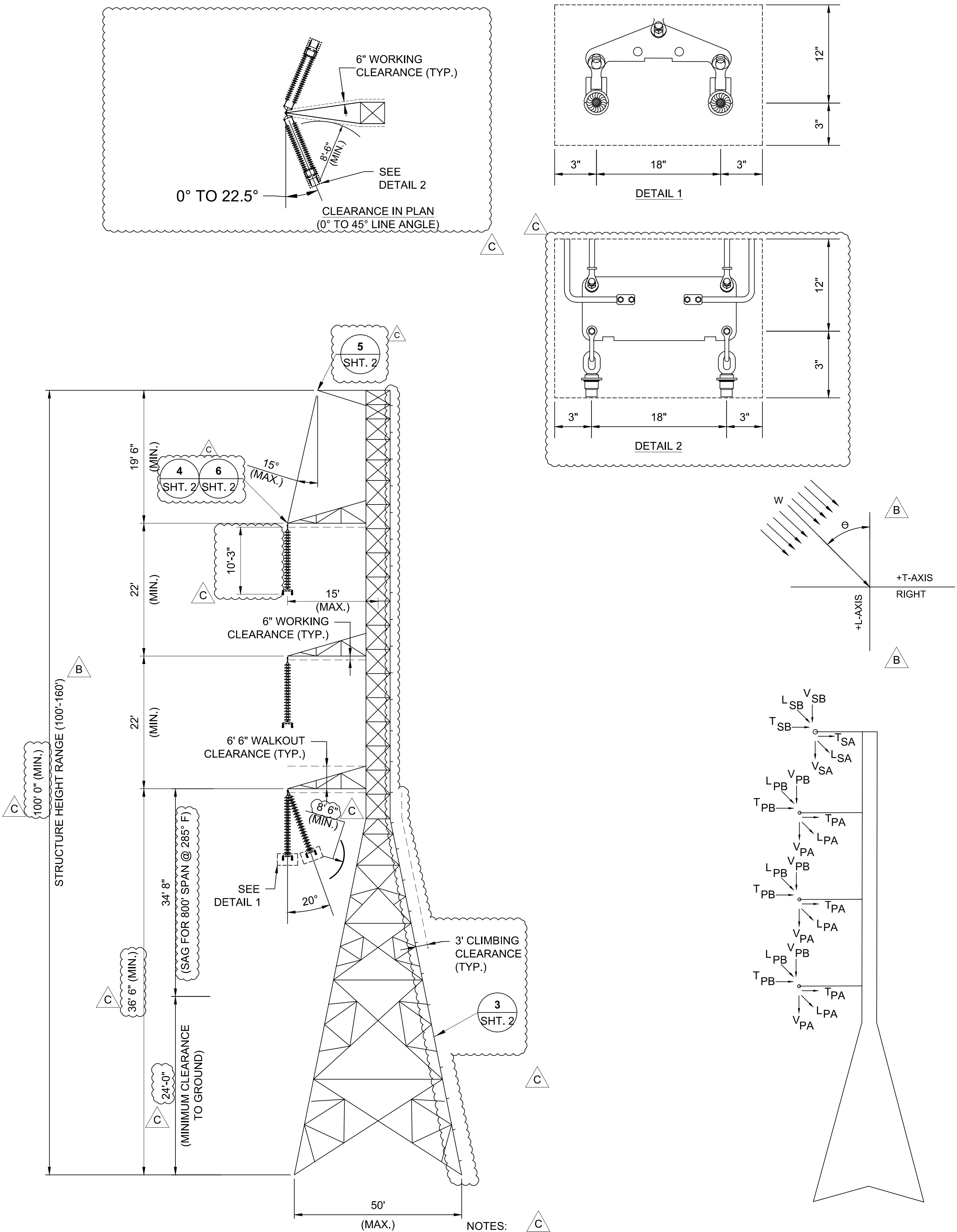
NOTES:

- HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
- STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
- STRUCTURE SHALL BE DESIGNED WITH SUSPENSION AND TENSION ATTACHMENT PLATES AS SHOWN IN DETAIL 4.
- FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

CONTRACT SERVICES							 THE NORTHERN PASS		<table><tr><td>B</td></tr><tr><td>DRAWN MSP</td></tr><tr><td>ENGINEER AKO</td></tr><tr><td>CHECKED TAB</td></tr><tr><td>APPROVED</td></tr><tr><td>DATE 5/1/15</td></tr></table>		B	DRAWN MSP	ENGINEER AKO	CHECKED TAB	APPROVED	DATE 5/1/15
	B															
	DRAWN MSP															
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						345kV AC DELTA TANGENT 0°-2° 30-SCDLT-LTG-002 LOAD & DESIGN DRAWING		<table><tr><td>SCALE NTS</td></tr><tr><td>FILE: LST-10-002.DWG</td></tr><tr><td>IMAGE:</td></tr><tr><td>DRAWING NO. LST-10-002</td></tr></table>		SCALE NTS	FILE: LST-10-002.DWG	IMAGE:	DRAWING NO. LST-10-002			
SCALE NTS																
FILE: LST-10-002.DWG																
IMAGE:																
DRAWING NO. LST-10-002																

PRELIMINARY - NOT  
FOR CONSTRUCTION





NOTES:


1. 8'-6" CLEARANCE MUST BE CONSIDERED FROM CLIMBING, WORKING, AND WALKOUT CLEARANCES.
2. 8'-1" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.

STRUCTURE NAME: 30-SCVLT-LDG-045  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 400 WIND SPAN BACK (FT): 400  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 0 - 45 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSb (k)	TSb (k)	LSb (k)	VPA (k)	TPA (k)	LPA (k)	VPb (k)	TPb (k)	LPb (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	4.19	9.62	0.84	4.19	-9.62	6.50	17.45	41.24	6.50	17.45	-41.24	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	2.16	4.51	0.26	2.16	-4.51	2.48	11.41	23.11	2.48	11.41	-23.11	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	3.40	8.01	1.15	3.40	-8.01	6.11	13.00	31.53	6.11	13.00	-31.53	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	4.20	9.92	1.56	4.20	-9.92	7.22	15.22	36.98	7.22	15.22	-36.98	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	2.43	5.83	0.56	2.43	-5.83	4.33	10.23	24.99	4.33	10.23	-24.99	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	2.31	5.50	0.56	2.31	-5.50	4.33	9.39	22.80	4.33	9.39	-22.80	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	2.31	5.50	0.56	2.31	0.00	4.33	9.39	22.80	4.33	0.67	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.47	0.27	1.74	2.06	-5.23	14.89	6.78	1.21	5.06	9.33	-23.49	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.33	2.26	5.92	2.33	2.26	-5.92	6.75	10.21	26.68	6.75	10.21	-26.68	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.26	1.94	4.51	0.26	1.94	-4.51	2.48	10.13	23.11	2.48	10.13	-23.11	29.00	45.00	1.00
11	UPLIFT	-20.00	0.00	0.00	0.26	1.70	4.43	0.26	1.70	-4.43	2.48	7.92	20.69	2.48	7.92	-20.69	0.00	90.00	1.00

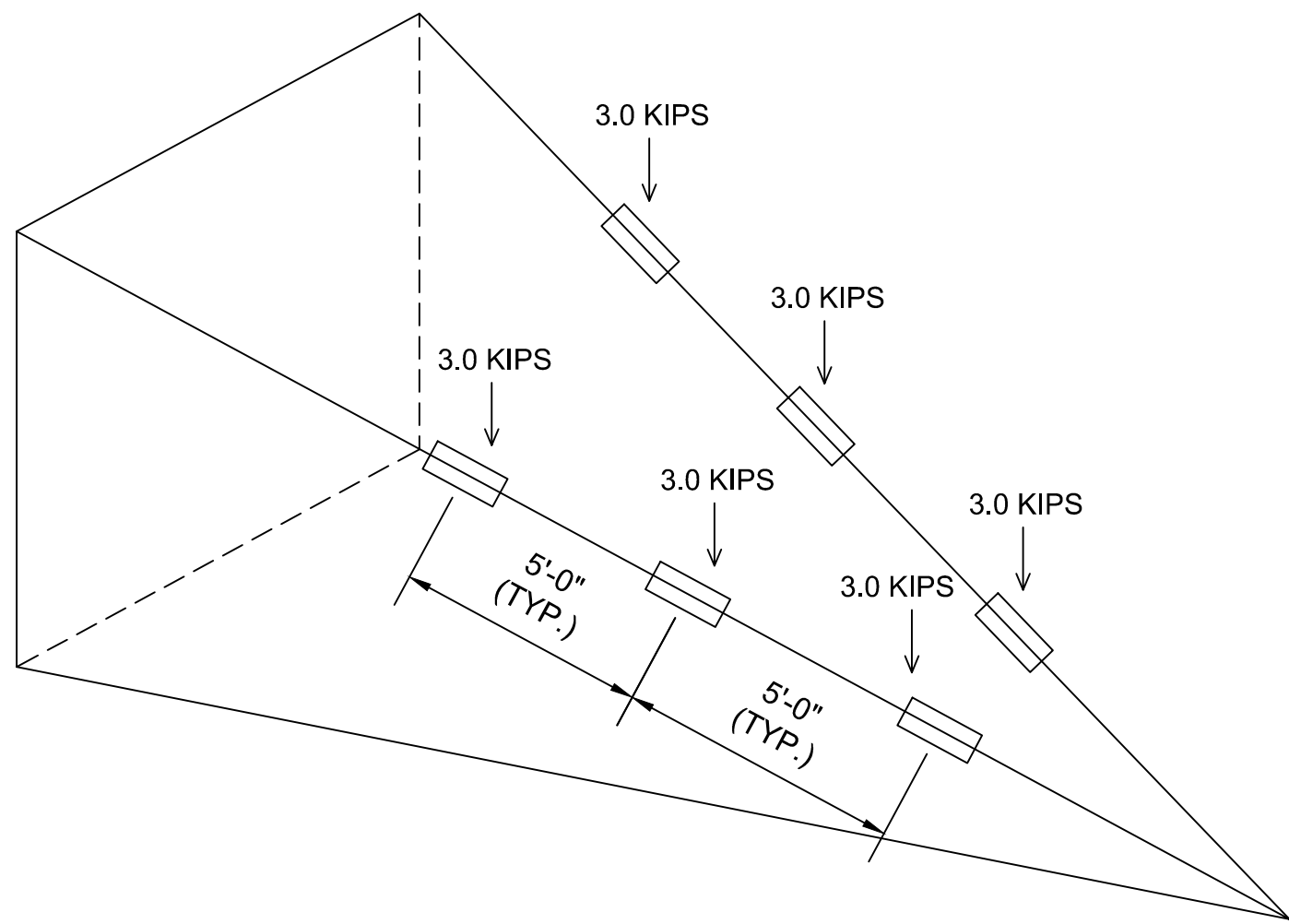
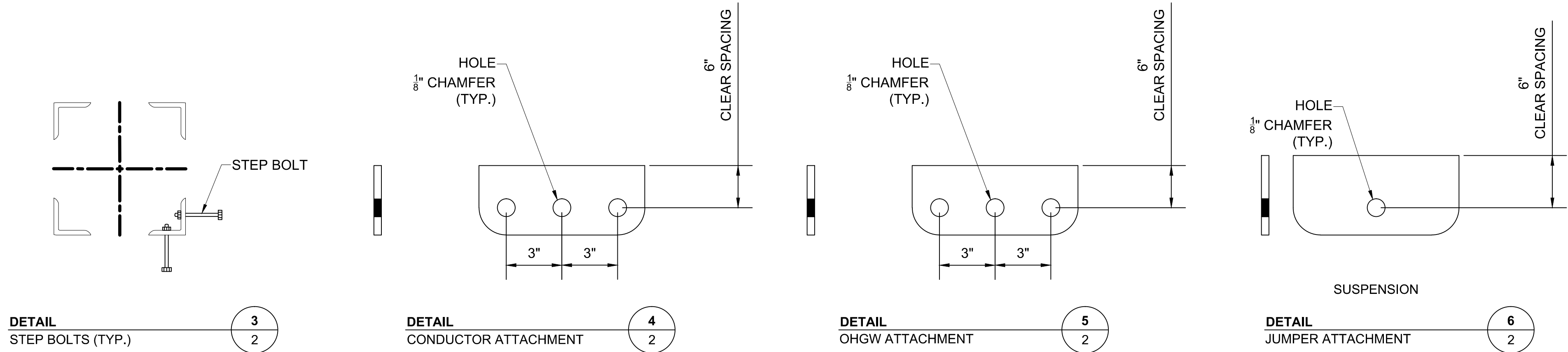
GENERAL NOTES:

1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
2. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
3. TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
4. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
6. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
7. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
8. EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
9. LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
10. ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
11. THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
12. ALL CLEARANCE CHECKS TO CONDUCTOR MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
13. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
14. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
15. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
16. CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
17. CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
18. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
19. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).
20. STRUCTURES SHALL ALSO BE DESIGNED WITH UPLIFT LOADING. UPLIFT SHALL BE CONSIDERED UNDER LOAD CASE 1, LOAD CASE 2, & LOAD CASE 11. FOR LOAD CASE 1 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH 0 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH 0 KIPS. FOR LOAD CASE 2 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH 0 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH 0 KIPS. FOR LOAD CASE 13 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.1 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -.8 KIPS.

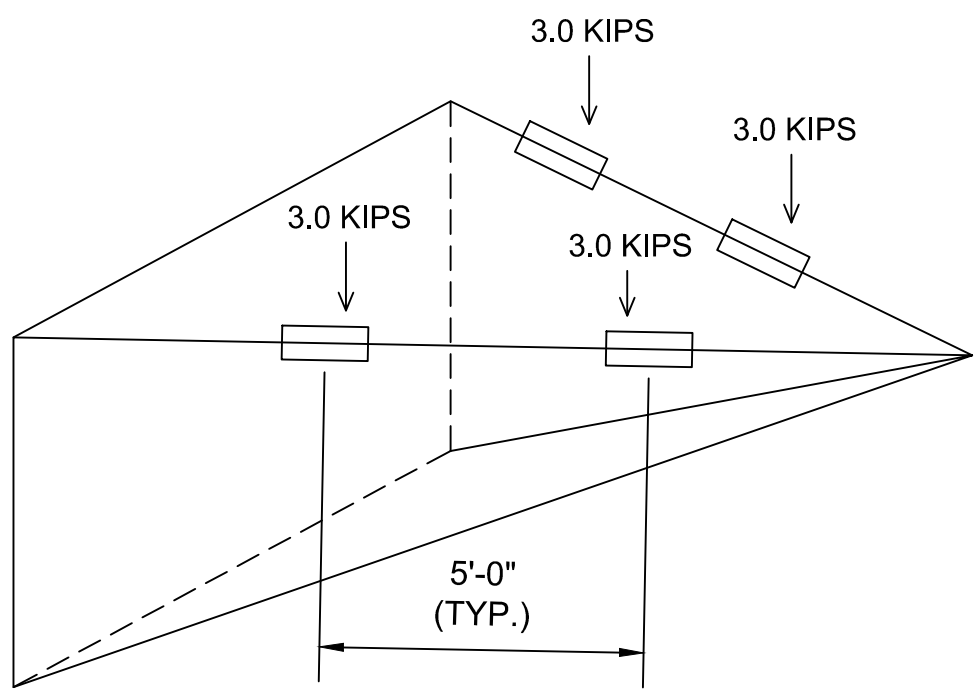
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										DRAWN MSP
										ENGINEER AKO
										CHECKED TAB
C		MISC. REVISIONS		5/21/15	MSP			SCALE NTS FILE: LST-11-001.DWG IMAGE: DRAWING NO. LST-11-001		DATE 5/1/15
B		MISC. REVISIONS		5/8/15	KAK					
A		RELEASED FOR RFP BID		5/1/15	MSP					
DWG REV		EPN/DESCRIPTION		CONT/PE#	DATE	DRN	CHKD	APPR		

PRELIMINARY - NOT FOR CONSTRUCTION






DETAIL FALL ARREST ATTACHMENT POINTS (TYPICAL FOR ALL CONDUCTOR CROSSARMS FRONT AND BACK, INCLUDING BOX ARMS.) 7/2



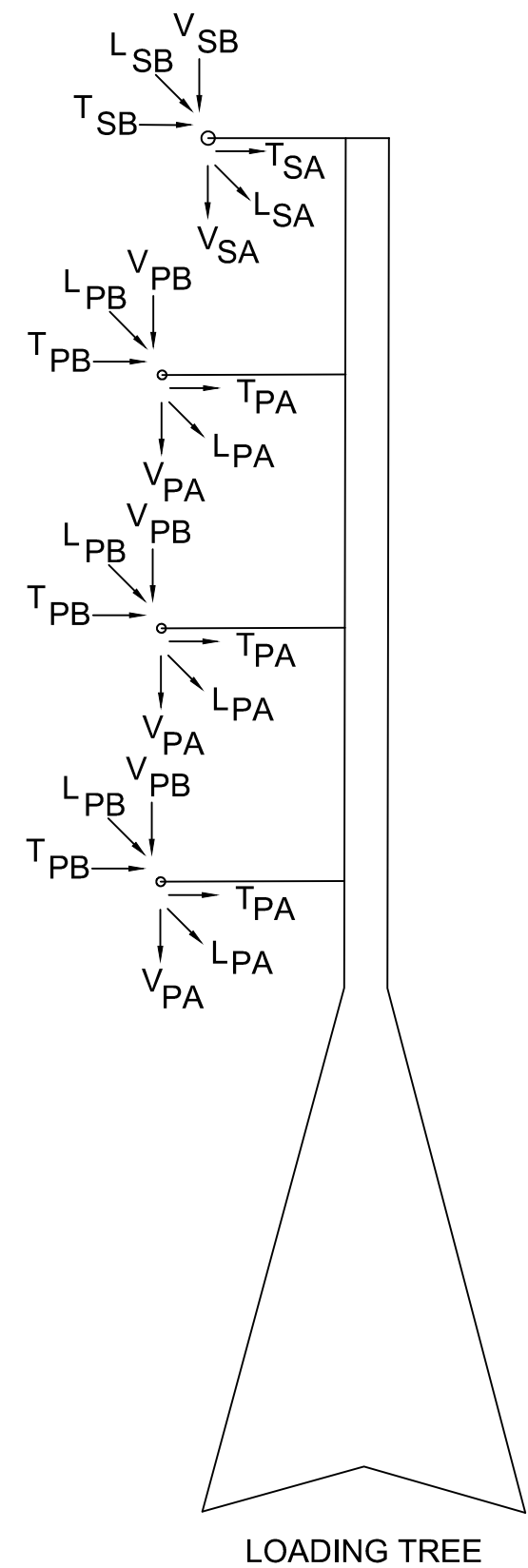
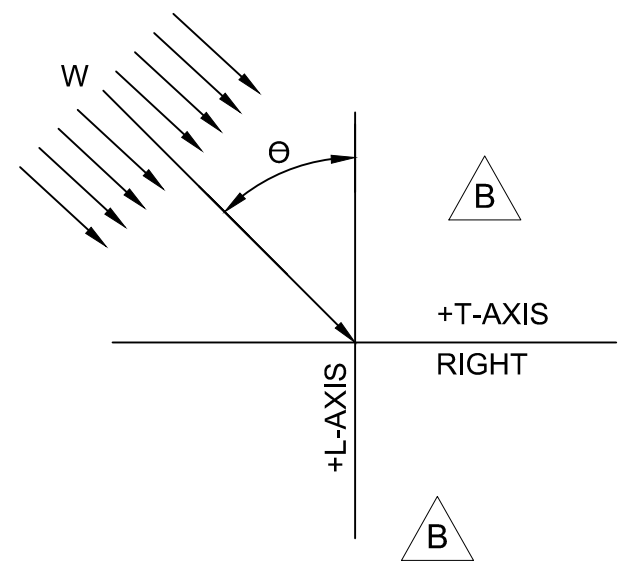
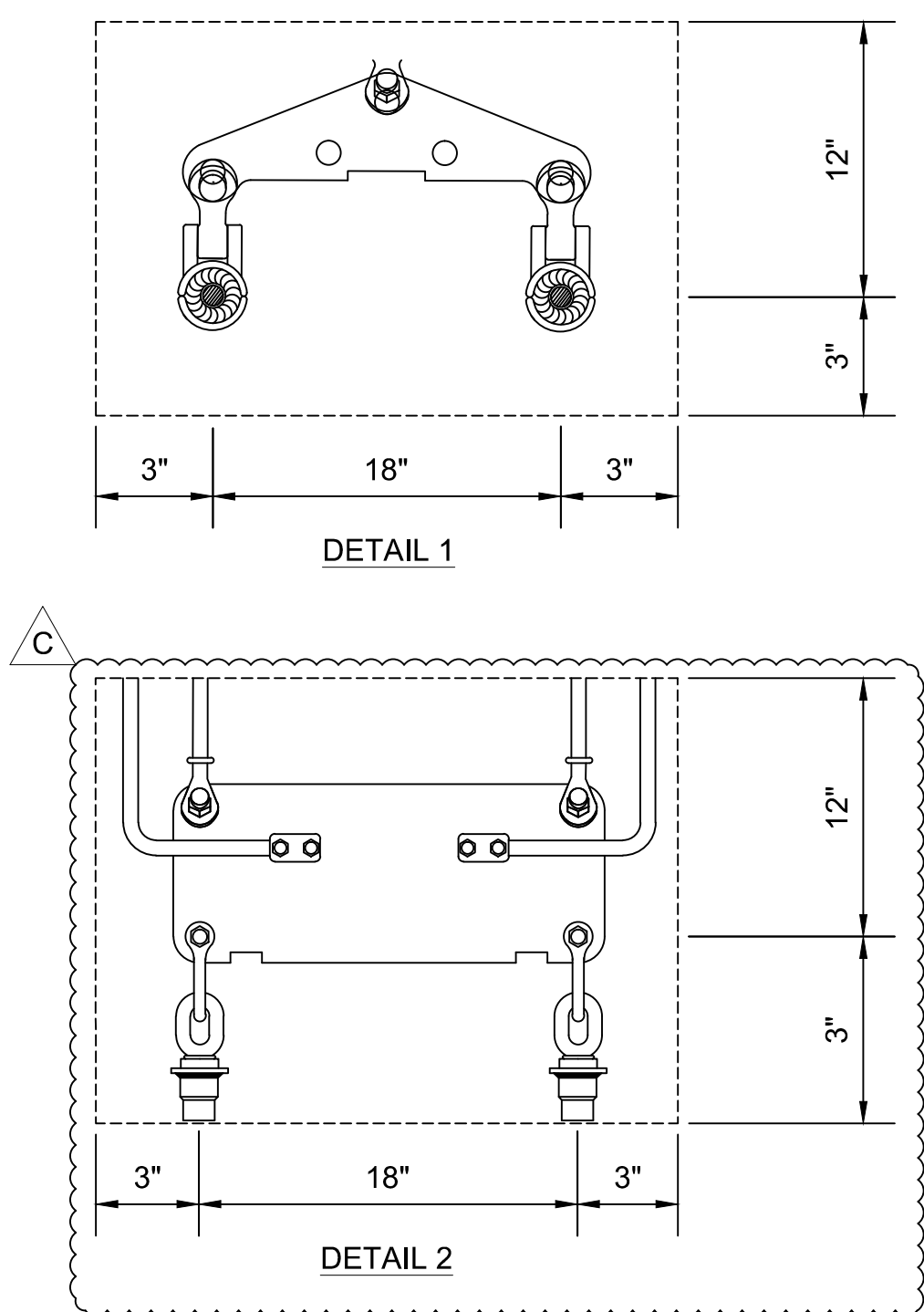
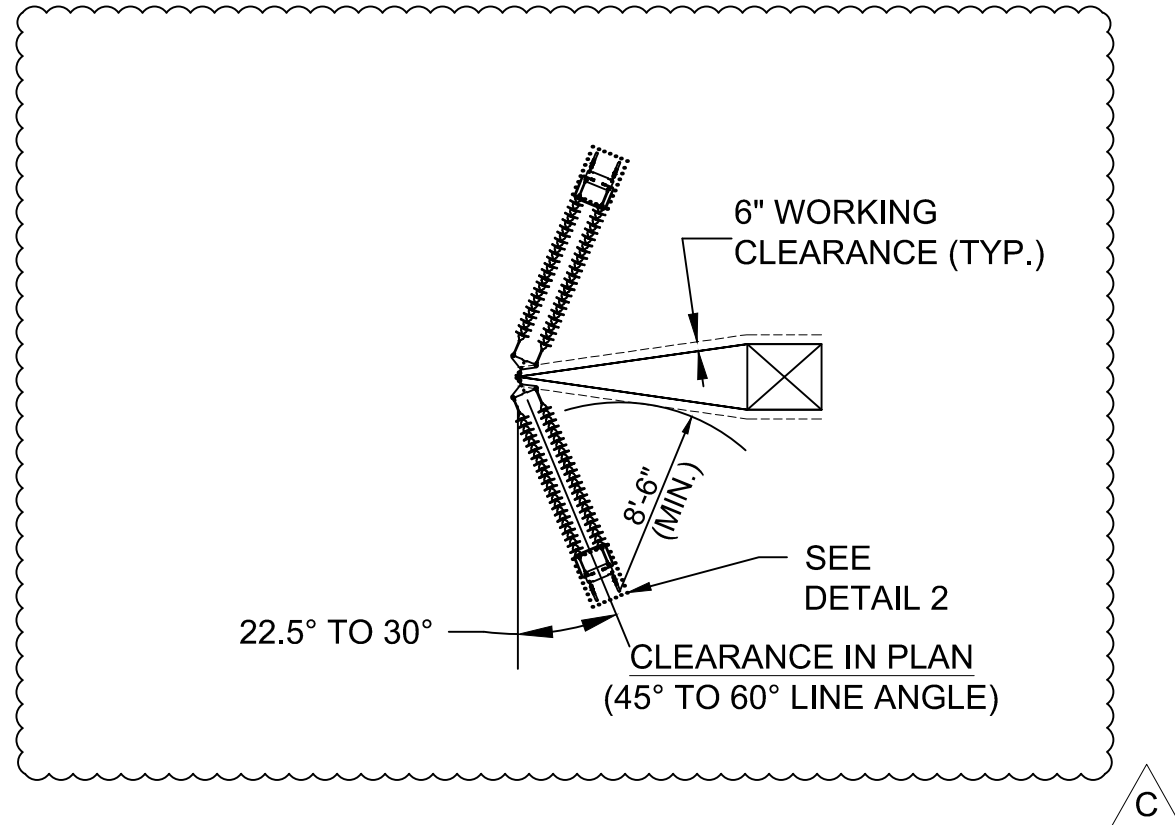
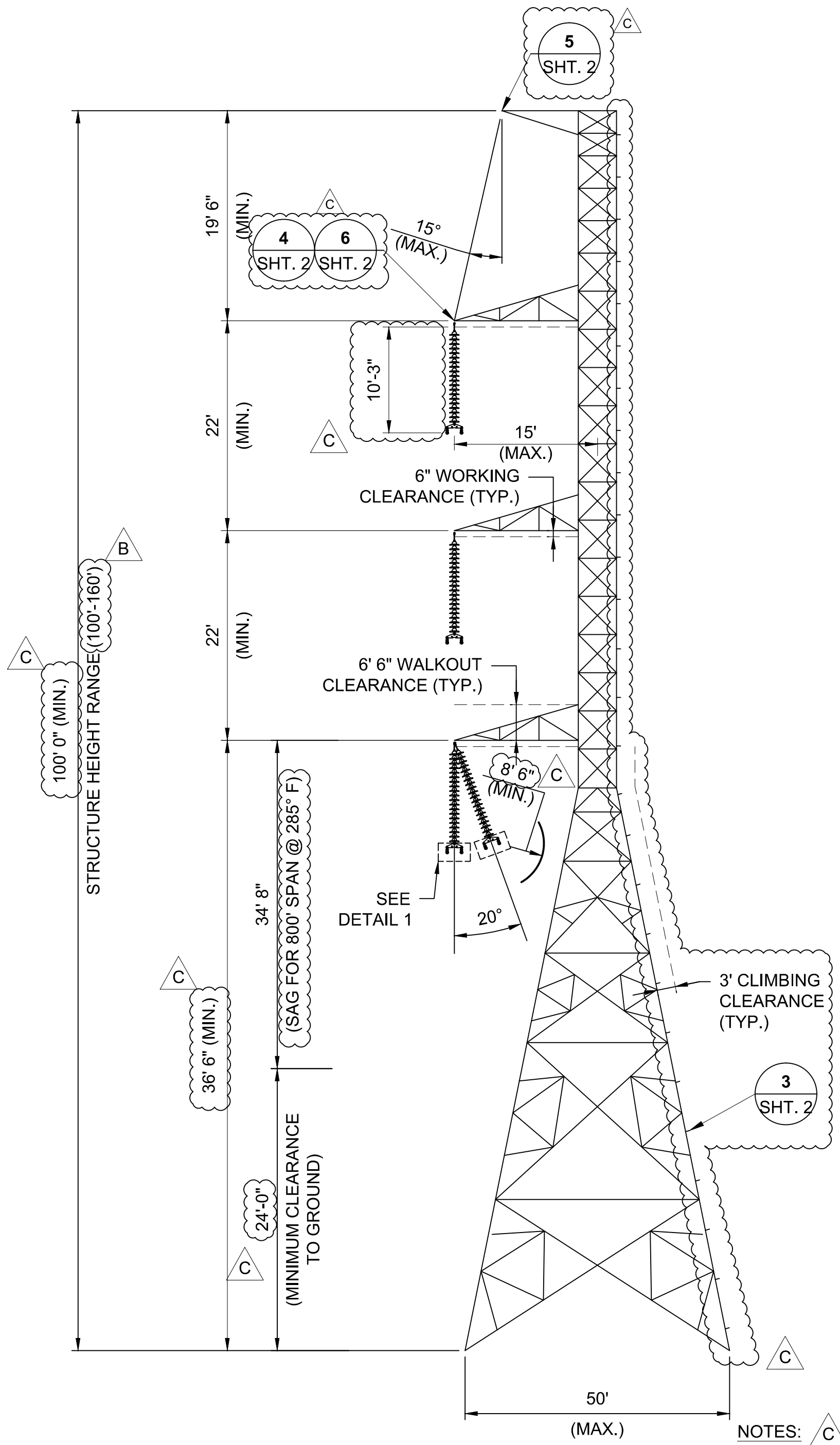
DETAIL FALL ARREST ATTACHMENT POINTS (TYPICAL FOR ALL OHSW CROSSARMS FRONT AND BACK, INCLUDING BOX ARMS.) 8/2

NOTES:

1. HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
2. STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16" INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
3. BOX ARMS SHALL HAVE PLATE ATTACHMENT HOLE AT EACH CORNER AND AT MIDPOINT.
4. FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

CONTRACT SERVICES								<div> THE NORTHERN PASS</div>		B	
										DRAWN MSP	
										ENGINEER AKO	
										CHECKED TAB	
										APPROVED	
										DATE 5/1/15	





- NOTES:
1. 8'-6" CLEARANCE MUST BE CONSIDERED FROM CLIMBING, WORKING, AND WALKOUT CLEARANCES.
  2. 8'-1" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.

STRUCTURE NAME: 30-SCVLT-MDG-060

345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)

OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)

WIND SPAN AHEAD (FT): 400    WIND SPAN BACK (FT): 400

WEIGHT SPAN AHEAD (FT): 475    WEIGHT SPAN BACK (FT): 475

LINE ANGLE: 45 - 60 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSb (k)	TSb (k)	LSb (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	5.32	8.89	0.84	5.32	-8.89	6.50	22.29	38.10	6.50	22.29	-38.10	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	2.69	4.17	0.26	2.69	-4.17	2.48	14.12	21.35	2.48	14.12	-21.35	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	4.34	7.40	1.15	4.34	-7.40	6.11	16.70	29.13	6.11	16.70	-29.13	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	5.36	9.17	1.56	5.36	-9.17	7.22	19.56	34.16	7.22	19.56	-34.16	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	3.12	5.39	0.56	3.12	-5.39	4.33	13.16	23.09	4.33	13.16	-23.09	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	2.95	5.08	0.56	2.95	-5.08	4.33	12.07	21.06	4.33	12.07	-21.06	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	2.95	5.08	0.56	0.20	0.00	4.33	12.07	21.06	4.33	0.67	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.45	0.25	1.74	2.67	-4.83	14.89	6.67	1.12	5.06	12.09	-21.70	3.45	90.00	1.50
9	MAINTENANCE	60.00	0.00	0.00	2.33	2.96	5.47	2.33	2.96	-5.47	6.75	13.34	24.65	6.75	13.34	-24.65	0.00	90.00	2.00
10	OBLIQUE WIND	60.00	0.00	100.00	0.26	2.47	4.17	0.26	2.47	-4.17	2.48	12.84	21.35	2.48	12.84	-21.35	29.00	45.00	1.00
11	UPLIFT	-20.00	0.00	0.00	0.26	2.22	4.09	0.26	2.22	-4.09	2.48	10.34	19.11	2.48	10.34	-19.11	0.00	90.00	1.00

- GENERAL NOTES:
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
  3. TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
  4. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
  7. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
  8. EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
  9. LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
  10. ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
  11. THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 15 DEGREES.
  12. ALL CLEARANCE CHECKS TO CONDUCTOR MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
  13. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  14. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
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  17. CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
  18. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
  19. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
C		MISC. REVISIONS		5/21/15	MSP		
B		MISC. REVISIONS		5/8/15	KAK		
A		RELEASED FOR RFP BID		5/1/15	MSP		
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR

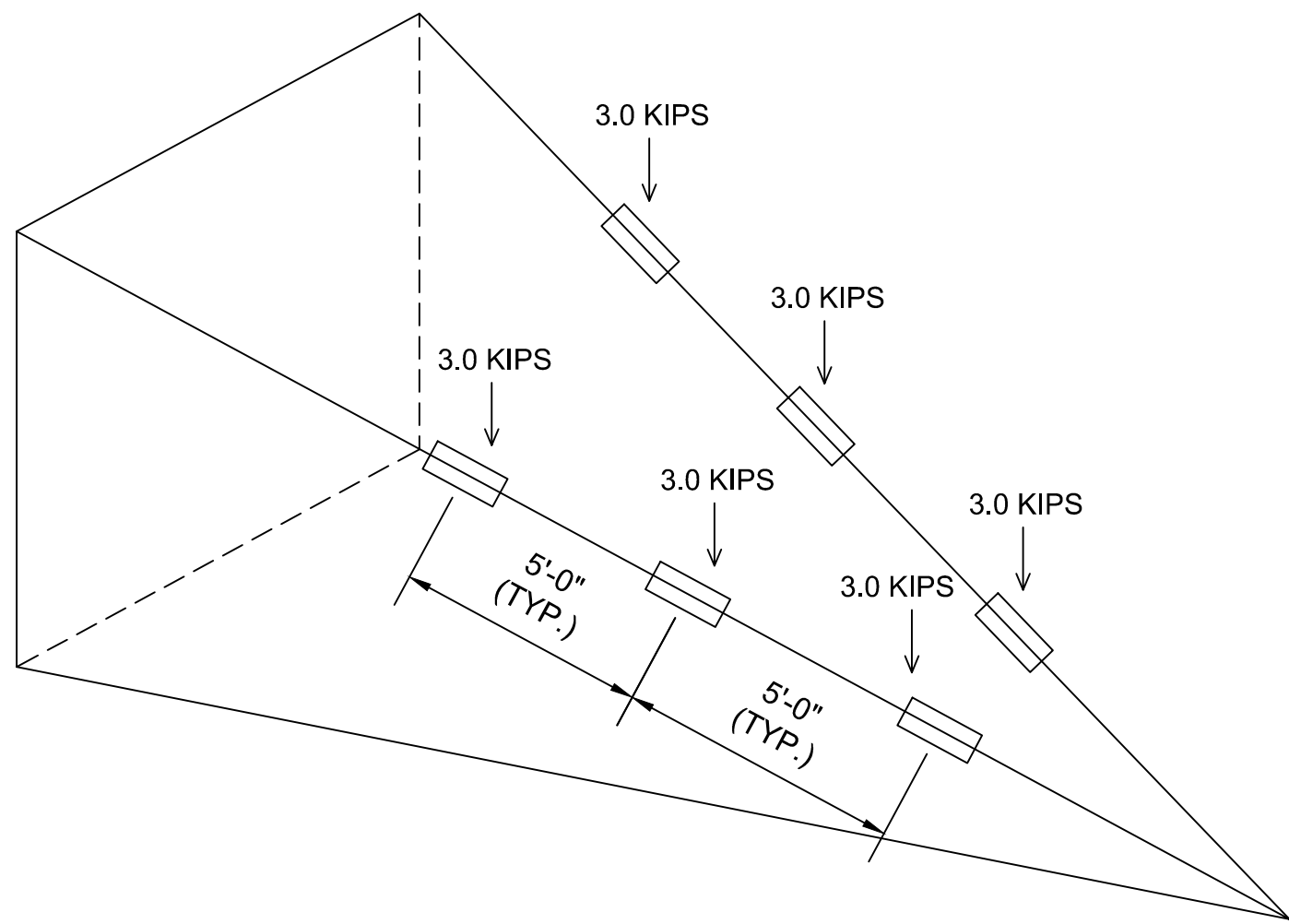
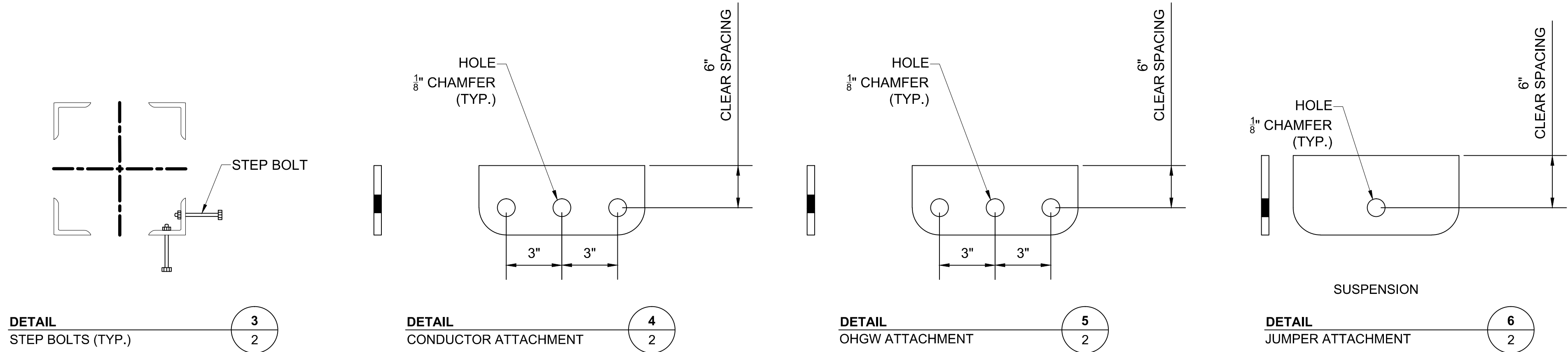
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30-SCVLT-MDG-060  
LOAD & DESIGN DRAWING

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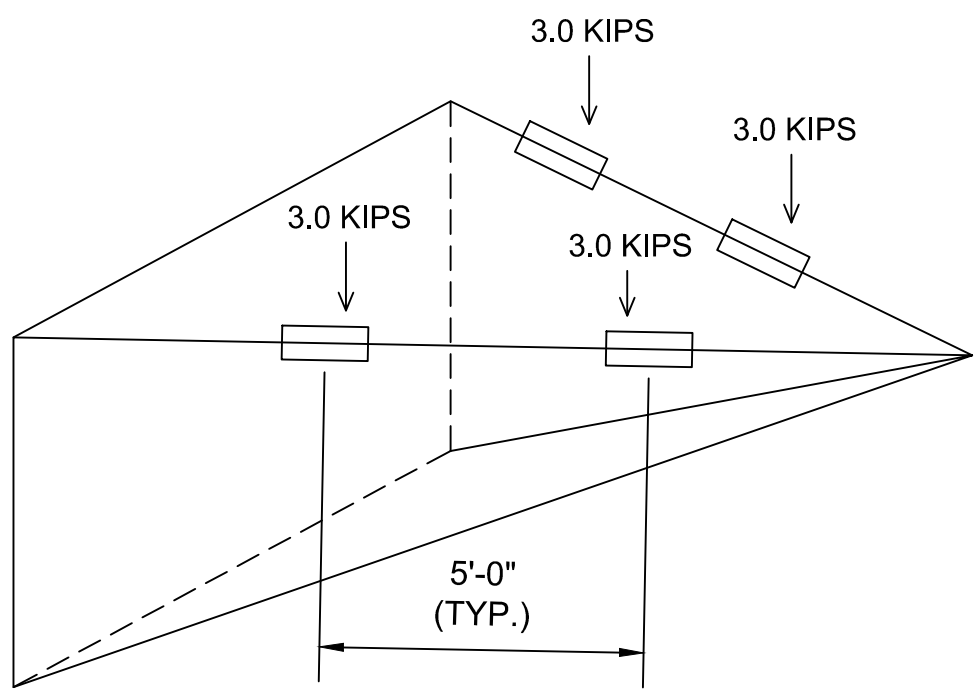
C	DRAWN MSP
ENGINEER AKO	CHECKED TAB
APPROVED	DATE 5/1/15

PRELIMINARY - NOT FOR CONSTRUCTION





**DETAIL 7**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL  
CONDUCTOR CROSSARMS FRONT  
AND BACK, INCLUDING BOX ARMS.)  
2



**DETAIL 8**  
FALL ARREST ATTACHMENT  
POINTS (TYPICAL FOR ALL OHSW  
CROSSARMS FRONT AND BACK,  
INCLUDING BOX ARMS.)  
2

NOTES:

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1. 5'-5" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
2. 10'-9" CLEARANCE MUST BE CONSIDERED FROM TOWER BODY AND ARMS.



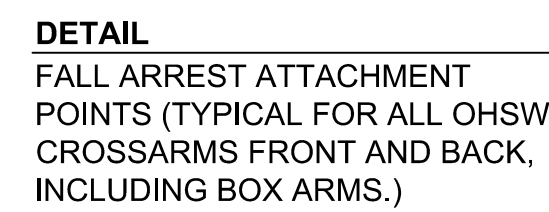
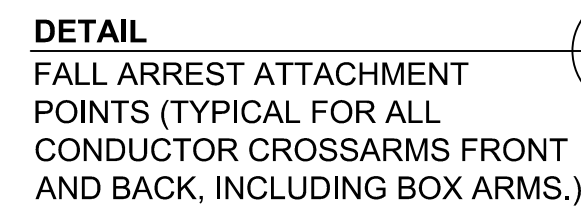
**B**

GENERAL NOTES:

1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
2. V, T, AND L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE, AND LONGITUDINAL AXIS RESPECTIVELY.
3. TEMPERATURE, RADIAL DESIGN ICE THICKNESS, AND WIND SPEED ARE INDICATED IN THE LOAD TABLE. THESE VALUES WERE USED TO CALCULATE THE VERTICAL, TRANSVERSE, AND LONGITUDINAL LOADS APPLIED TO THE STRUCTURE.
4. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.6 SHALL BE APPLIED TO THE WIND LOAD. WIND SHALL BE BLOWN ON TWO FACES OF THE LATTICE TOWER.
5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
6. THETA ( $\theta$ ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION.
7. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - C. ANY ONE PHASE AND GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
8. EACH MEMBER, WHICH IS INCLINED AT AN ANGLE OF LESS THAN 45 DEGREES WITH THE HORIZONTAL SHALL BE OF SUFFICIENT SECTION TO WITHSTAND, INDEPENDENT OF ALL OTHER LOADS, A CONCENTRATED LOAD OF 350 POUNDS APPLIED NORMAL TO THE MEMBER ON ITS WEAKEST AXIS AT ANY POINT ALONG ITS LENGTH. CONCENTRATED LOAD SHALL BE MULTIPLIED BY AN OVERLOAD FACTOR OF 2.0.
9. LATTICE MEMBER ORIENTATION SHALL MINIMIZE SNOW ACCUMULATION ON THE STRUCTURE.
10. ELECTRICAL CLEARANCES MUST BE CHECKED TO THE SURFACE OF THE NEAREST MEMBER.
11. THE MAXIMUM SHIELDING ANGLE AT THE STRUCTURE SHALL BE 25 DEGREES.
12. ALL CLEARANCE CHECKS TO CONDUCTOR MUST BE CHECKED TO CLEARANCE ENVELOPE PROVIDED IN DETAIL 1.
13. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
14. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR HELICOPTER AND CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
15. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
16. CROSSARMS, AND GROUND WIRE PEAKS SHALL BE DESIGNED WITH FALL ARREST ATTACHMENT POINTS. FALL ARREST ATTACHMENT POINTS SHALL SUPPORT A LOAD OF 3,000 POUNDS AND BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE. AT EACH FALL ARREST ATTACHMENT POINT, A GUSSET PLATE OR VANG WITH A 1-INCH DIAMETER HOLE SHALL BE PROVIDED.
17. CROSSARMS AND HORIZONTAL MEMBERS ADJACENT TO PHASES SHALL BE DESIGNED TO SUPPORT A LADDER LOAD OF 1,200 POUNDS. LADDER LOAD SHALL BE APPLIED AS TWO POINT LOADS OF 600 POUNDS SPACED AT 15 INCHES. LOAD SHALL BE APPLIED IN CONJUNCTION WITH THE MAINTENANCE LOAD CASE.
18. CLIMBING AND WORKING CLEARANCES MUST BE PROVIDED AS INDICATED IN THE ELEVATION VIEW.
19. STRUCTURE SHALL BE DESIGNED TO WITHSTAND UNEVEN LEG EXTENSION DIFFERENTIAL ASSUMING VERTICAL TO HORIZONTAL GROUND SLOPE RATIO OF (1:2).
20. STRUCTURES SHALL ALSO BE DESIGNED WITH UPLIFT LOADING. UPLIFT SHALL BE CONSIDERED UNDER LOAD CASE 1, LOAD CASE 2, & LOAD CASE 11. FOR LOAD CASE 1 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -1 KIPS. FOR LOAD CASE 2 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.1 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -1.6 KIPS. FOR LOAD CASE 13 REPLACE  $V_{SA}$  &  $V_{SB}$  WITH -0.2 KIPS AND  $V_{PA}$  &  $V_{PB}$  WITH -2.3 KIPS.

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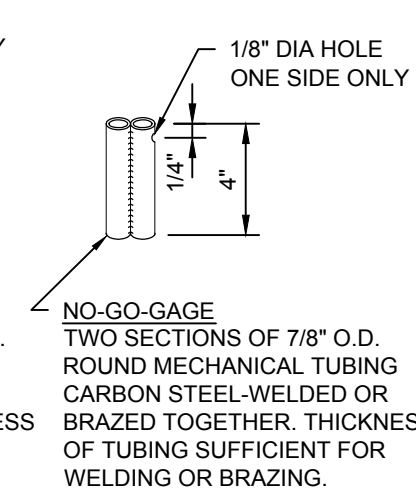
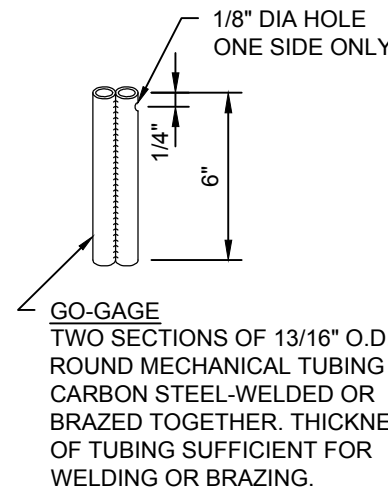
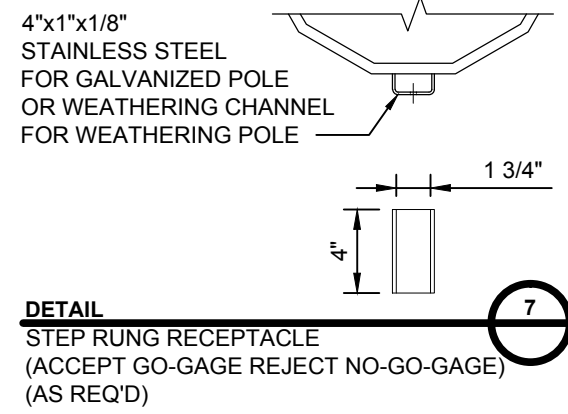
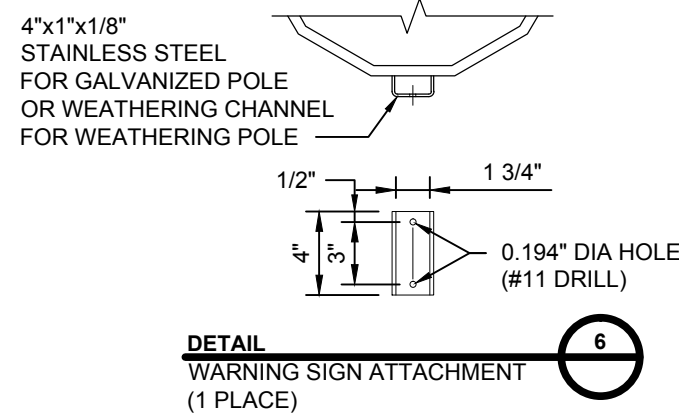
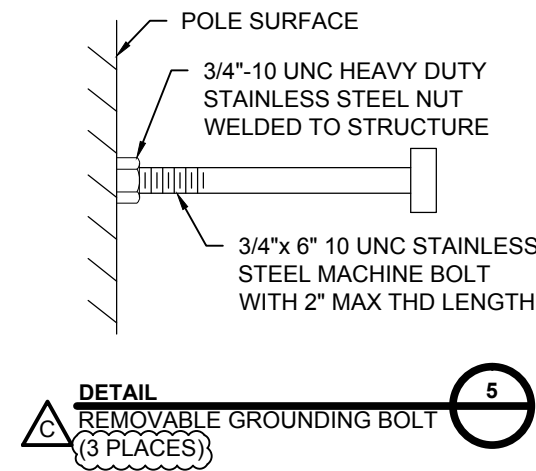
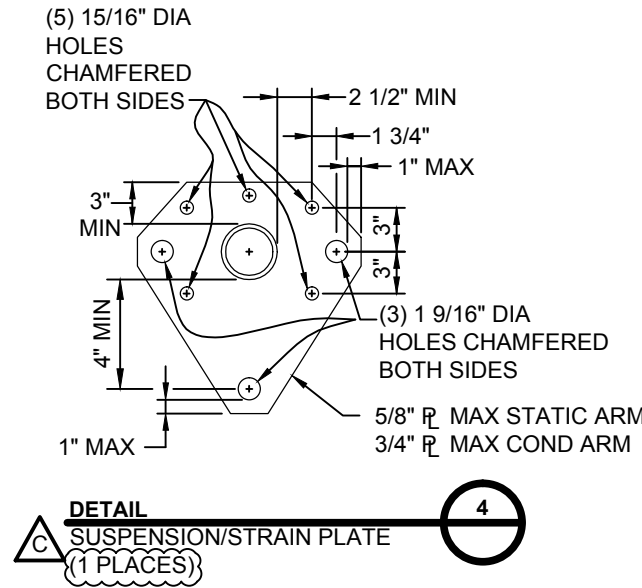
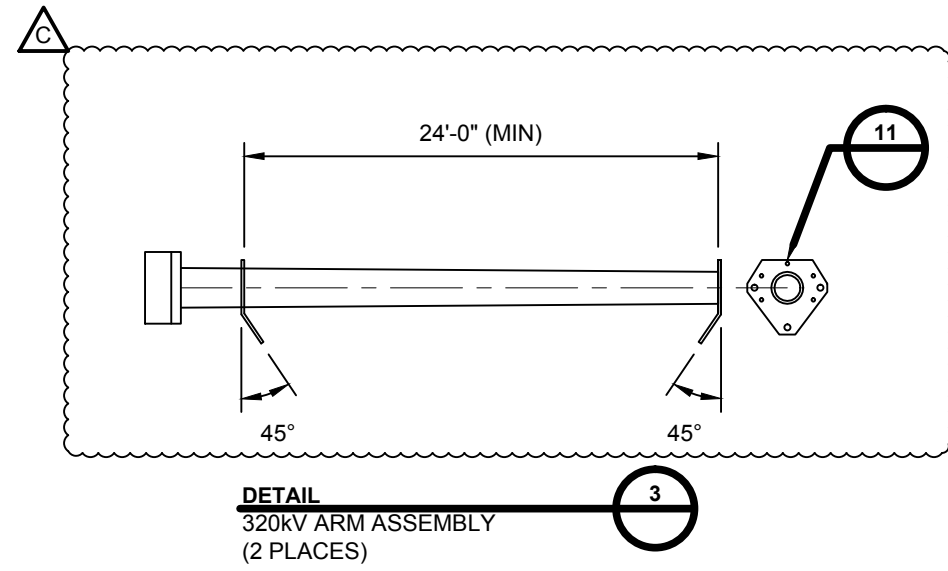
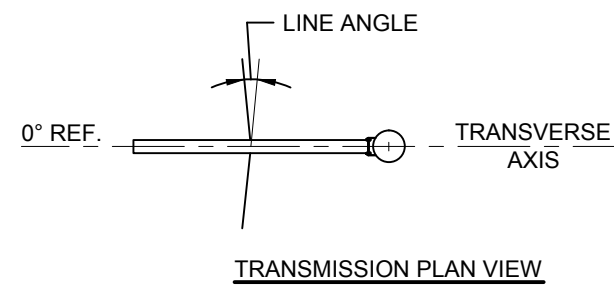
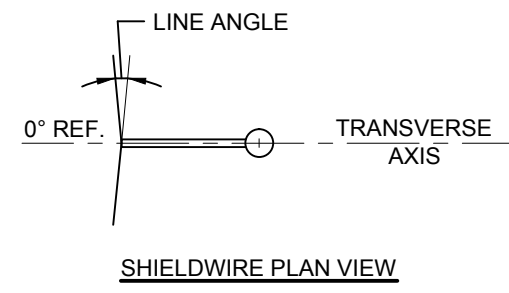
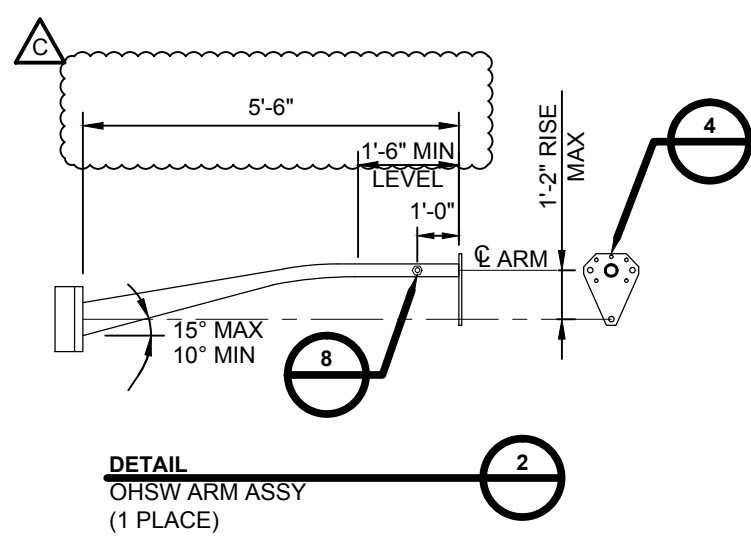
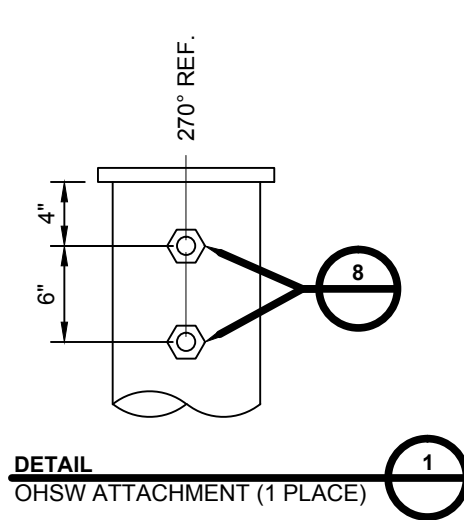
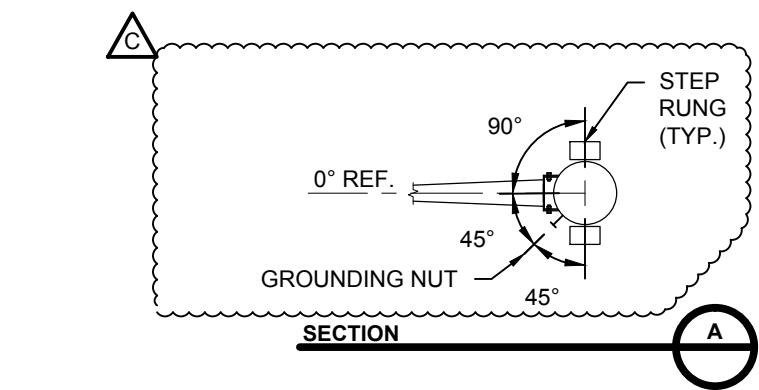




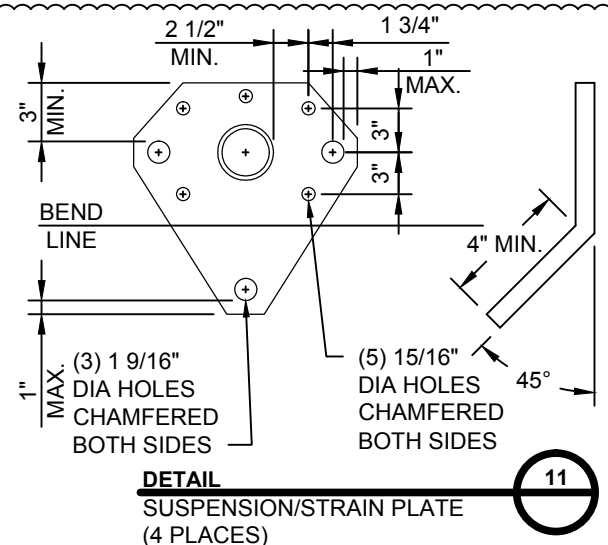
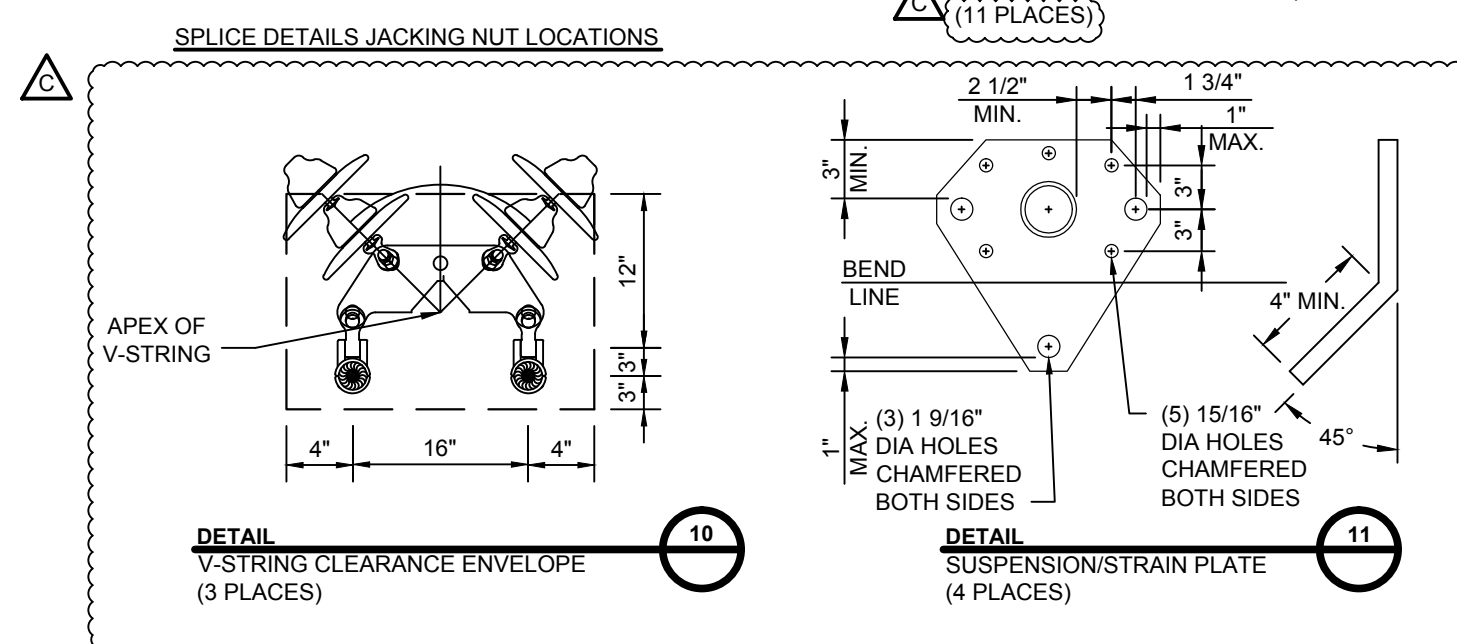
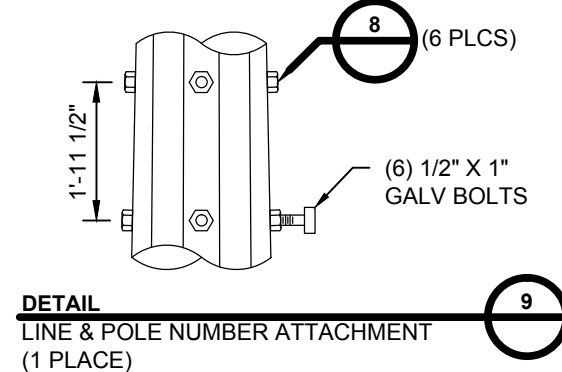
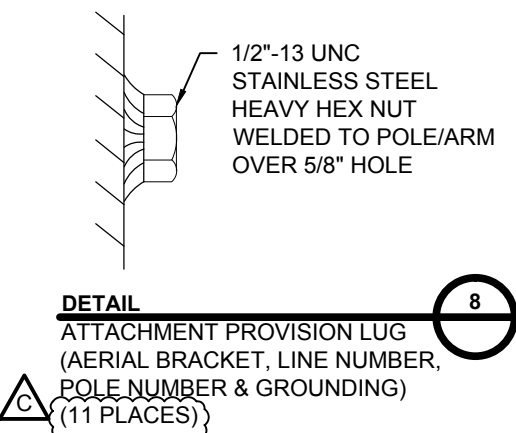
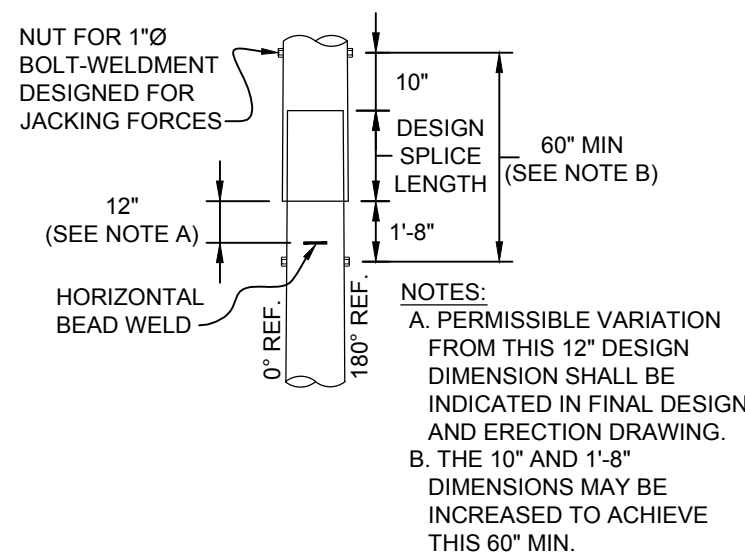
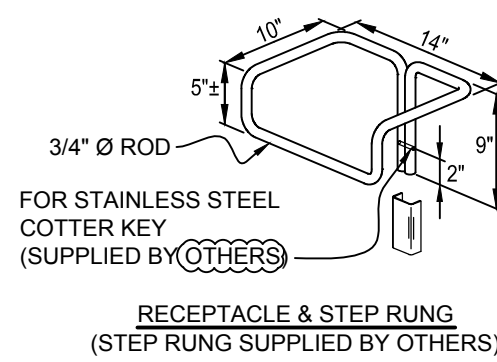
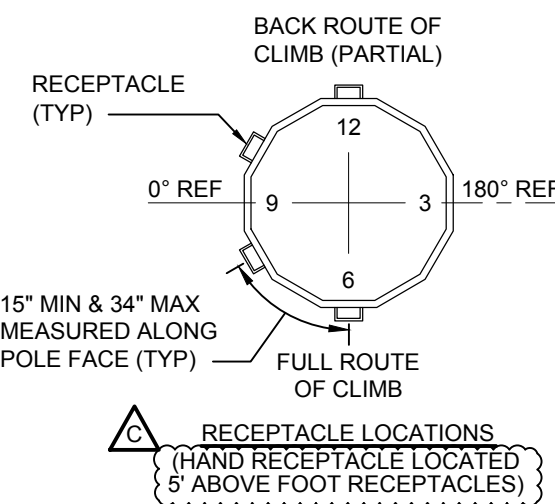
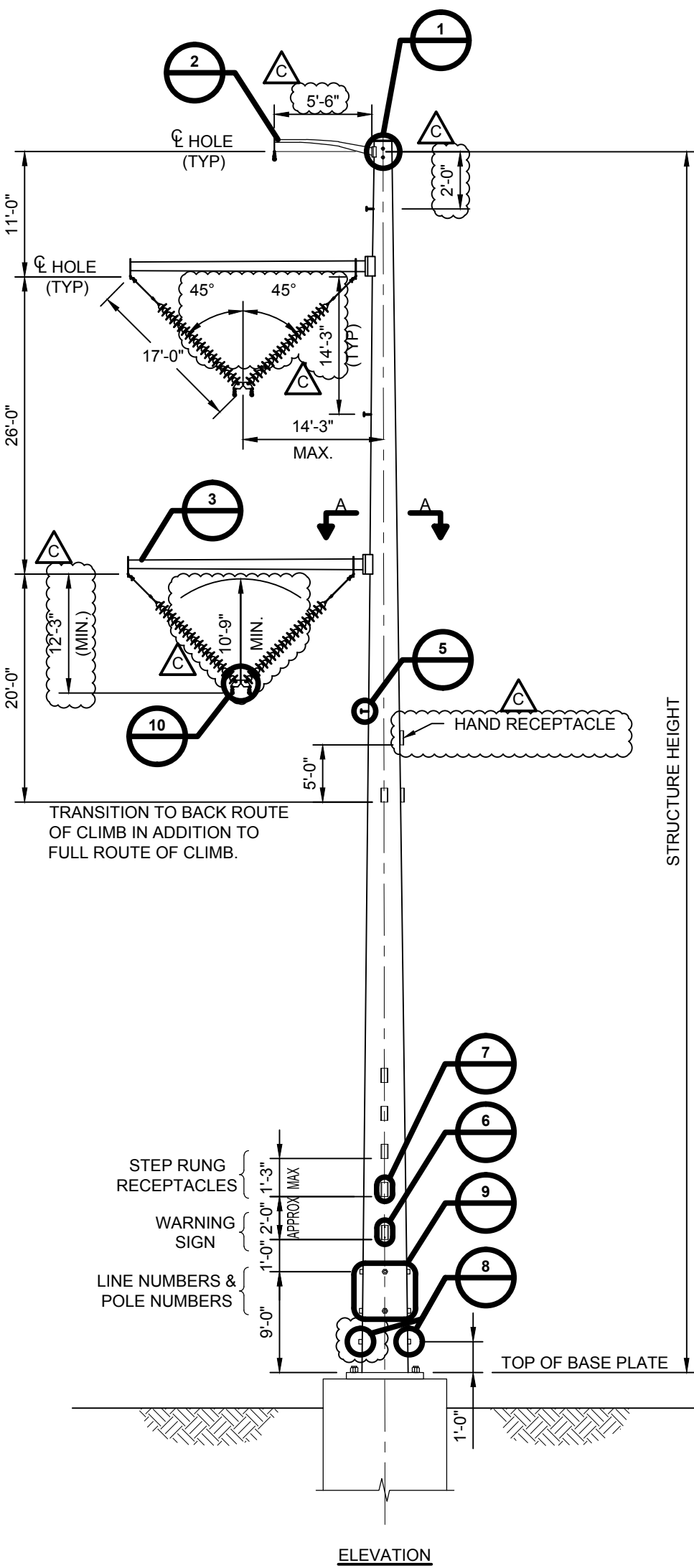
- NOTES:**
1. HOLE DIAMETERS AND VANG DIMENSIONS TO BE DETERMINED DURING DETAIL DESIGN THROUGH COORDINATION WITH TOWER VENDOR AND HARDWARE MANUFACTURER.
  2. STEP BOLTS SHALL BE INSTALLED ON ALTERNATE FLANGES OF ONE LEG. SPACING SHALL NOT EXCEED 16 INCHES. STEP BOLTS SHALL BE PROVIDED FROM TOWER BASE TO TOP OF TOWER.
  3. BOX ARMS SHALL HAVE PLATE ATTACHMENT HOLE AT EACH CORNER AND AT MIDPOINT.
  4. FALL ARREST LOADS SHALL BE APPLIED SINGULARLY AT EACH LOCATION.

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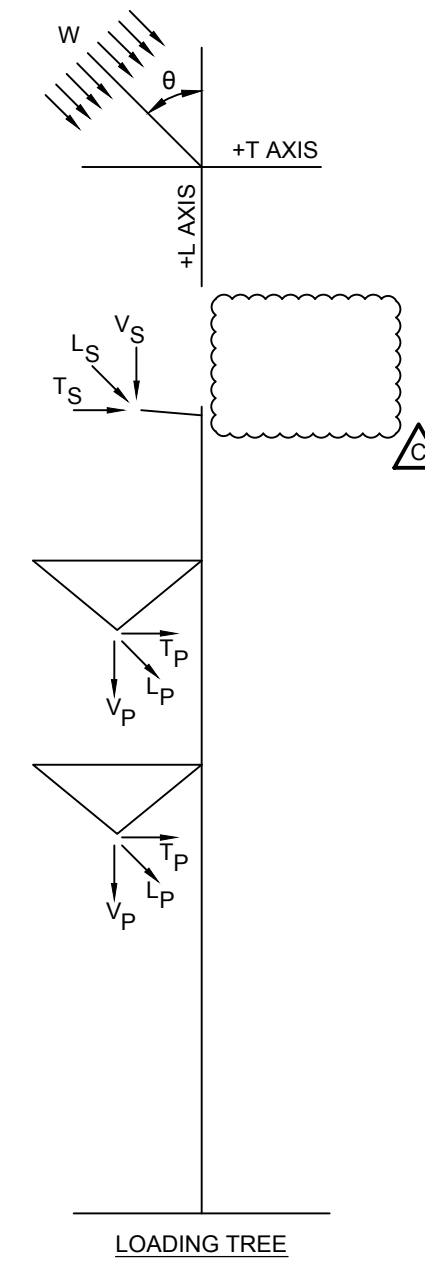
STEP RUNG RECEPTACLE GAGES



STRUCTURE NAME: 32-SCVSP-LTW-002  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 550  
WEIGHT SPAN (FT): 850  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.45	1.03	0.00	13.54	5.30	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.43	0.75	0.00	5.61	5.98	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.03	0.74	0.00	12.70	3.28	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.62	1.06	0.00	17.43	4.15	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.96	0.48	0.00	9.02	2.65	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.96	0.47	0.00	9.02	2.49	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.96	0.37	5.50	9.02	1.51	24.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.58	0.27	0.27	23.61	2.17	2.27	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.43	0.10	0.00	5.61	0.83	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.66	0.21	0.00	13.01	1.66	0.00	0.00	90.00	2.00

- REFERENCES:
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

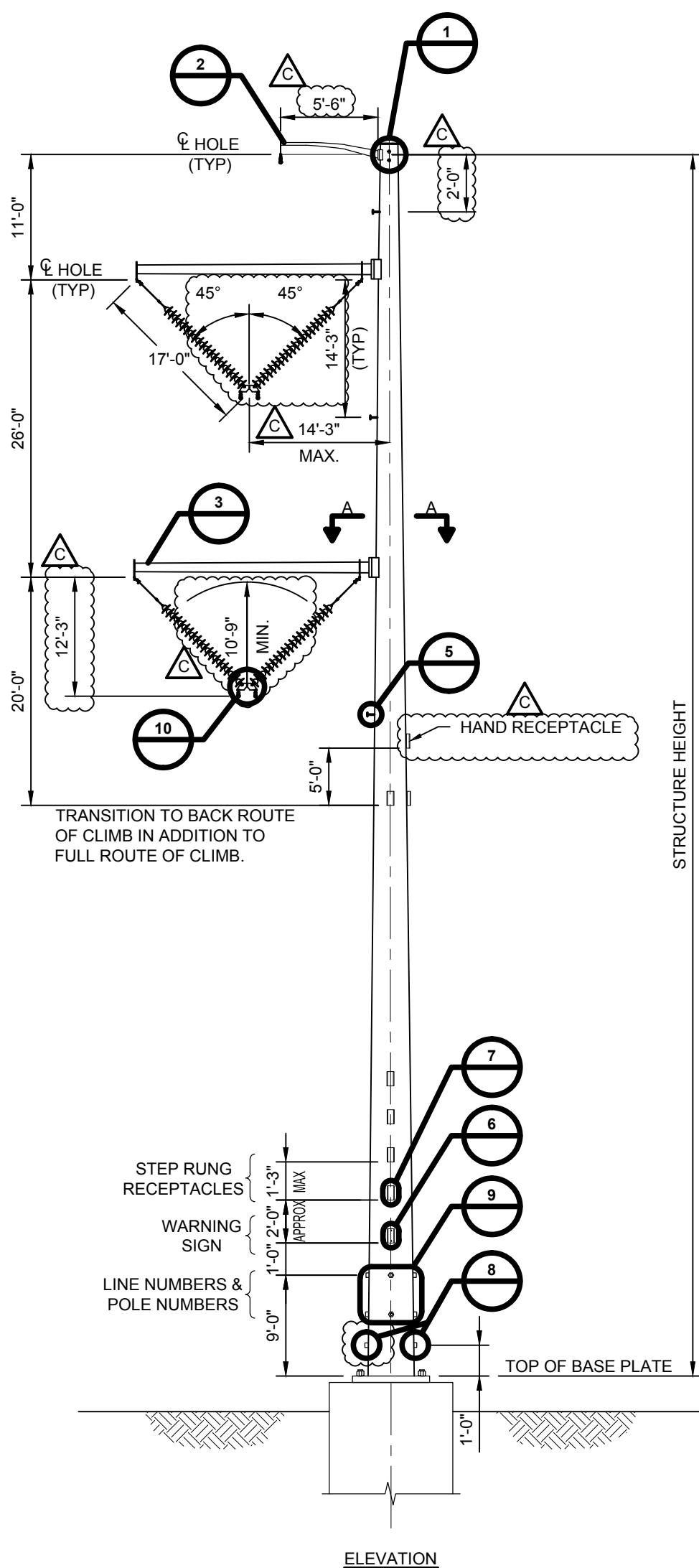


- NOTES:
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 65°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - PROVIDE STEP RUNG RECEPTABLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTABLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - TEMPORARY LIFT OR TENSION POINTS: CLOSE TO THE NORMAL POINTS OF THE CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNS TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

PRELIMINARY - NOT  
FOR CONSTRUCTION

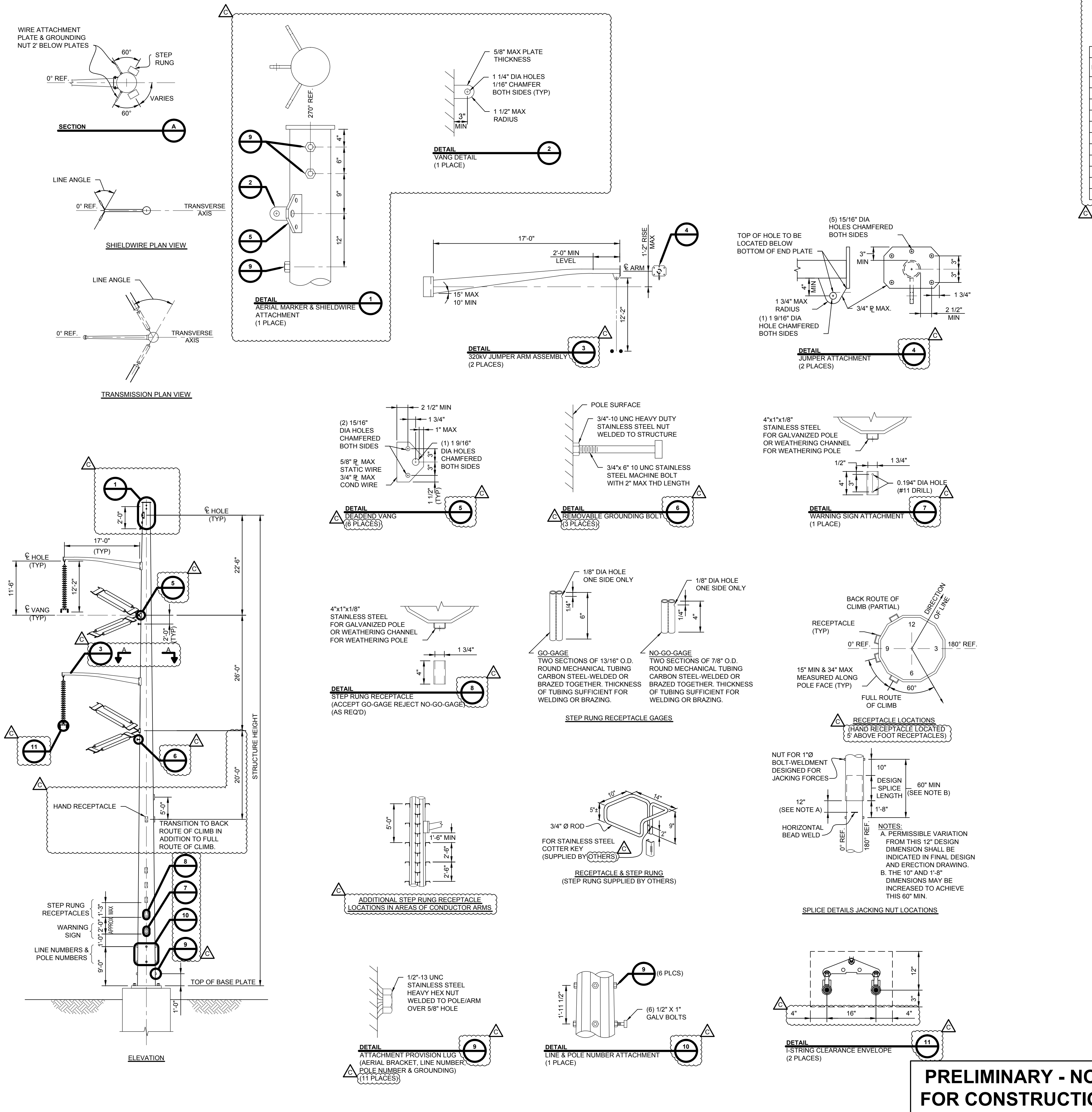
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**PRELIMINARY - NOT  
FOR CONSTRUCTION**





STRUCTURE NAME: 32-SCVSP-LDW-045

320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)

OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)

WIND SPAN AHEAD (FT): 550 WIND SPAN BACK (FT): 550

WEIGHT SPAN AHEAD (FT): 825 WEIGHT SPAN BACK (FT): 825

LINE ANGLE: 0 - 45 DEGREES

LOADING CASE					DESIGN LOADS															
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSb (k)	TSb (k)	LSb (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K	
1	NESC 250B	0.00	0.50	39.53	1.41	4.37	9.62	1.41	4.37	-9.62	13.36	30.89	73.59	13.36	30.89	-73.59	10.00	90.00	1.50	
2	NESC 250C	60.00	0.00	100.00	0.42	2.32	4.51	0.42	2.32	-4.51	5.52	19.43	38.67	5.52	19.43	-38.67	29.00	90.00	1.00	
3	NESC 250D	15.00	1.00	39.53	1.97	3.53	8.01	1.97	3.53	-8.01	12.47	21.41	52.13	12.47	21.41	-52.13	4.00	90.00	1.00	
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	5.25	12.04	3.51	5.25	-12.04	16.96	27.33	66.65	16.96	27.33	-66.65	4.00	90.00	1.00	
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	2.51	5.83	0.94	2.51	-5.83	8.91	18.16	44.60	8.91	18.16	-44.60	4.00	90.00	1.00	
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	2.38	-5.50	8.91	16.40	40.00	8.91	16.40	-40.00	4.00	90.00	1.00	
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	0.28	0.00	8.91	16.40	40.00	8.91	1.09	0.00	4.00	90.00	1.00	
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.52	0.27	1.98	2.08	-5.23	30.33	12.71	2.27	9.63	17.56	-44.25	3.45	90.00	1.50	
9	DEFLECTION	60.00	0.00	0.00	0.42	1.13	2.96	0.42	1.13	-2.96	5.52	9.08	23.72	5.52	9.08	-23.72	0.00	90.00	1.00	
10	MAINTENANCE	60.00	0.00	0.00	2.64	2.26	5.92	2.64	2.26	-5.92	12.84	18.16	47.44	12.84	18.16	-47.44	0.00	90.00	2.00	
11	UPLIFT	-20.00	0.00	0.00	0.42	1.70	4.43	0.42	1.70	-4.43	5.52	16.59	43.34	5.52	16.59	-43.34	0.00	90.00	1.00	

**REFERENCES:**

- GROUNDING NUT: SKETCH B
- STEP RUNG + RECEPTACLE: SKETCH E
- GAGES FOR RECEPTACLE: SKETCH L
- CLIMBING FACILITIES: SKETCH B
- RECEPTACLE LOCATIONS: SKETCH C
- ADDITIONAL RECEPTACLE LOCATION: SKETCH D
- ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
- LIFTING VANG PROVISIONS: SKETCH J + K
- FALL PROTECTION VANGS: SKETCH N + Q
- JACKING NUT LOCATIONS: SKETCH I

**LOADING TREE**

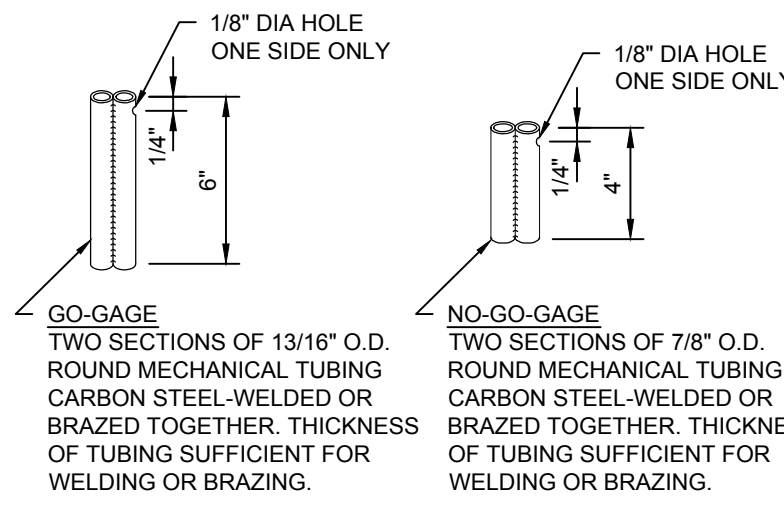
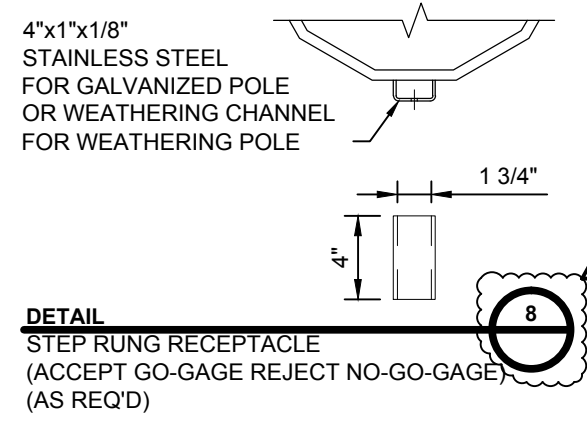
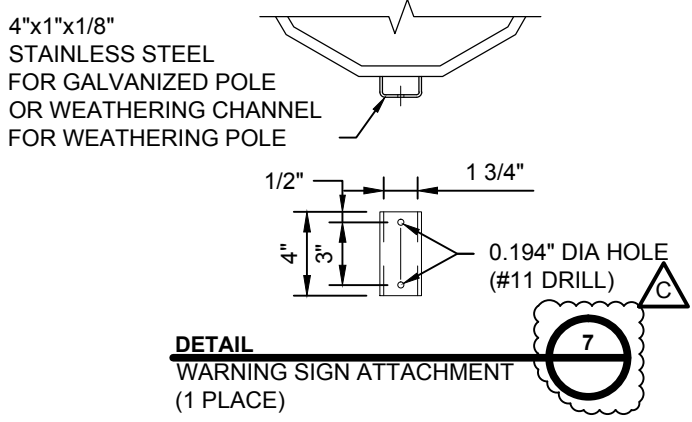
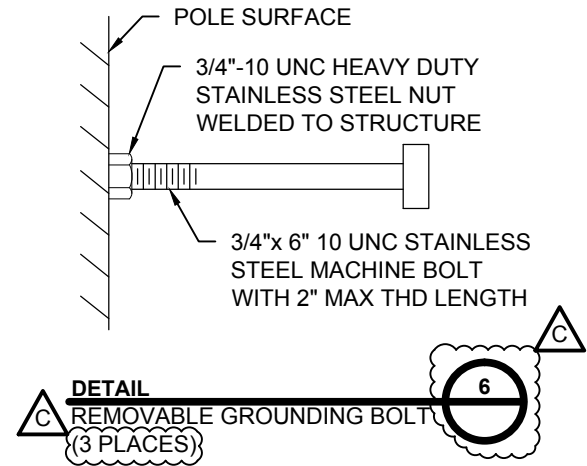
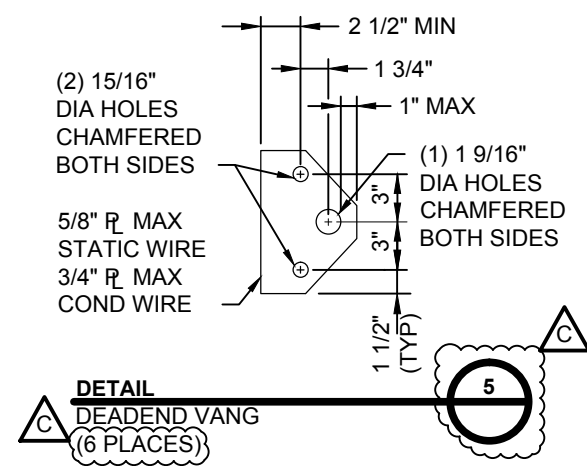
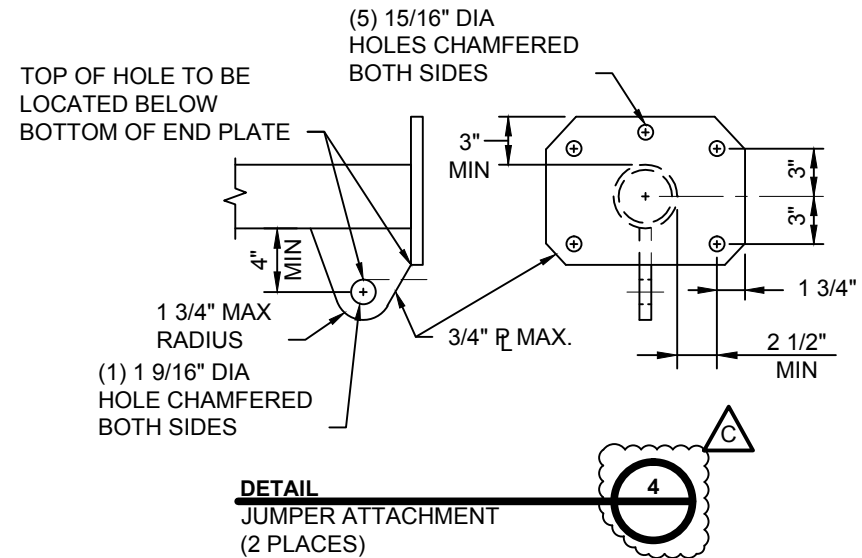
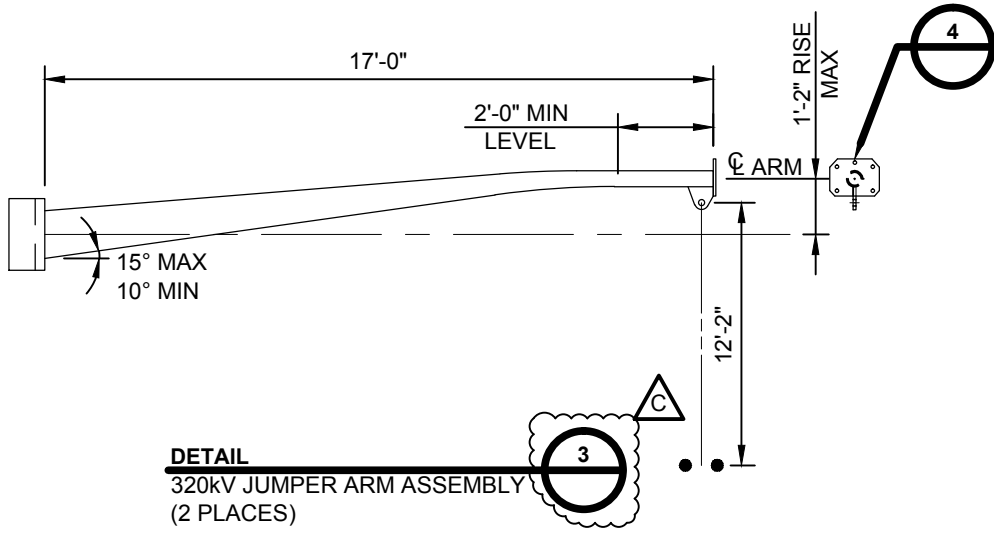
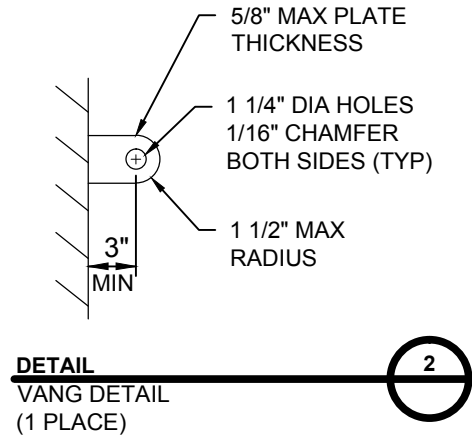
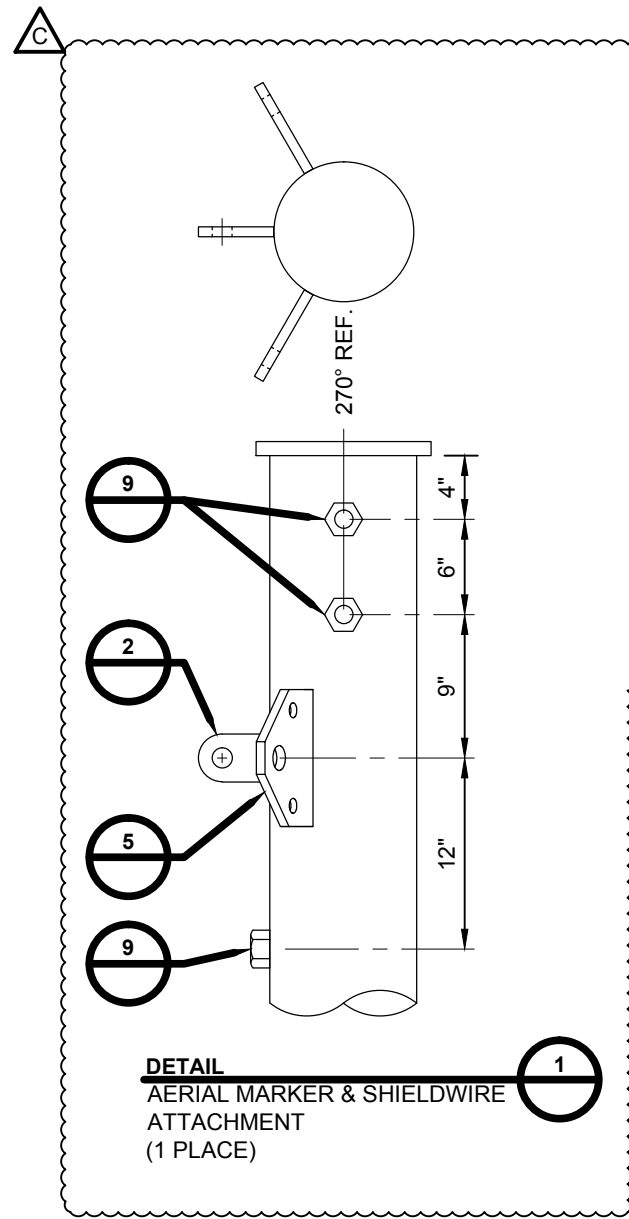
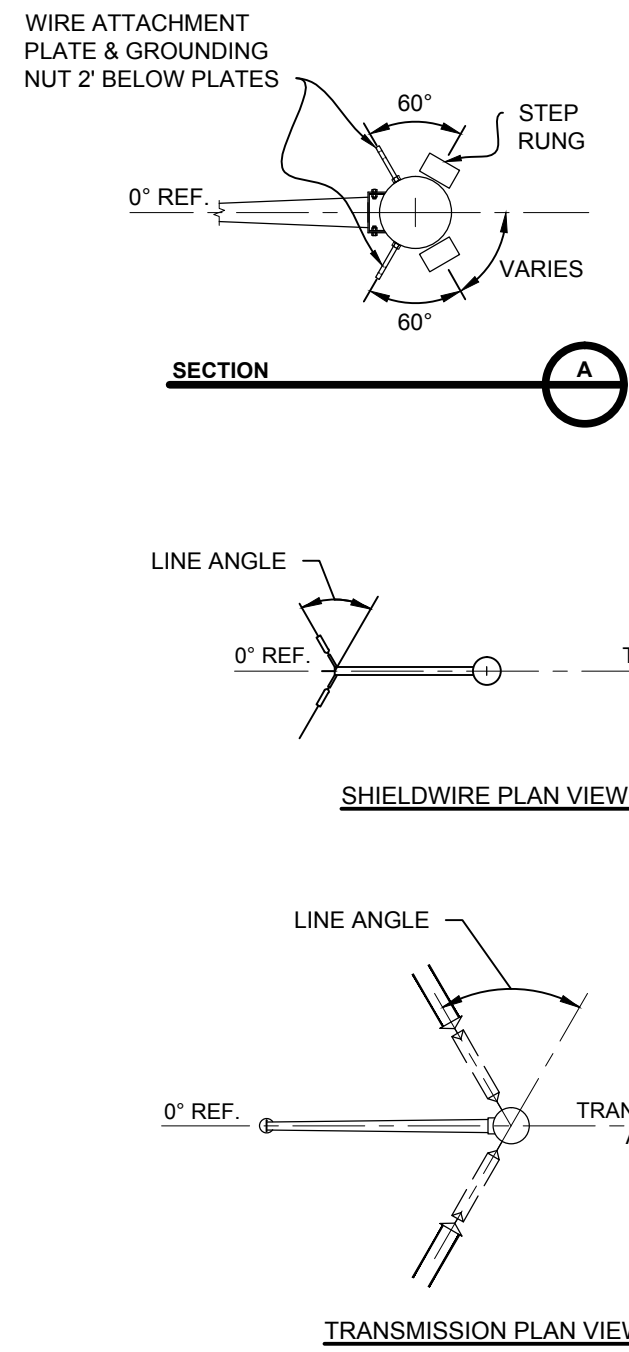
**NOTES:**

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
- THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
- SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25°.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 12.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
- TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
- PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
- CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
- VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
- MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
- ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
- JUMPER ARM SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,800 POUNDS.
- 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
- 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
- FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

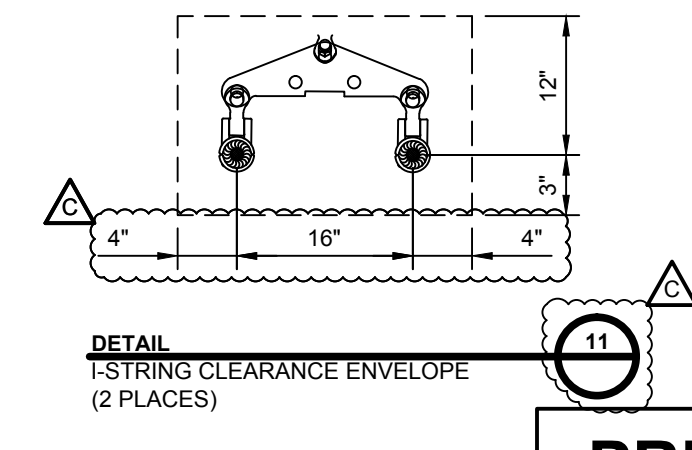
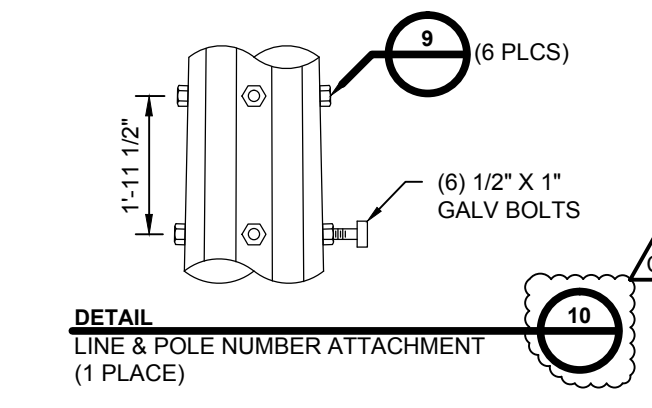
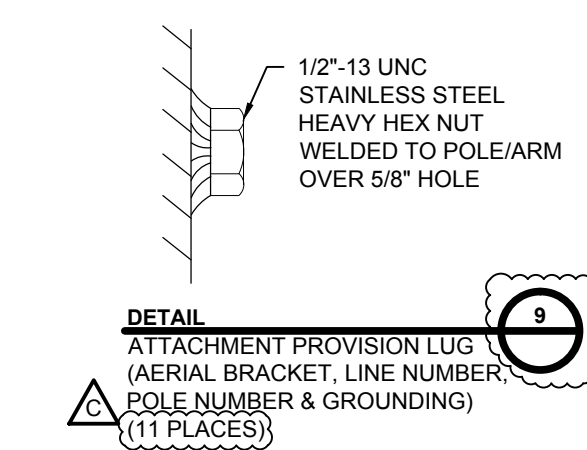
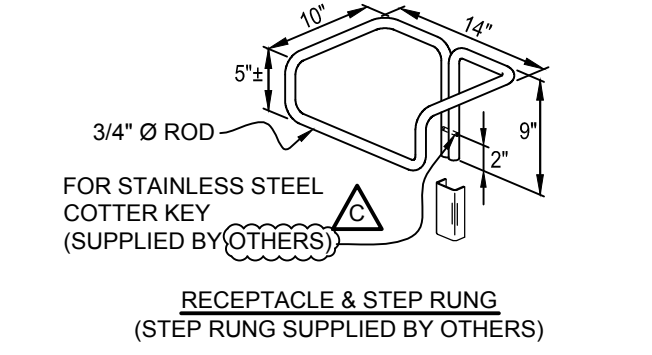
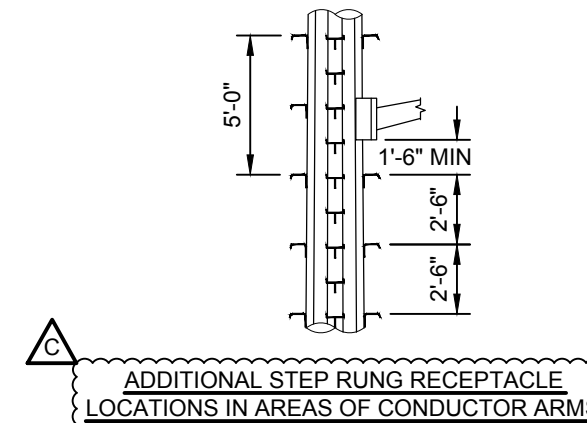
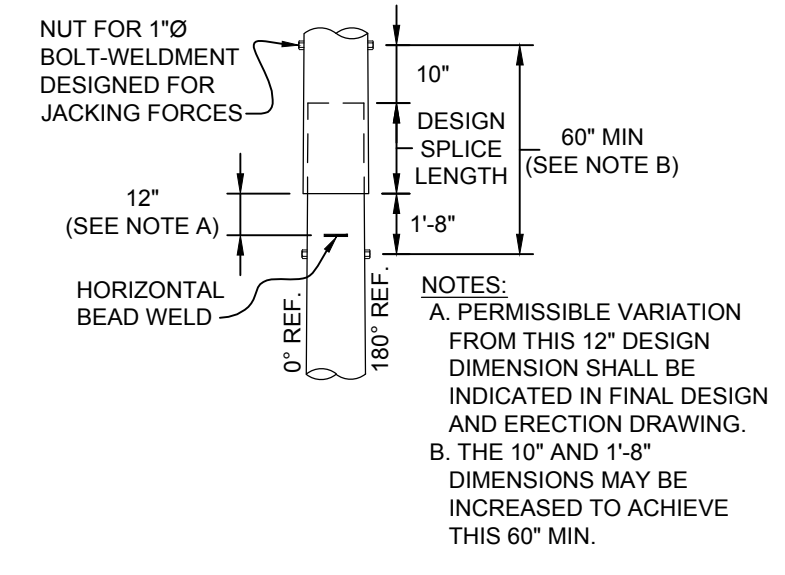
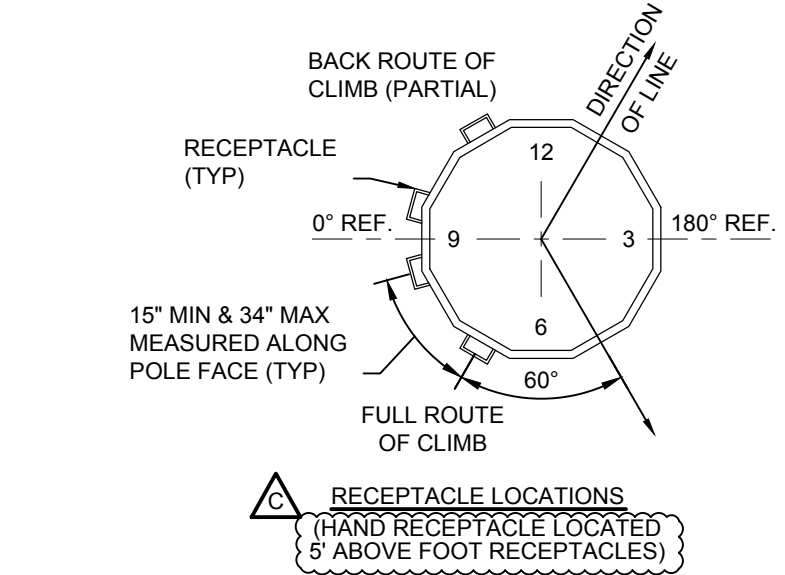
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STEP RUNG RECEPTACLE GAGES

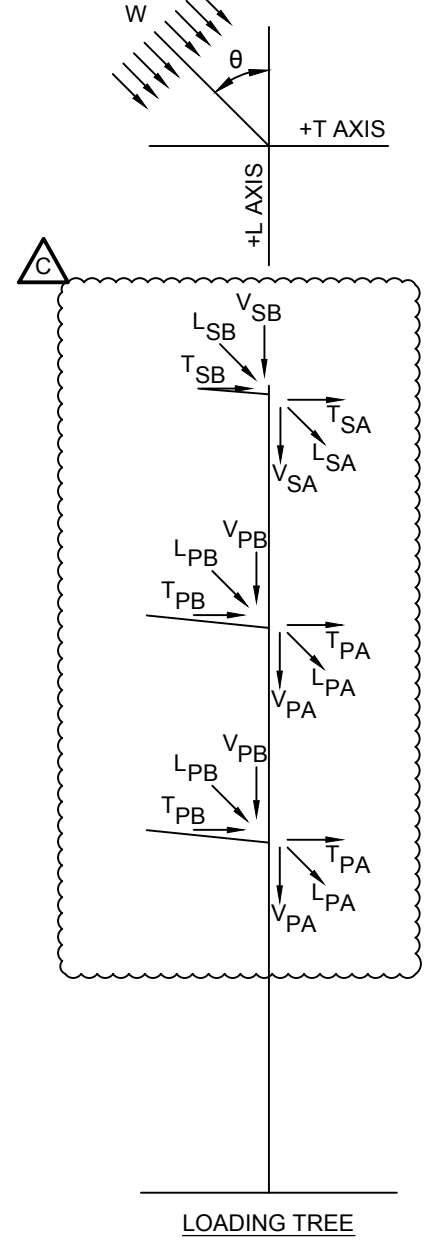


**PRELIMINARY - NOT FOR CONSTRUCTION**

STRUCTURE NAME: 32-SCVSP-HDW-090  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 550 WIND SPAN BACK (FT): 550  
WEIGHT SPAN AHEAD (FT): 825 WEIGHT SPAN BACK (FT): 825  
LINE ANGLE: 45 - 90 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSb (k)	TSb (k)	LSb (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.41	7.50	8.89	1.41	7.50	-8.89	13.36	54.76	67.99	13.36	54.76	-67.99	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.42	3.79	4.17	0.42	3.79	-4.17	5.52	31.98	35.73	5.52	31.98	-35.73	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.97	6.12	7.40	1.97	6.12	-7.40	12.47	38.32	48.17	12.47	38.32	-48.17	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	9.16	11.13	3.51	9.16	-11.13	16.96	48.95	61.57	16.96	48.95	-61.57	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	4.40	5.39	0.94	4.40	-5.39	8.91	32.63	41.21	8.91	32.63	-41.21	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	4.17	-5.08	8.91	29.38	36.96	8.91	29.38	-36.96	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	4.17	-5.08	8.91	29.38	36.96	8.91	1.09	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.38	0.25	1.98	3.78	-4.83	30.33	11.55	2.10	9.63	31.91	-40.88	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.42	2.09	2.73	0.42	2.09	-2.73	5.52	16.77	21.92	5.52	16.77	-21.92	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.64	4.18	5.47	2.64	4.18	-5.47	12.84	33.55	43.83	12.84	33.55	-43.83	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.42	3.13	4.09	0.42	3.13	-4.09	5.52	30.65	40.04	5.52	30.65	-40.04	0.00	90.00	1.00

- REFERENCES:**
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I



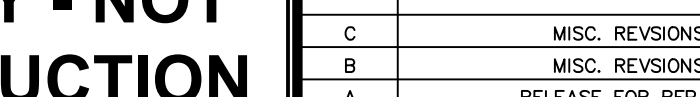
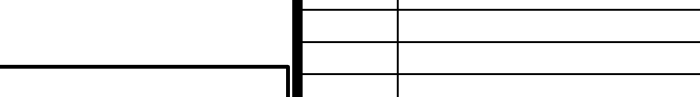
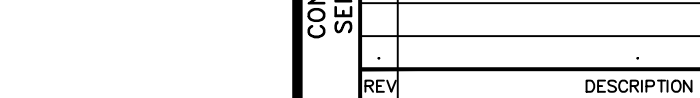
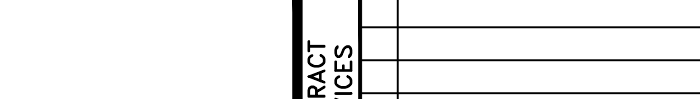
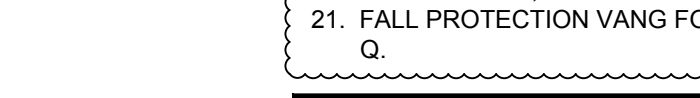
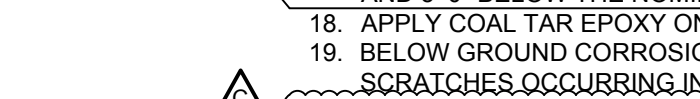
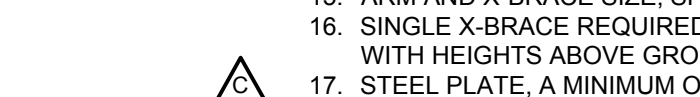
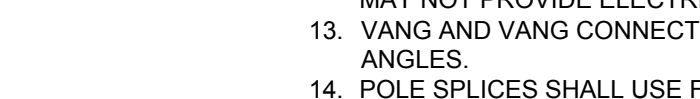
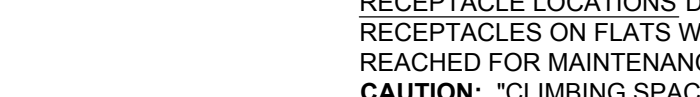
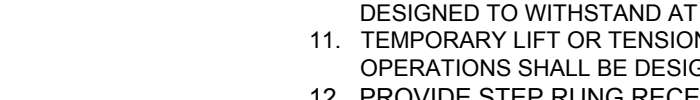
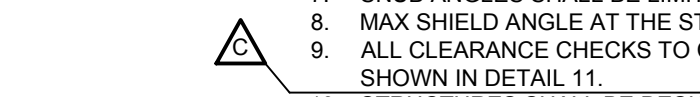
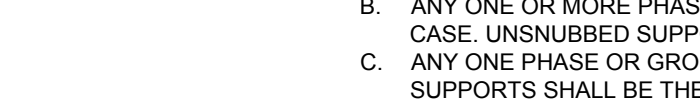
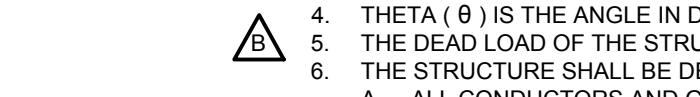
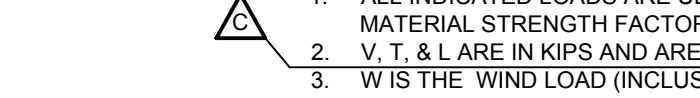
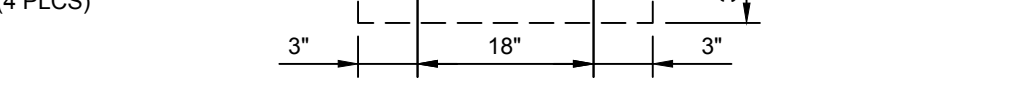
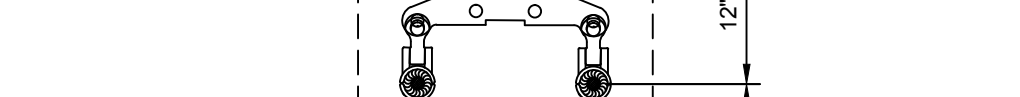
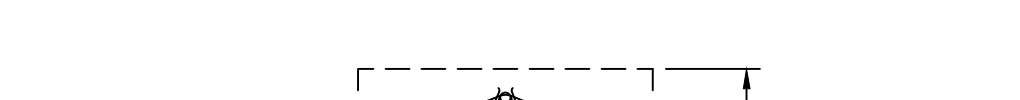
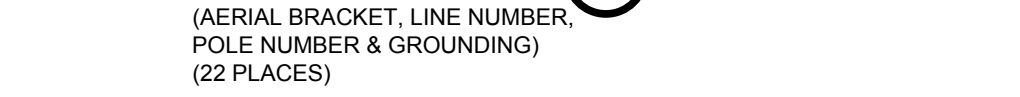
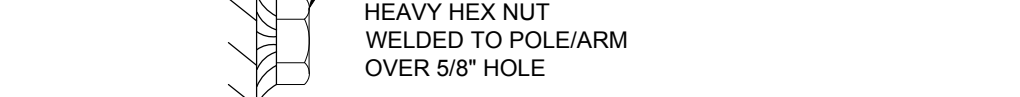
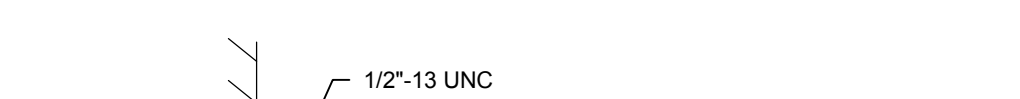
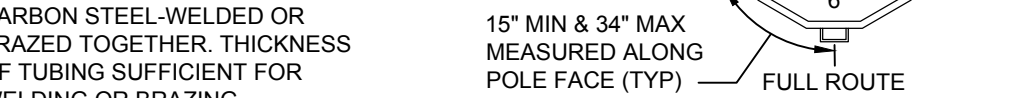
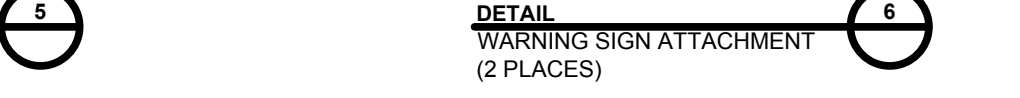
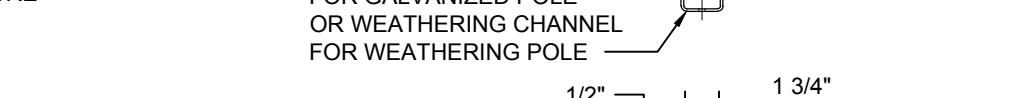
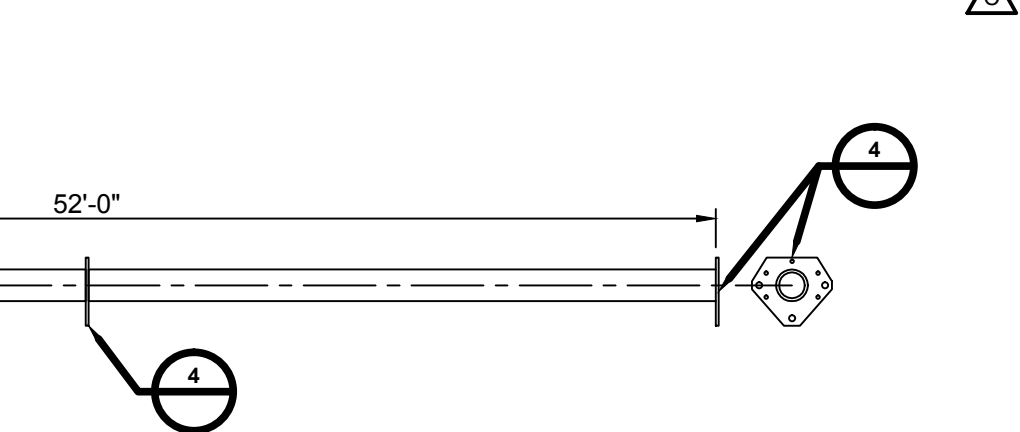
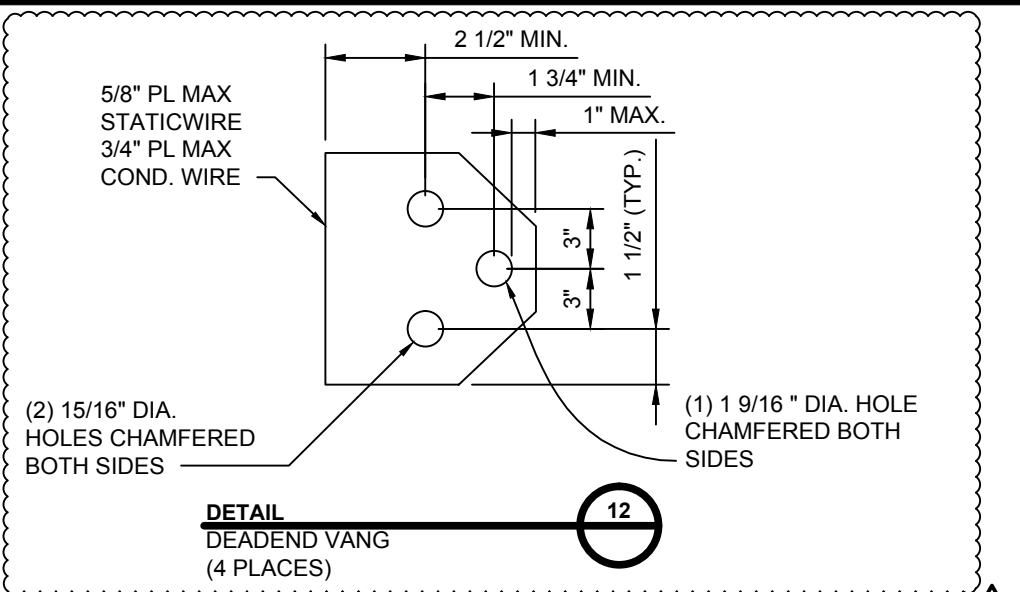
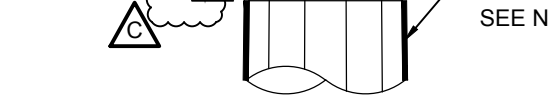
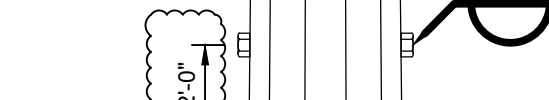
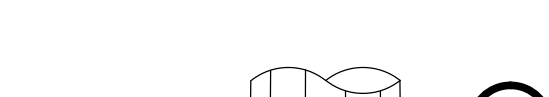
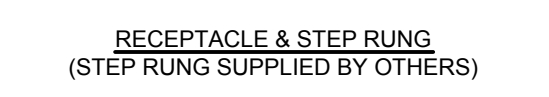
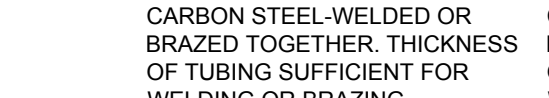
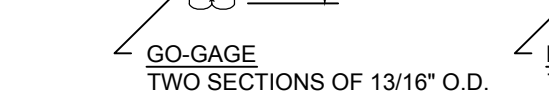
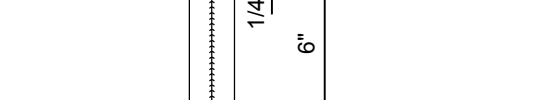
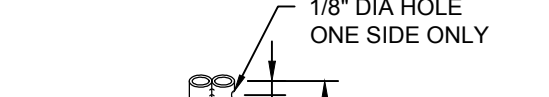
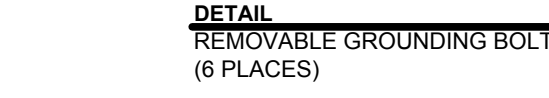
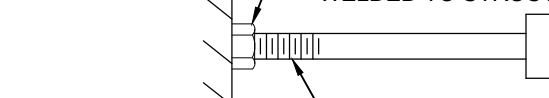
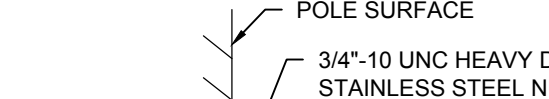
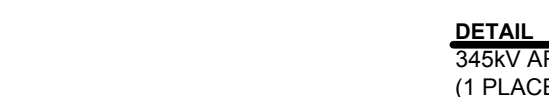
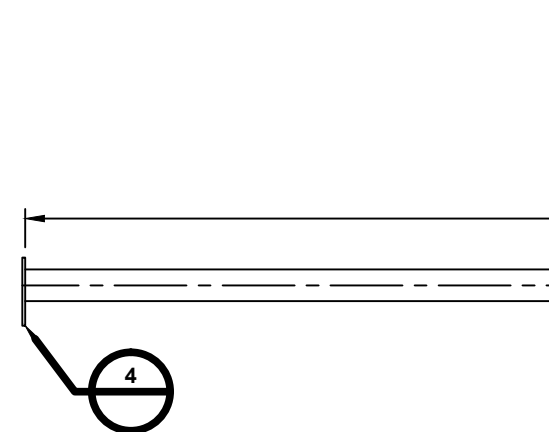
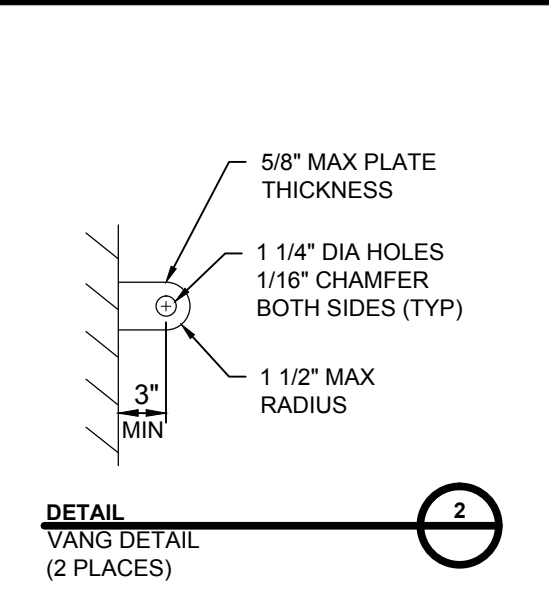
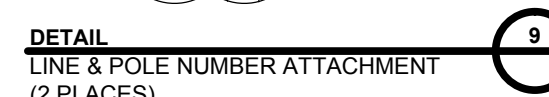
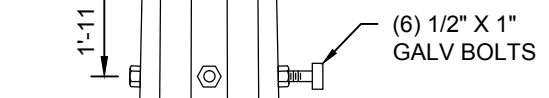
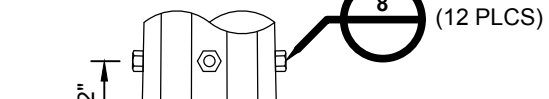
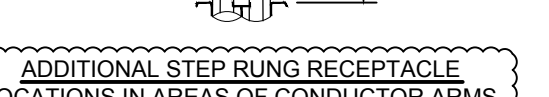
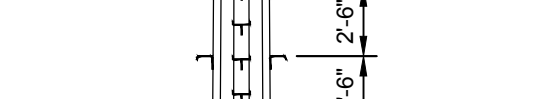
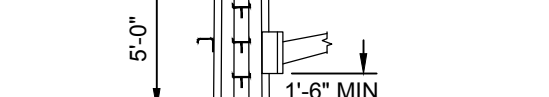
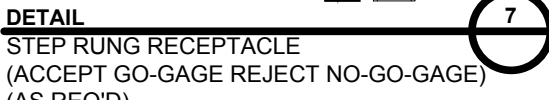
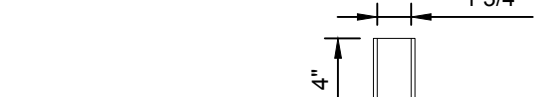
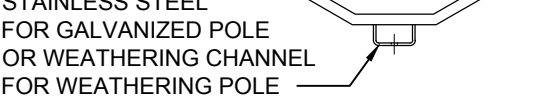
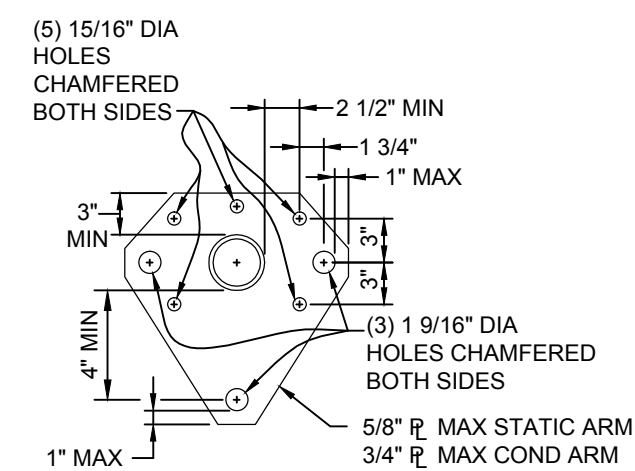
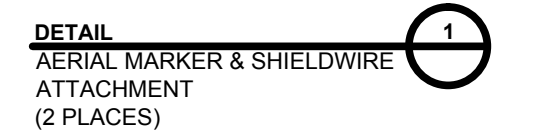
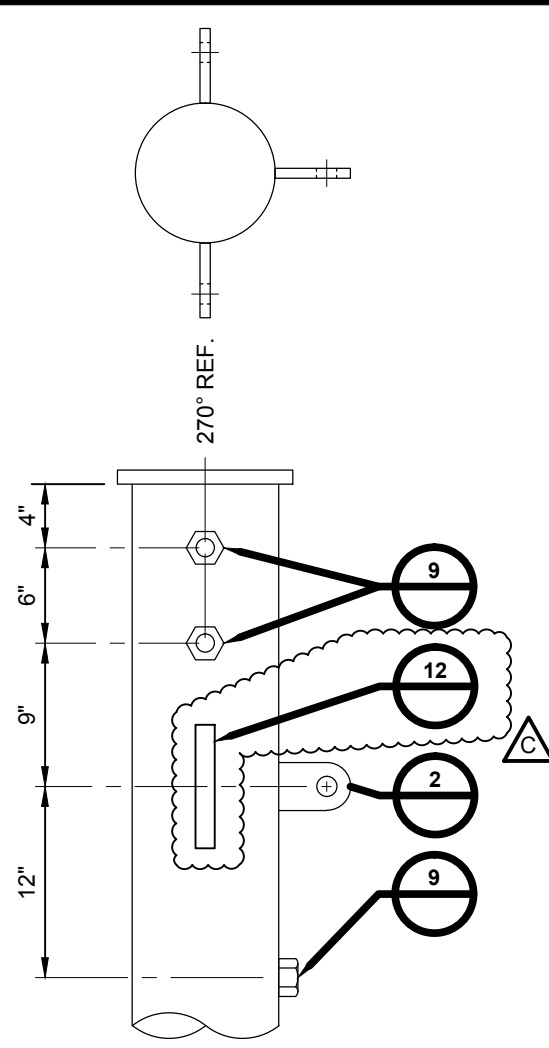
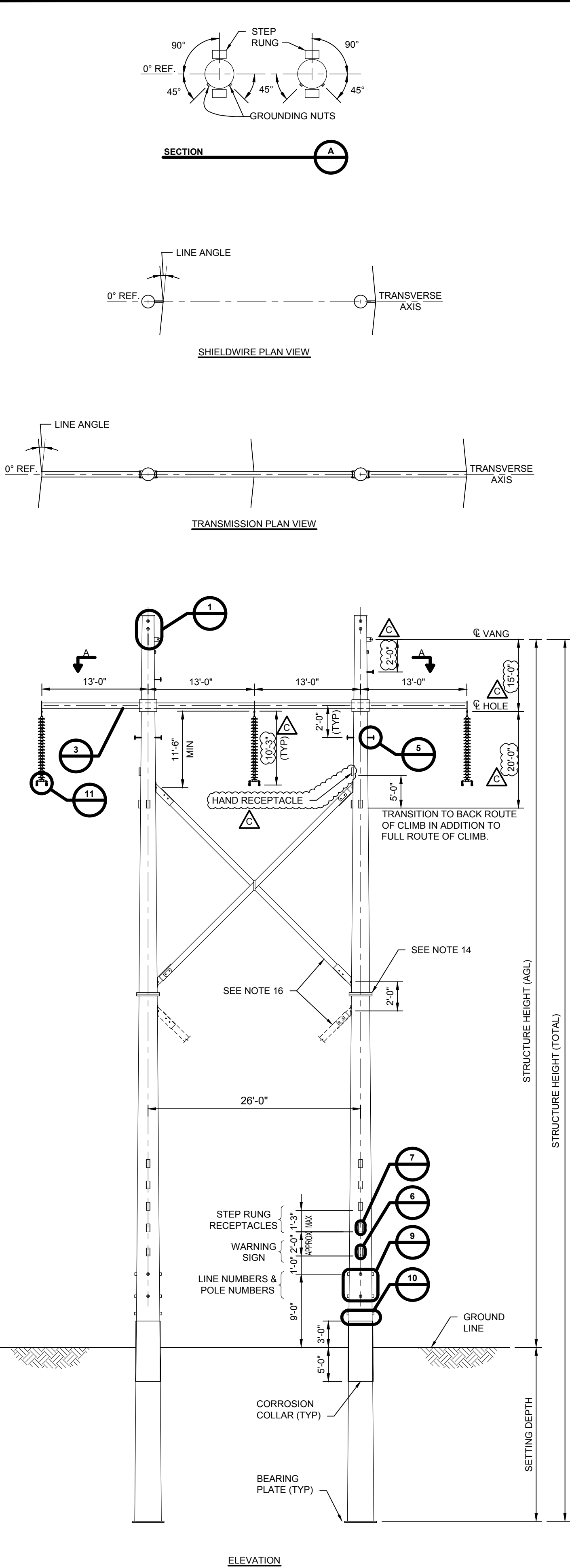
- NOTES:**
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
  - SNUB ANGLES SHALL BE LIMITED TO A 15° DEGREE DEFLECTION LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 12.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
 

**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - JUMPER ARM SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,500 POUNDS.
  - 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

CONTRACT SERVICES						THE NORTHERN PASS						C	
REV						DESCRIPTION						DRAWN BLH	
ENG/PE#						DATE						ENGINEER CET	
DRN						CHKD						CHECKED TAB	
APPR												APPROVED	
												DATE	
C						MISC. REVISIONS						5/21/15 KAK	
B						MISC. REVISIONS						5/8/15 BLH	
A						RELEASE FOR RFP BID						5/1/15 BLH	
DWG REV						EPN/DESCRIPTION						CONT/PE#	
DATE						DRN						CHKD	
APPR													
SCALE NTS						FILE: TSP-04.DWG						DRAWING NO. TSP-04-001	
IMAGE:													

320KV DC HEAVY DEADEND 45-90°  
32-SCVSP-HDW-090  
LOAD & DESIGN DRAWING

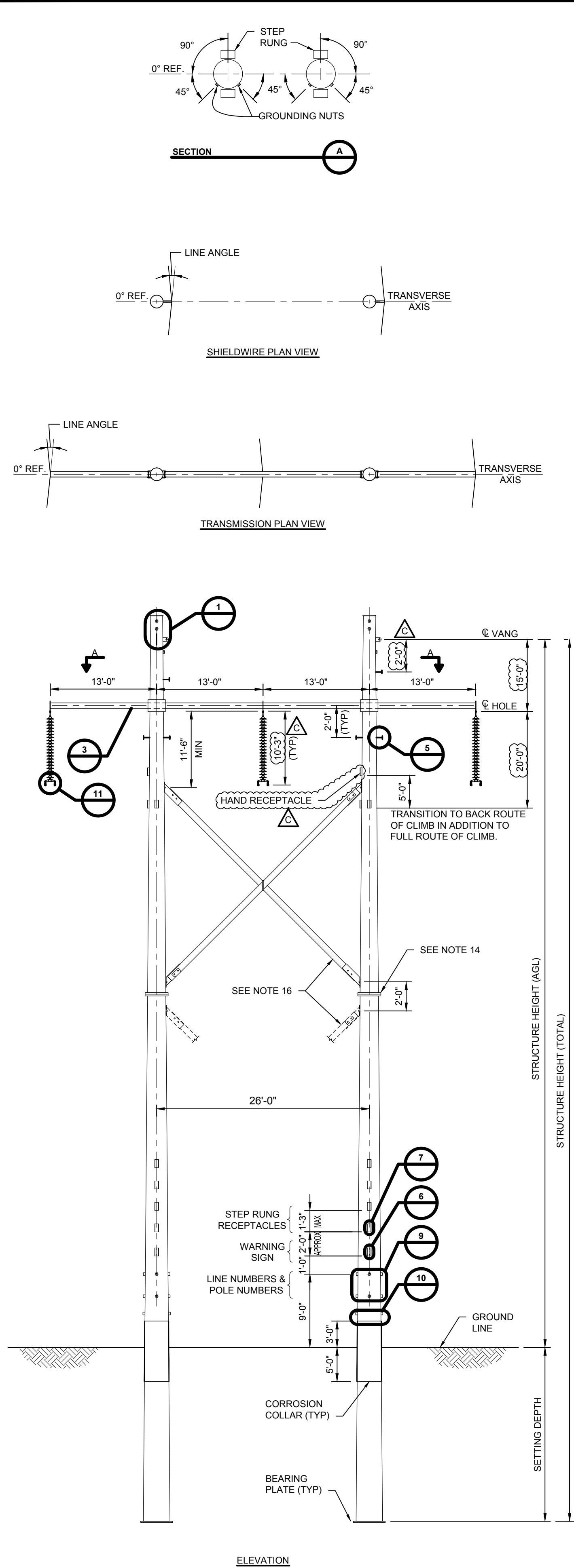




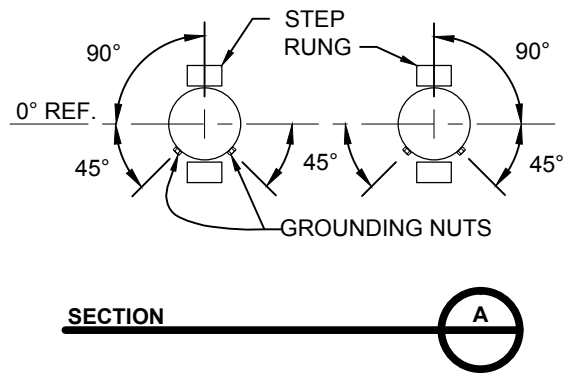
STRUCTURE NAME: 30-SCHSP-LTW-002  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESG HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESG HEAVY)  
WIND SPAN (FT): 800  
WEIGHT SPAN (FT): 800  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.37	1.34	0.00	8.49	4.78	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.41	1.03	0.00	3.31	5.94	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.91	0.95	0.00	8.65	2.97	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.60	1.15	0.00	10.51	3.43	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.91	0.61	0.00	5.66	2.21	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.91	0.59	0.00	5.66	2.13	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.91	0.50	5.50	5.66	1.57	13.68	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.55	0.30	0.27	13.60	1.52	1.21	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.41	0.10	0.00	3.31	0.47	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.62	0.21	0.00	8.43	0.93	0.00	0.00	90.00	2.00

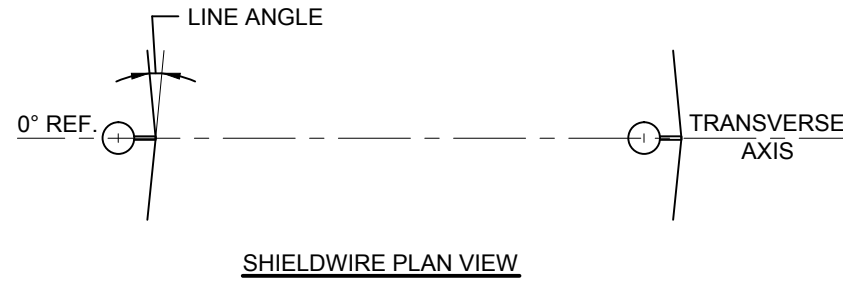




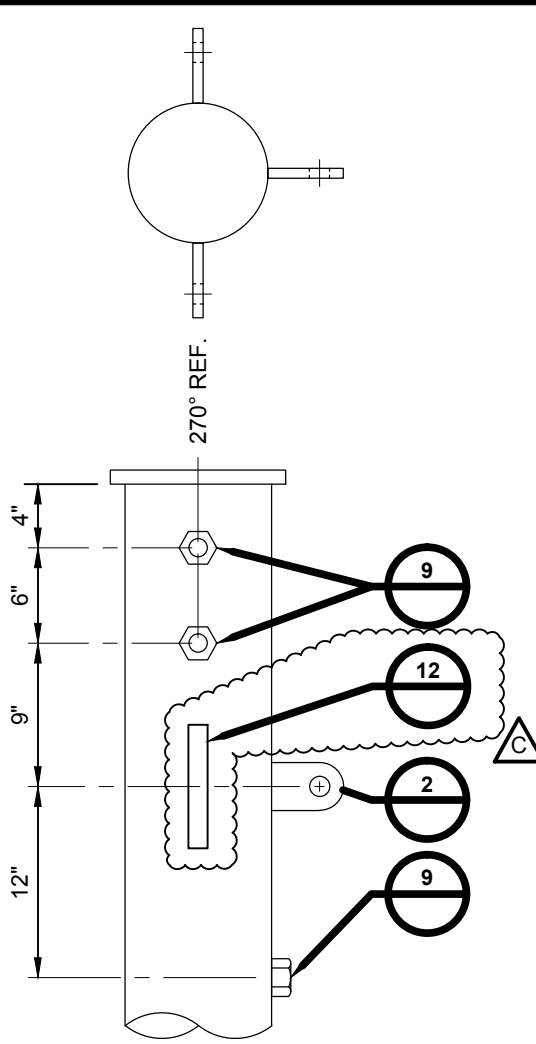
ELEVATION



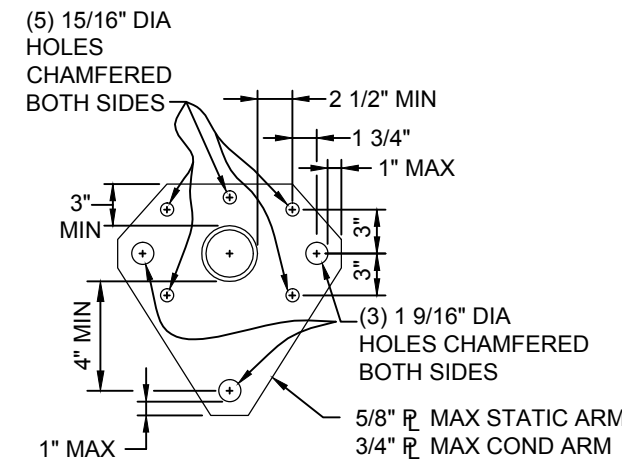
SECTION



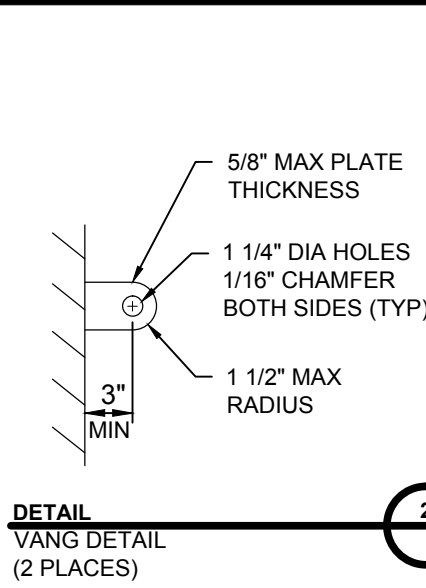
TRANSMISSION PLAN VIEW



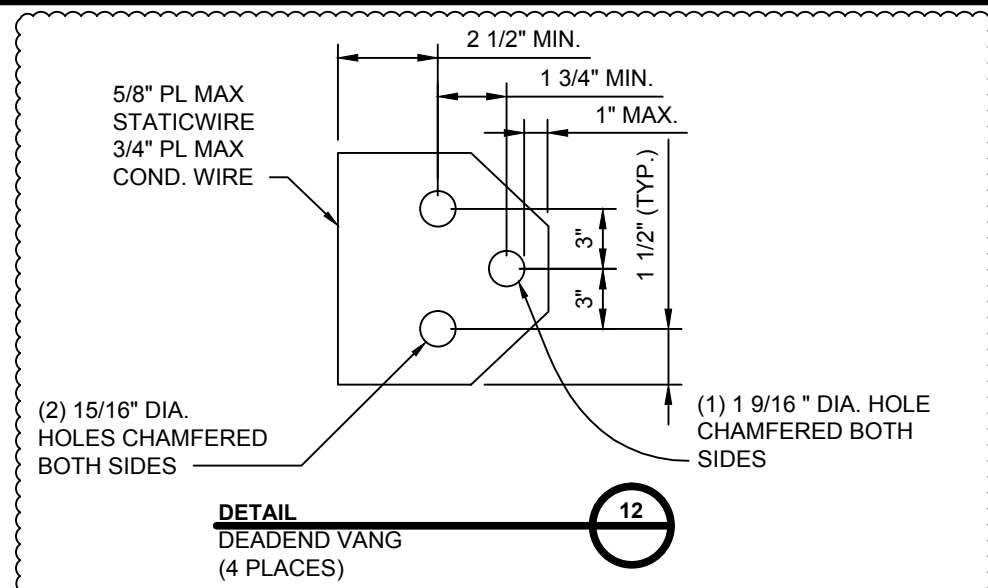
DETAIL  
AERIAL MARKER & SHIELDWIRE  
ATTACHMENT  
(2 PLACES)



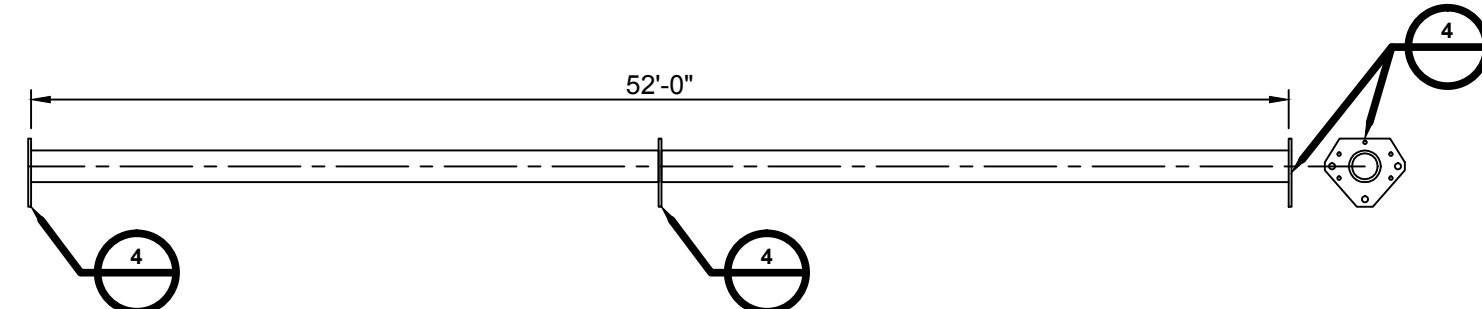
DETAIL  
SUSPENSION/STRAIN PLATE  
(3 PLACES)



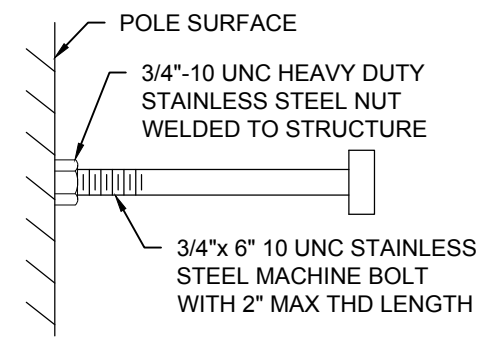
DETAIL  
VANG DETAIL  
(2 PLACES)



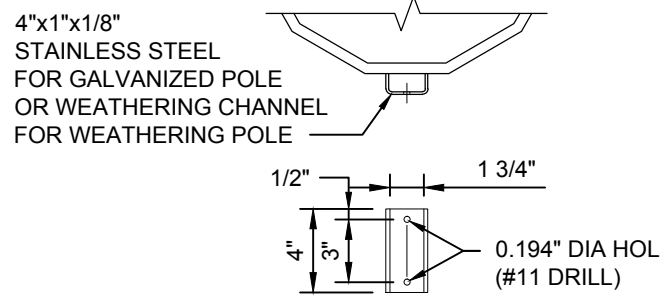
DETAIL  
DEADEND VANG  
(4 PLACES)



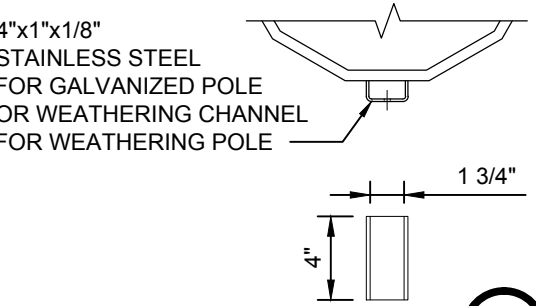
DETAIL  
345KV ARM ASSEMBLY  
(1 PLACE)



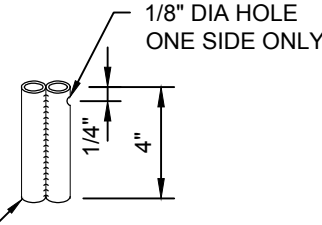
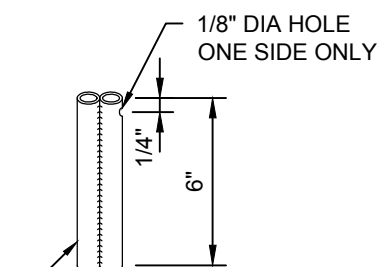
DETAIL  
REMOVABLE GROUNDING BOLT  
(6 PLACES)



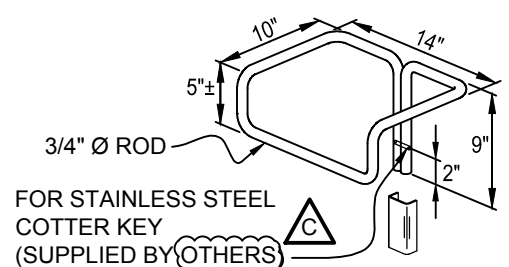
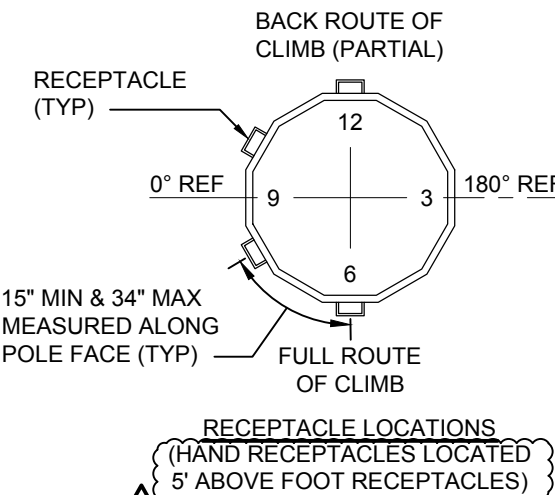
DETAIL  
WARNING SIGN ATTACHMENT  
(2 PLACES)



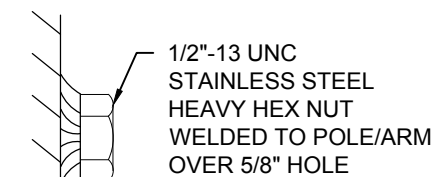
DETAIL  
STEP RUNG RECEPTACLE  
(ACCEPT GO-GAGE REJECT NO-GO-GAGE)  
(AS REQ'D)



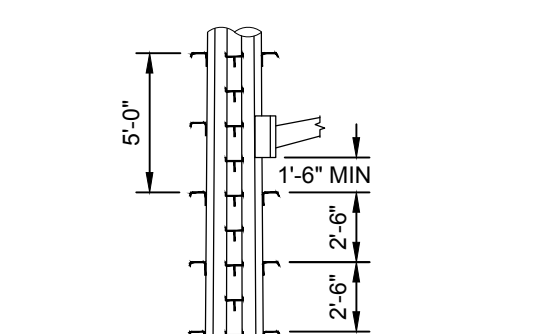
STEP RUNG RECEPTACLE GAGES



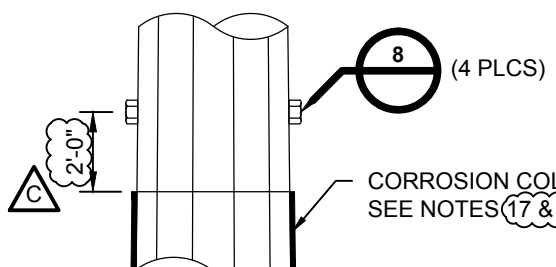
RECEPTACLE & STEP RUNG  
(STEP RUNG SUPPLIED BY OTHERS)



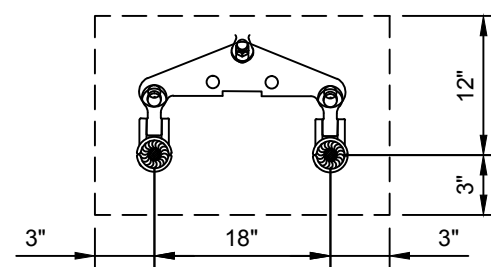
DETAIL  
ATTACHMENT PROVISION LUG  
(AERIAL BRACKET, LINE NUMBER,  
POLE NUMBER & GROUNDING)  
(22 PLACES)



DETAIL  
LINE & POLE NUMBER ATTACHMENT  
(2 PLACES)



DETAIL  
STRUCTURE GROUNDING

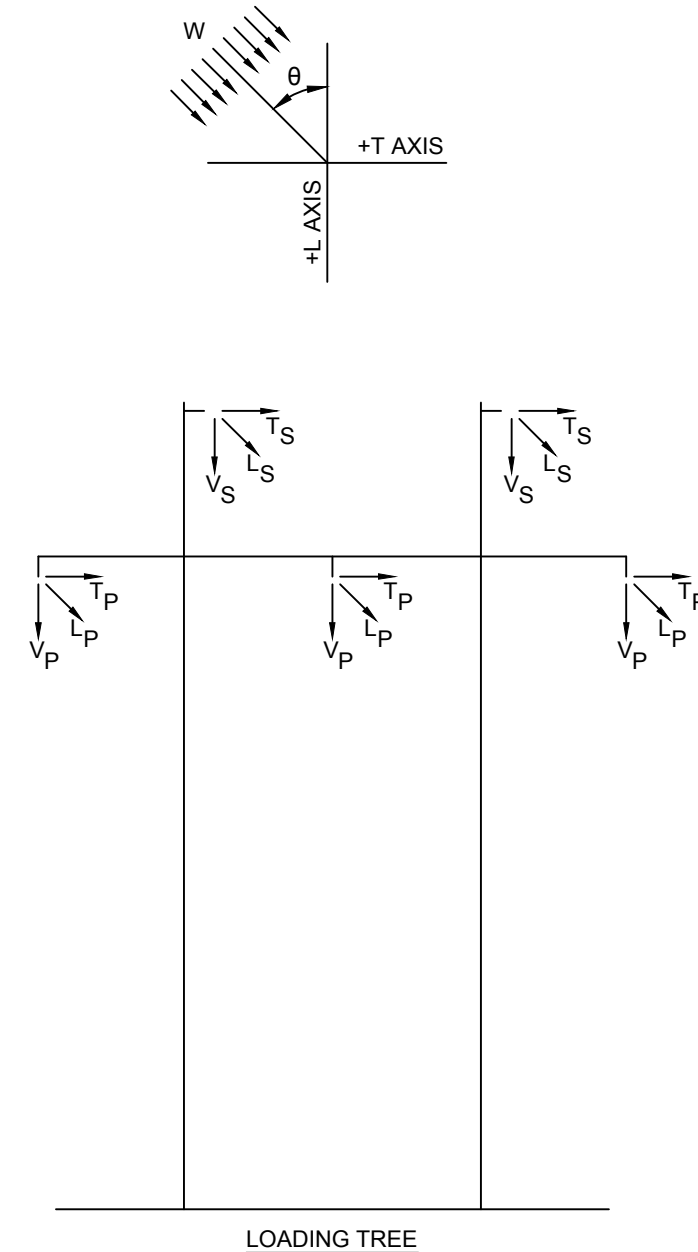


DETAIL  
1-STRING CLEARANCE ENVELOPE  
(3 PLACES)

STRUCTURE NAME: 30-SCHSP-MTW-002  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400H @ NESG HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500H @ NESG HEAVY)  
WIND SPAN (FT): 800  
WEIGHT SPAN (FT): 1100  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.85	1.34	0.00	11.22	4.78	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.54	1.03	0.00	4.39	5.94	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.61	0.95	0.00	11.59	2.97	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	3.55	1.15	0.00	14.16	3.43	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.23	0.61	0.00	7.48	2.21	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.23	0.59	0.00	7.48	2.13	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.23	0.50	5.50	7.48	1.63	17.10	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.75	0.30	0.27	15.21	1.52	1.21	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.54	0.10	0.00	4.39	0.47	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.89	0.21	0.00	10.58	0.93	0.00	0.00	90.00	2.00

- REFERENCES:
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I



- NOTES:
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE "WIND LOAD" (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 0.6 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. VANG AND WING CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  15. POLE SPLICES SHALL USE FLANGED DESIGN.
  16. ARM AND X-BRACE SIZE, SHAPE AND MOUNTING HARDWARE REQUIRED SHALL BE DETERMINED AND FURNISHED BY POLE SUPPLIER.
  17. SINGLE X-BRACE REQUIRED FOR STRUCTURES UP TO 95 FEET IN HEIGHT ABOVE GROUND LINE. TWO X-BRACES SHALL BE USED FOR STRUCTURES WITH HEIGHTS ABOVE GROUND LINE EXCEEDING 95 FEET.
  18. STEEL PLATE, A MINIMUM OF 1/4" THICKNESS GREATER THAN THAT REQUIRED FOR COLUMN STRENGTH SHALL BE IN PLACE IN THE AREA 3'-0" ABOVE AND 5'-0" BELOW THE NOMINAL GROUND LINE.
  19. APPLY COAL TAR EPOXY ON INSIDE AND OUTSIDE OF POLE FROM BUTT OF POLE TO 12" ABOVE TOP OF CORROSION COLLAR.
  20. BELOW GROUND CORROSION PROTECTION COATING MATERIAL SHALL BE SUPPLIED (ONE QUART PER TWO STRUCTURES) TO "TOUCH UP" SCRATCHES OCCURRING IN SHIPPING AND HANDLING. A COPY OF THE MSDS SHEET SHALL BE SUPPLIED WITH THE "TOUCH UP" MATERIALS.
  21. BRACING USE, CONFIGURATION AND LOCATIONS TO BE DETERMINED BY MANUFACTURER.
  22. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

CONTRACT SERVICES							
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	
C	MISC. REVISIONS		5/27/15	KAK			
B	MISC. REVISIONS		5/8/15	BLH			
A	RELEASE FOR RFP BID		5/1/15	BLH			
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	

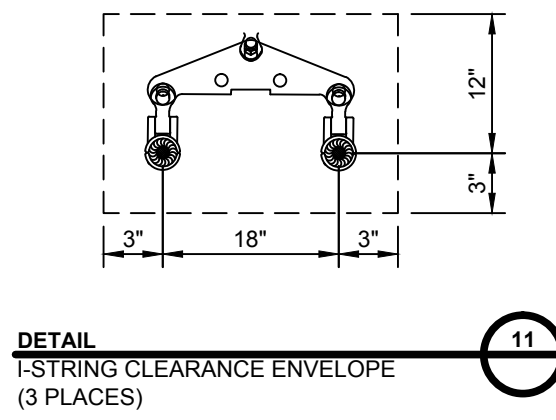
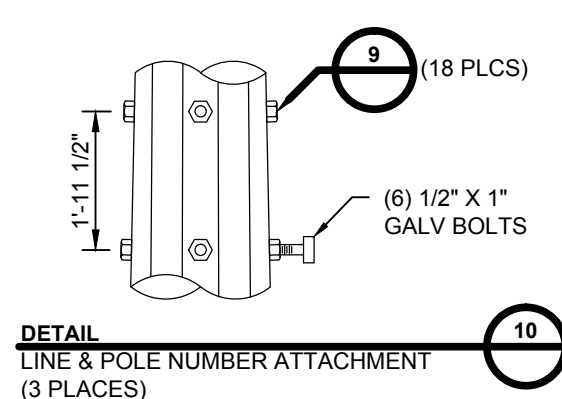
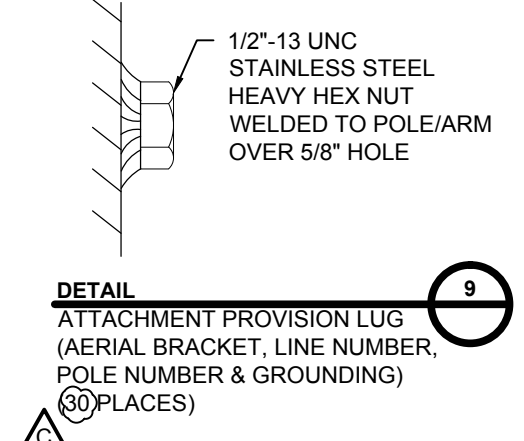
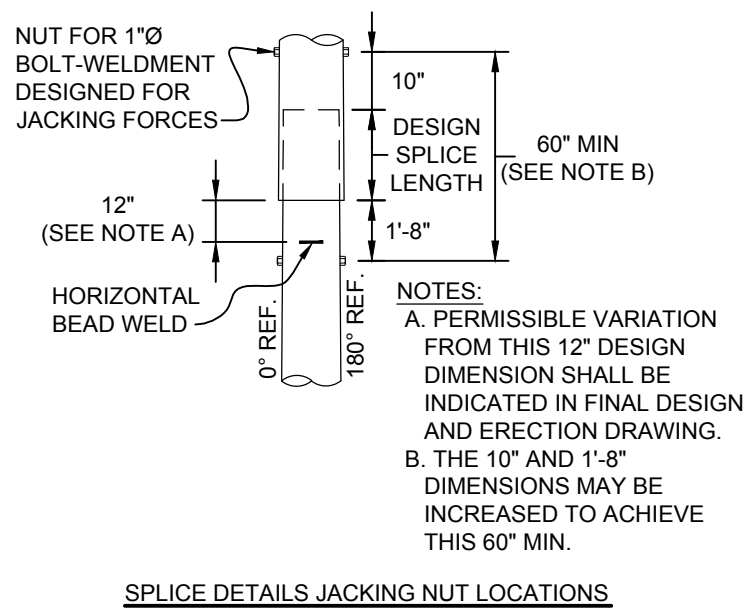
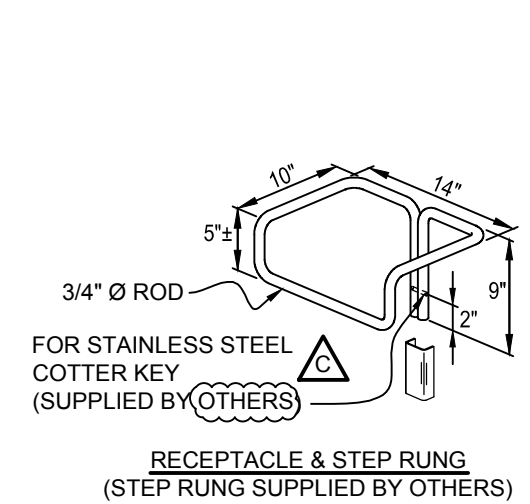
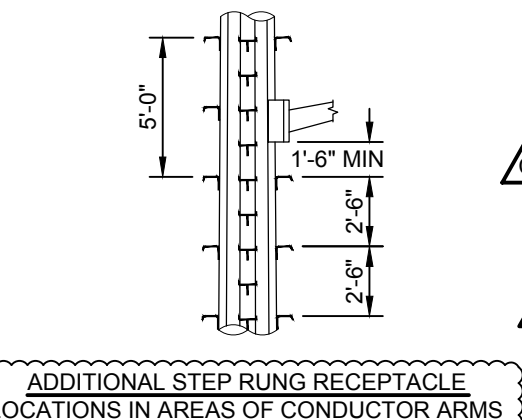
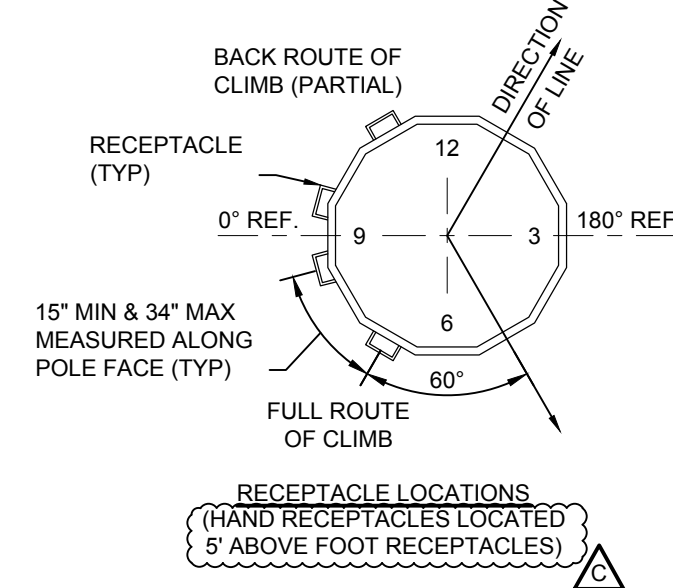
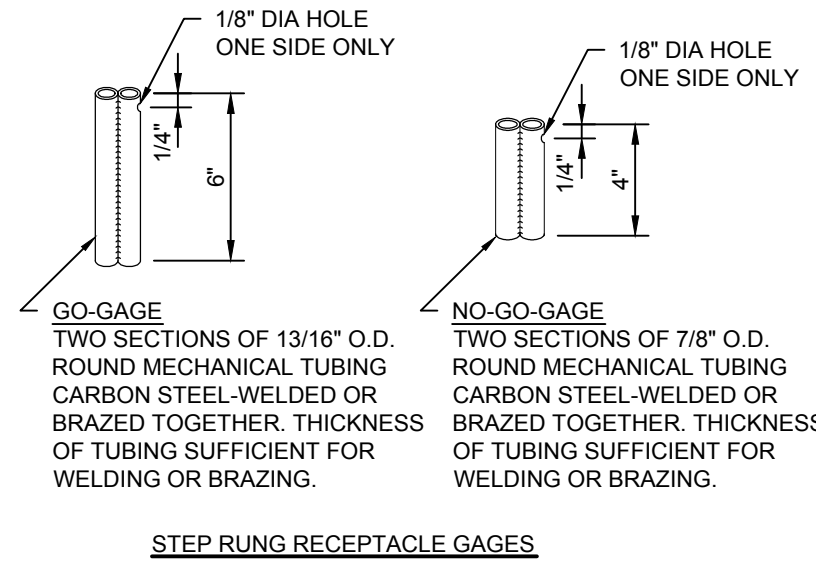
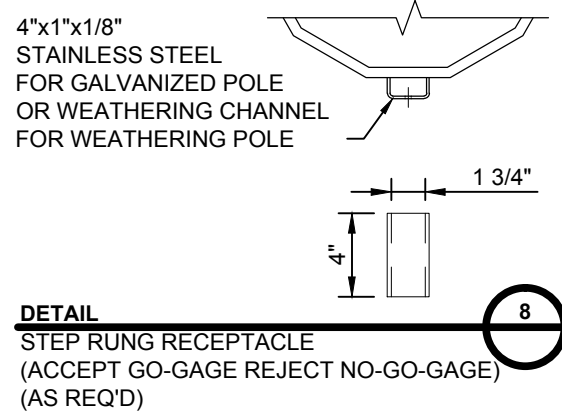
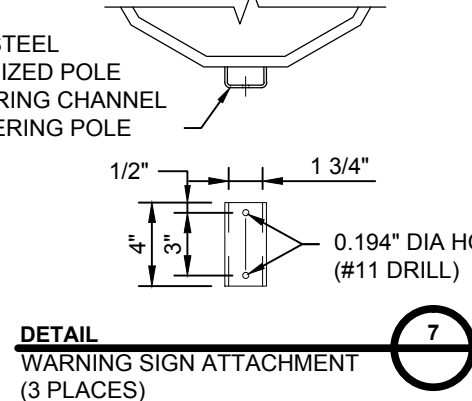
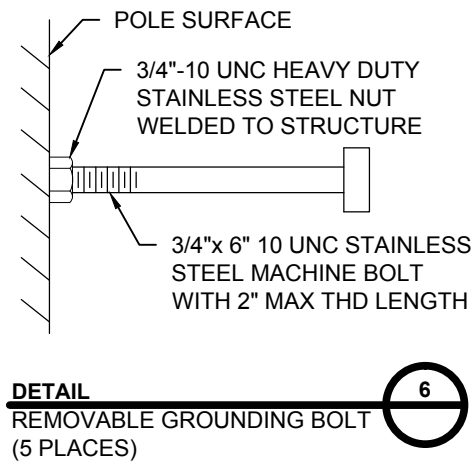
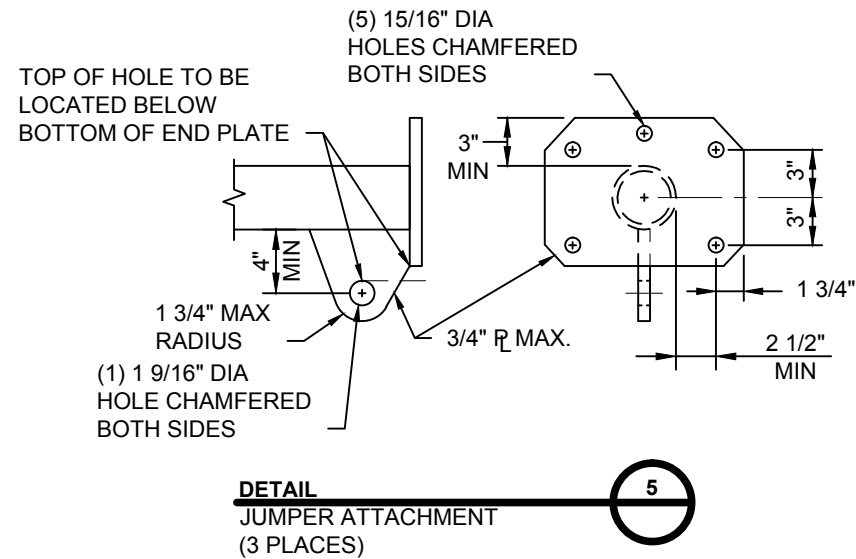
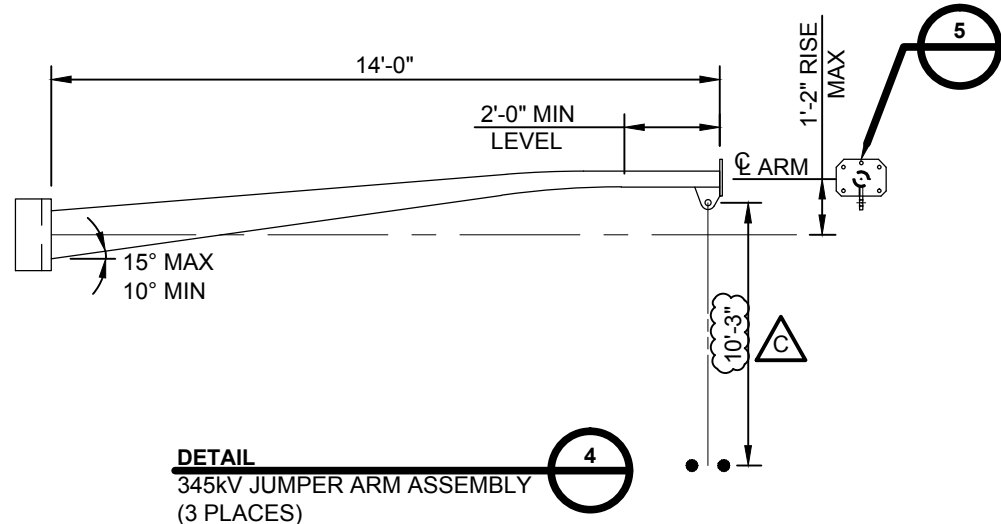
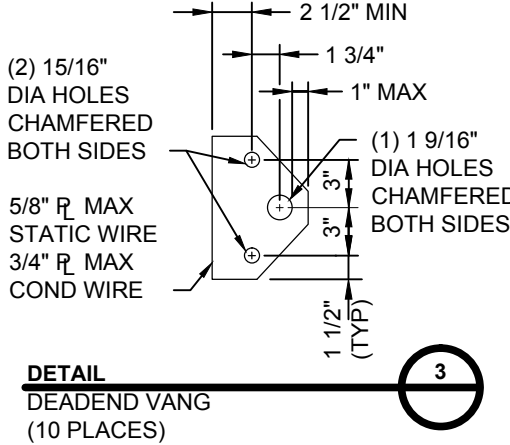
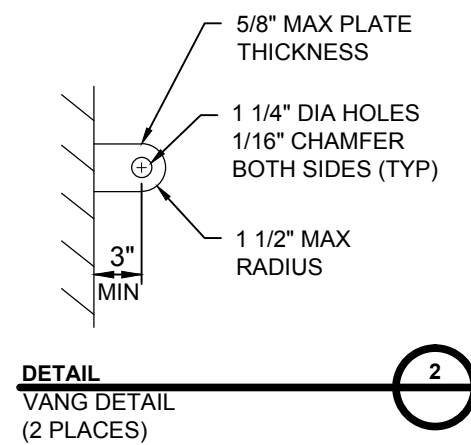
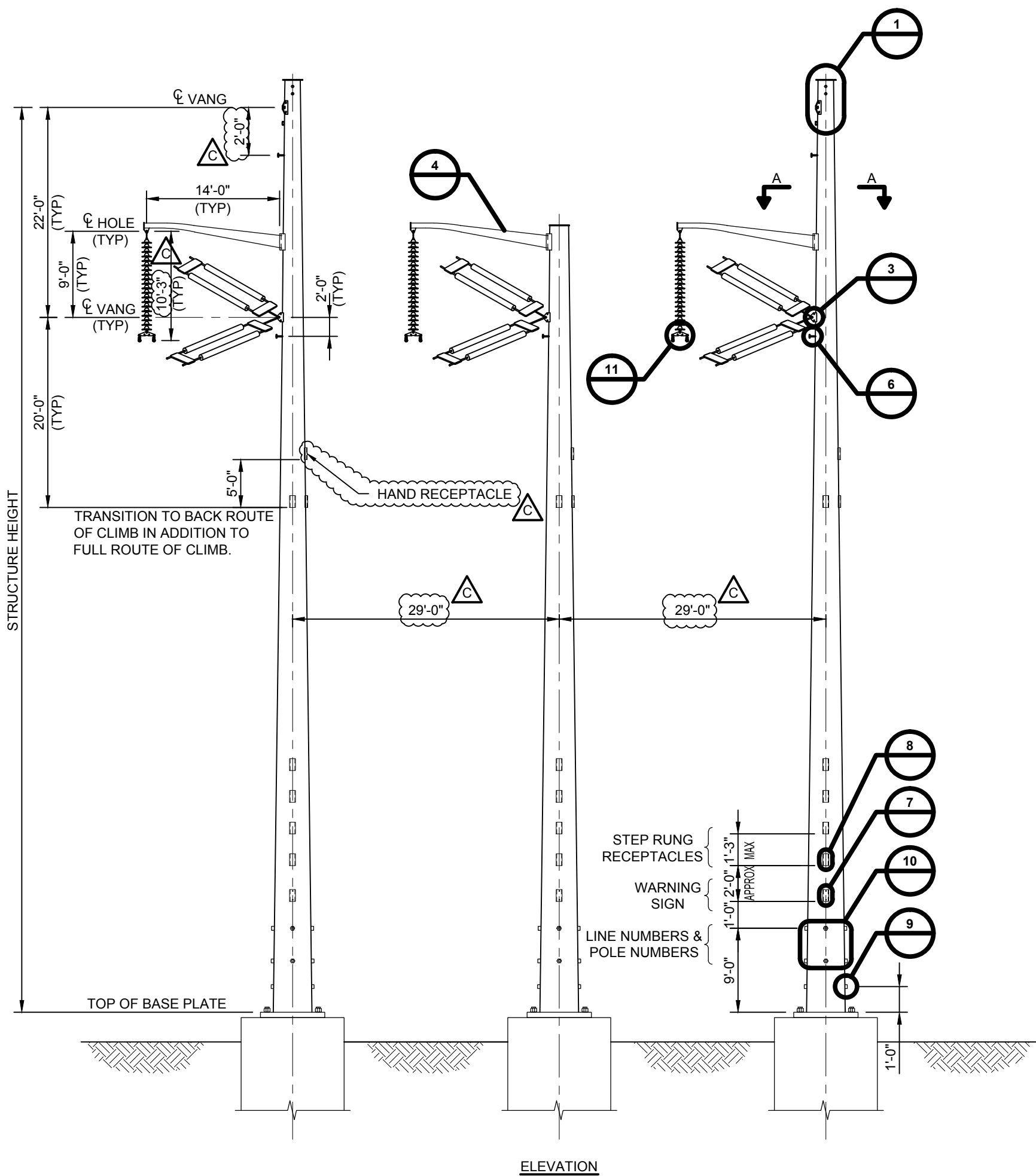
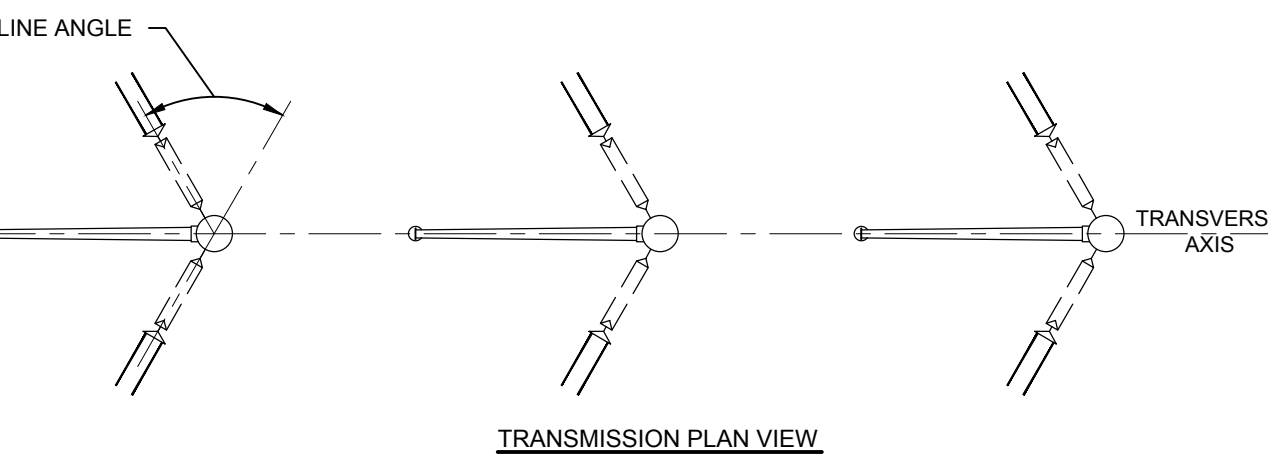
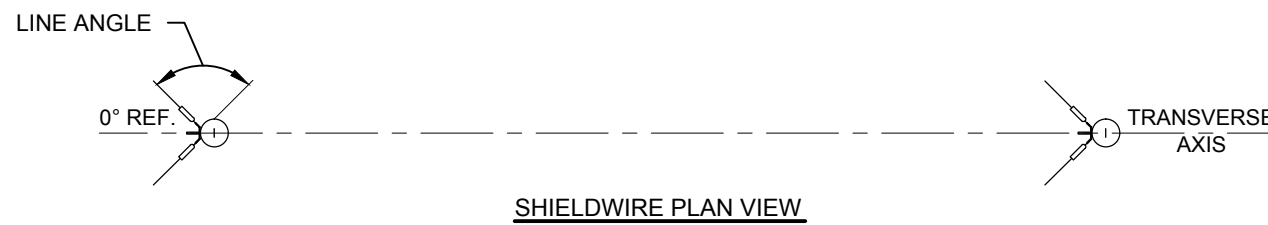
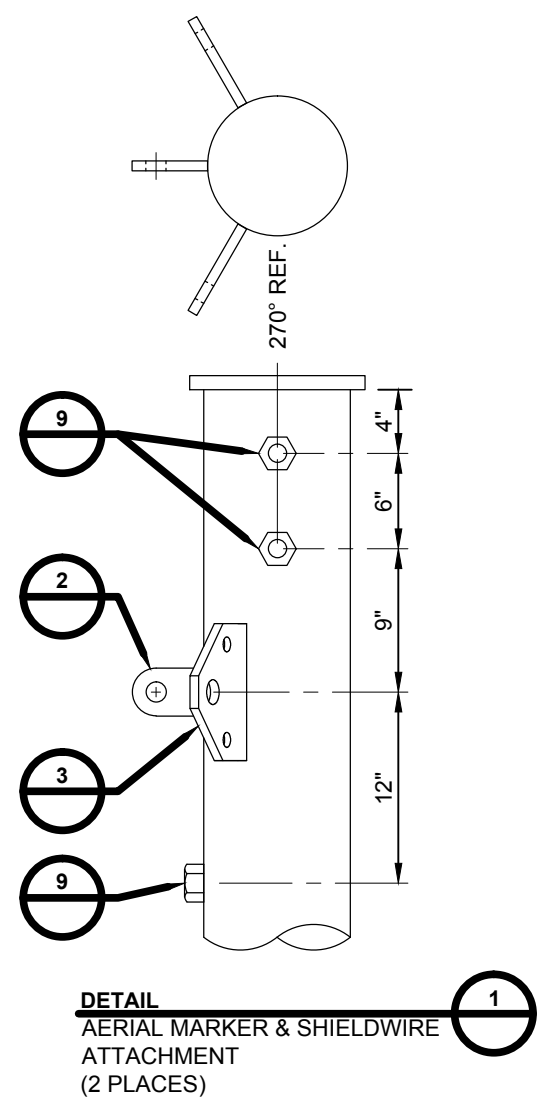
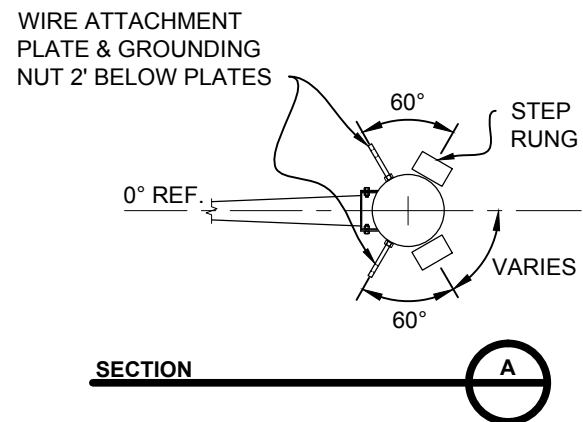
345kV AC MEDIUM TANGENT 0-2°  
30-SCHSP-MTW-002  
LOAD & DESIGN DRAWING

C	DRAWN	BLH
CET	ENGINEER	
TAB	CHECKED	
	APPROVED	
5/1/15	DATE	

SCALE	FILE: TSP-06.DWG	DRAWING NO.
NTS	IMAGE:	TSP-06-001

PRELIMINARY - NOT  
FOR CONSTRUCTION

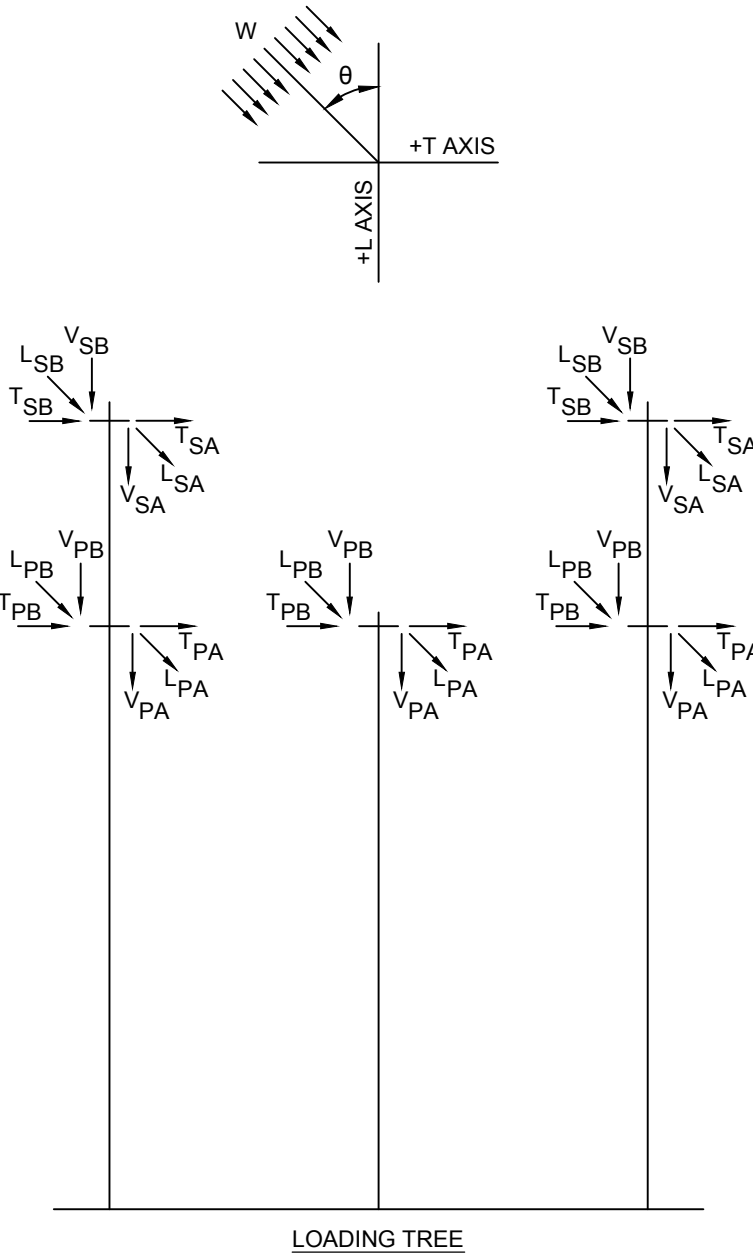




STRUCTURE NAME: 30-SCHSP-LDW-045  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 475 WIND SPAN BACK (FT): 475  
WEIGHT SPAN AHEAD (FT): 625 WEIGHT SPAN BACK (FT): 625  
LINE ANGLE: 0 - 45 DEGREES


LOADING CASE		DESIGN LOADS																	
		TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.08	4.28	9.62	1.08	4.28	-9.62	7.87	17.76	41.24	7.87	17.76	-41.24	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.33	2.24	4.51	0.33	2.24	-4.51	3.01	11.89	23.11	3.01	11.89	-23.11	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.50	3.46	8.01	1.50	3.46	-8.01	7.58	13.17	31.53	7.58	13.17	-31.53	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.04	4.27	9.92	2.04	4.27	-9.92	9.04	15.42	36.98	9.04	15.42	-36.98	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.72	2.47	5.83	0.72	2.47	-5.83	5.25	10.36	24.99	5.25	10.36	-24.99	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.72	2.34	5.50	0.72	2.34	-5.50	5.25	9.52	22.80	5.25	9.52	-22.80	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.72	2.34	5.50	0.72	0.24	0.00	5.25	9.52	22.80	5.25	0.79	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.85	1.50	0.27	1.85	2.07	-5.23	16.51	6.91	1.21	5.87	9.40	-23.49	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.33	1.13	2.96	0.33	1.13	-2.96	3.01	5.10	13.34	3.01	5.10	-13.34	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.46	2.26	5.92	2.46	2.26	-5.92	7.83	10.21	26.68	7.83	10.21	-26.68	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.33	1.70	4.43	0.33	1.70	-4.43	3.01	7.92	20.69	3.01	7.92	-20.69	0.00	90.00	1.00

- REFERENCES:
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

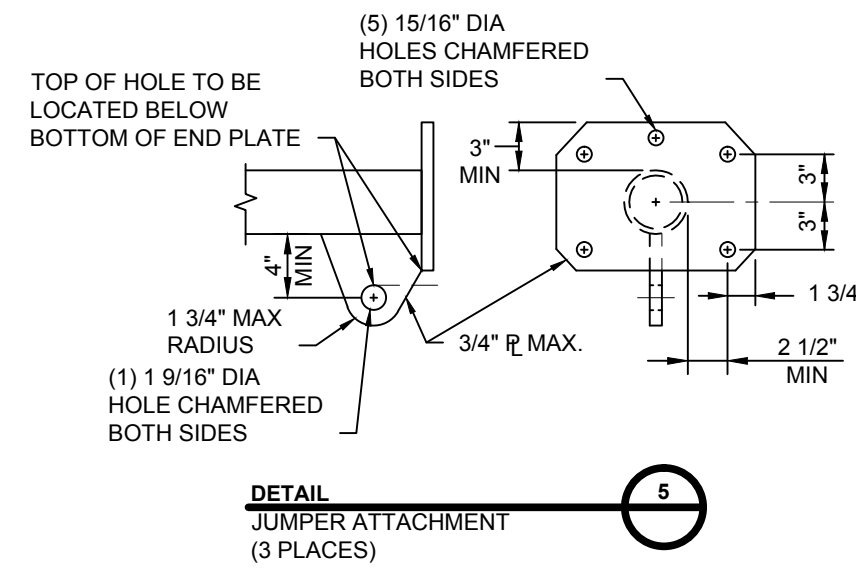
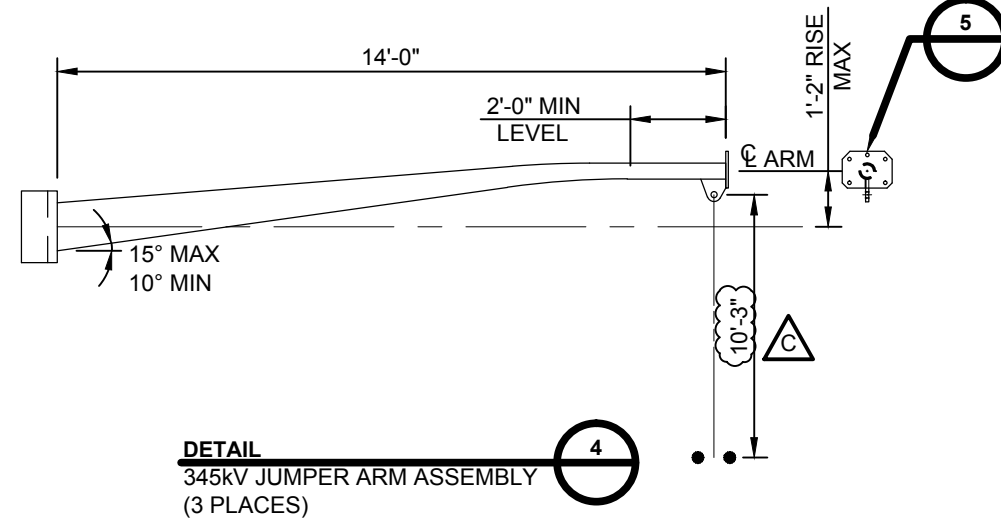
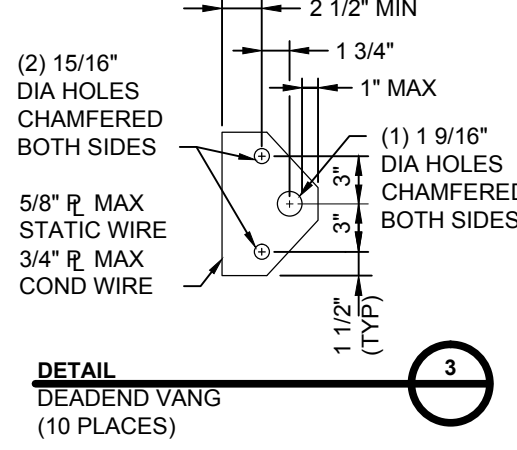
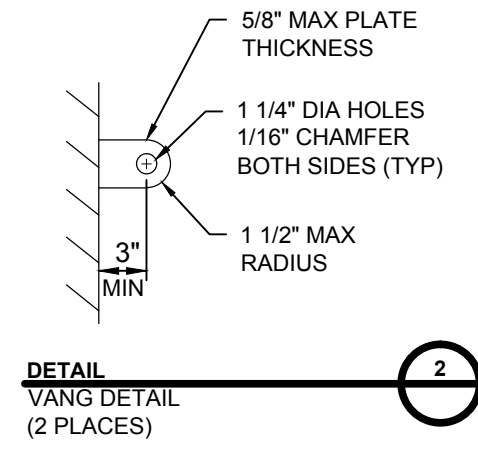
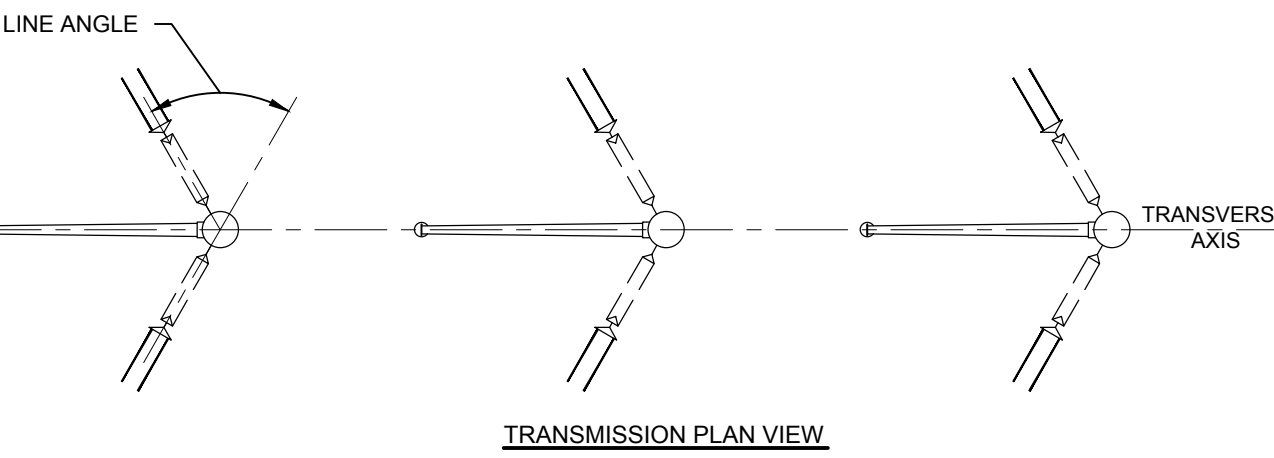
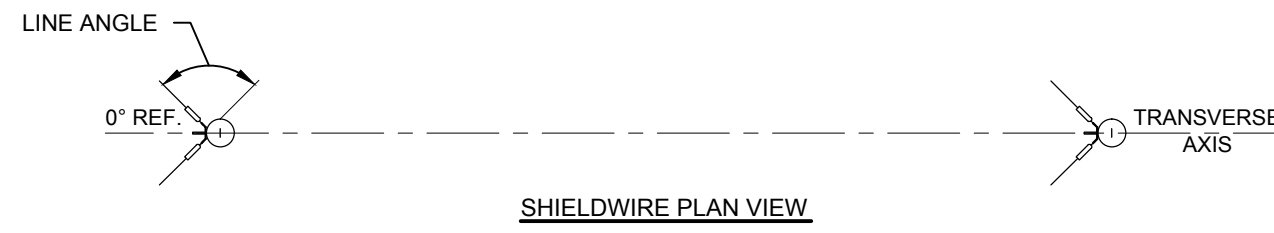
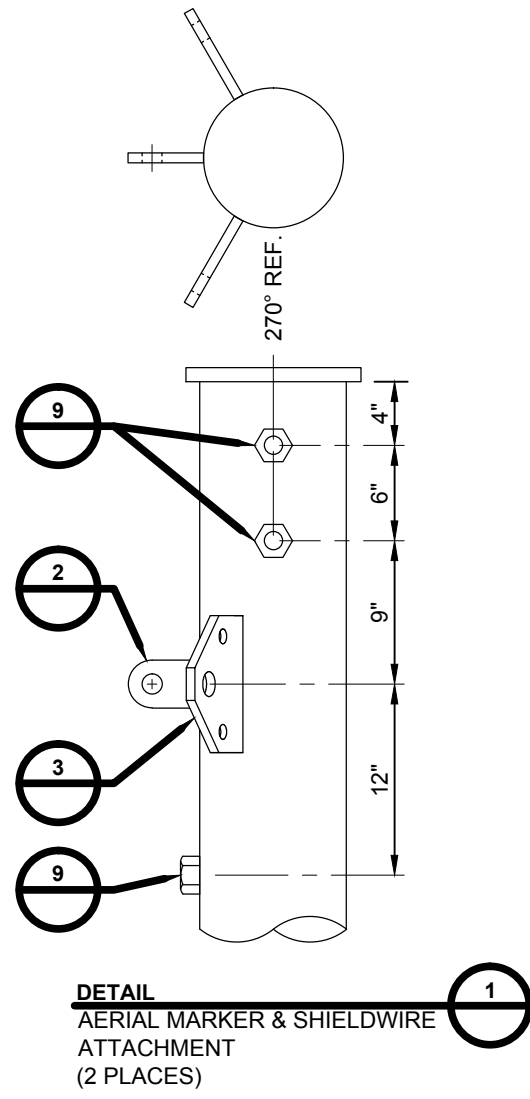
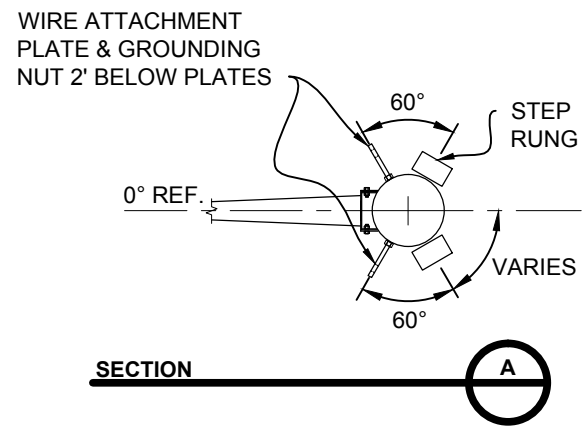


- NOTES:
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  - SNUB ANGLES SHALL BE LIMITED TO A 15° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

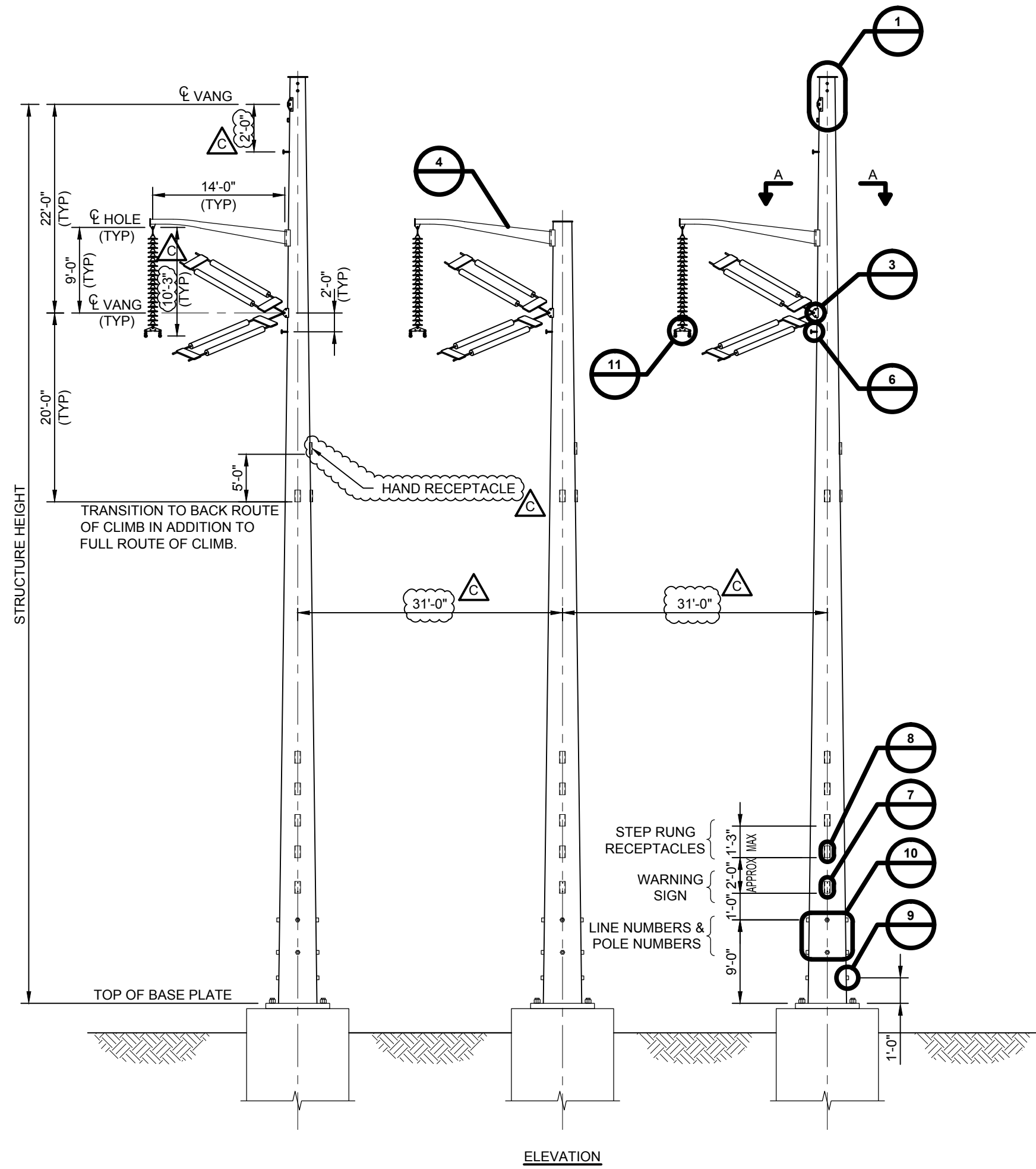
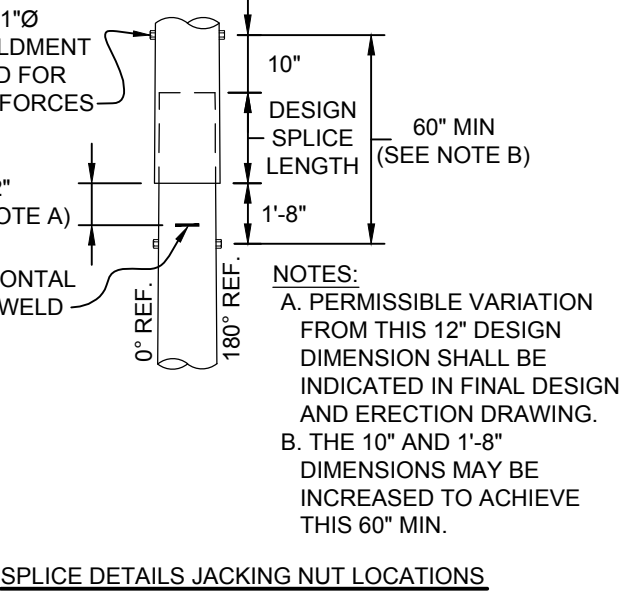
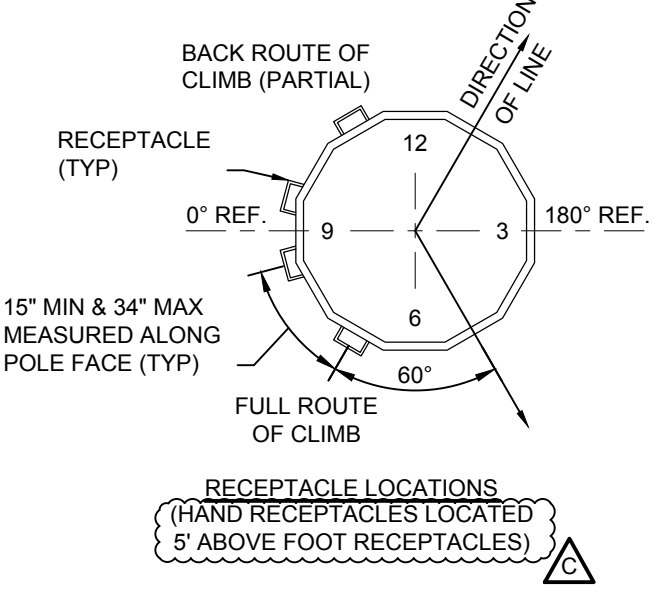
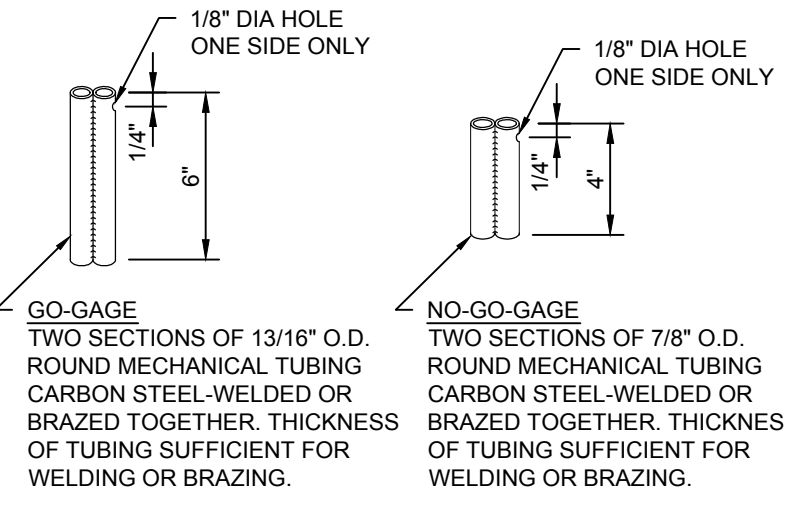
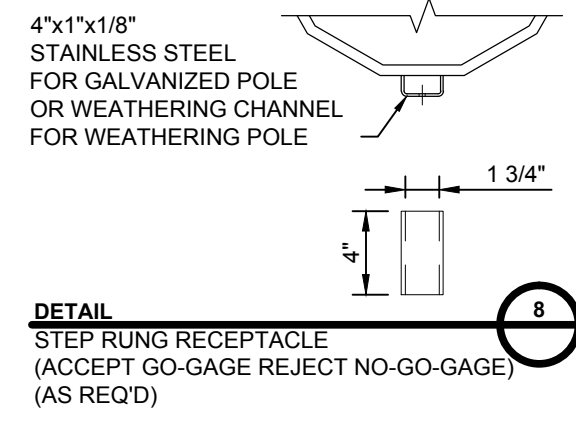
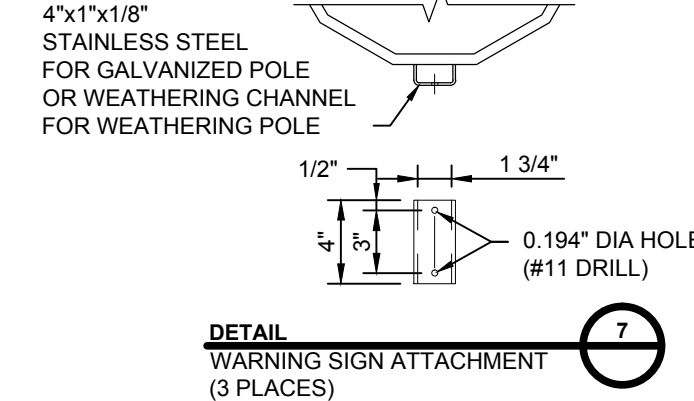
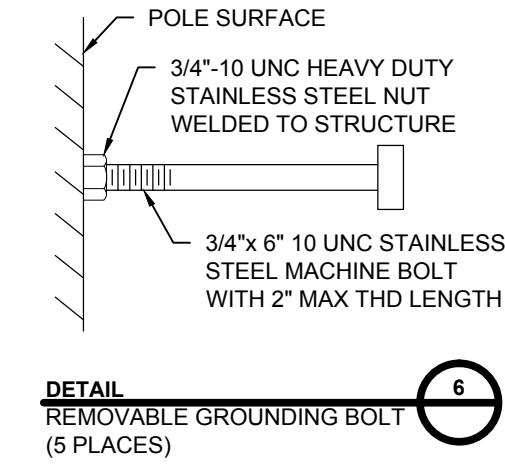
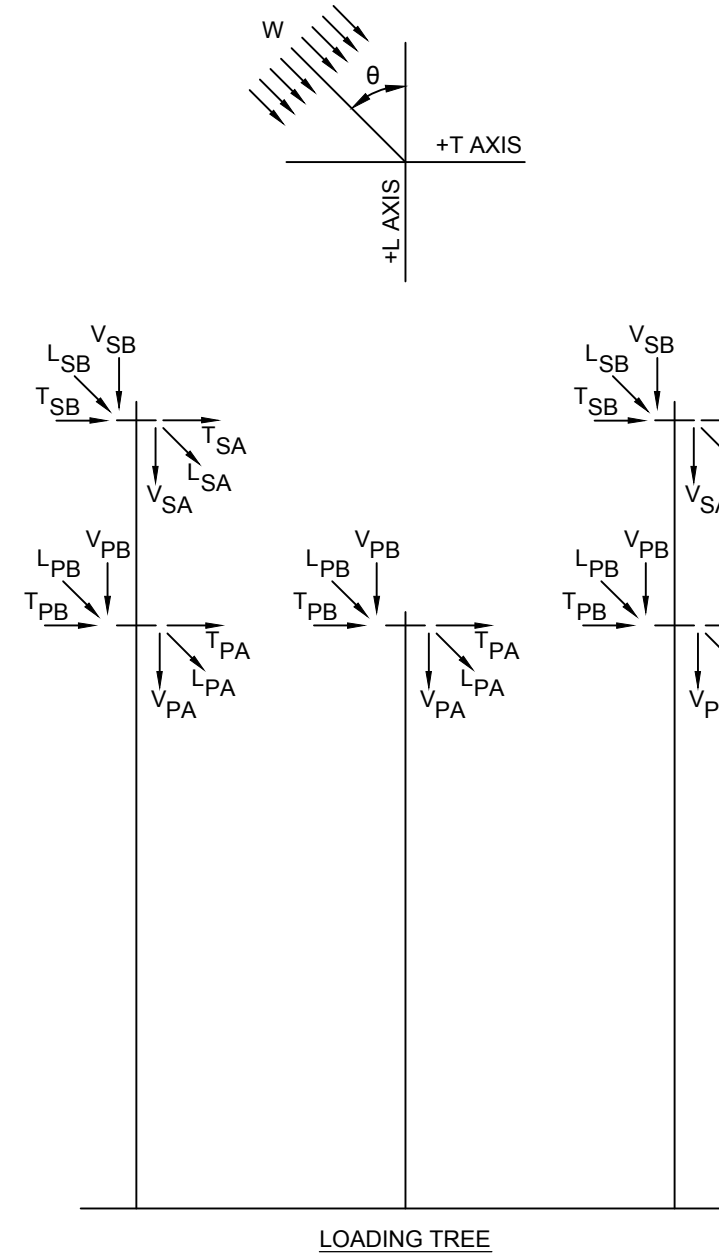
PRELIMINARY - NOT FOR CONSTRUCTION

CONTRACT SERVICES								 THE NORTHERN PASS	C	
									DRAWN BLH	
									ENGINEER CET	
									CHECKED TAB	
									APPROVED	
	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	345kV AC LIGHT DEADEND 0-45° 30-SCHSP-LOW-045 LOAD & DESIGN DRAWING		DATE 5/1/15
	C	MISC. REVISIONS		5/27/15	MSP					
	B	MISC. REVISIONS		5/8/15	BLH					
	A	RELEASE FOR RFP BID		5/1/15	BLH					
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	SCALE NTS	FILE: TSP-07.DWG IMAGE:	DRAWING NO. TSP-07-001





- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE - SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I



STRUCTURE NAME: 30-SCHSP-MDW-065  
 345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
 OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
 WIND SPAN AHEAD (FT): 275 WIND SPAN BACK (FT): 275  
 WEIGHT SPAN AHEAD (FT): 300 WEIGHT SPAN BACK (FT): 300  
 LINE ANGLE: 45 - 65 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.56	5.52	8.89	0.56	5.52	-8.89	4.91	23.30	38.10	4.91	23.30	-38.10	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.18	2.72	4.17	0.18	2.72	-4.17	1.85	14.18	21.35	1.85	14.18	-21.35	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	0.75	4.53	7.40	0.75	4.53	-7.40	4.39	17.58	29.13	4.39	17.58	-29.13	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.00	5.61	9.17	1.00	5.61	-9.17	5.09	20.60	34.16	5.09	20.60	-34.16	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.37	3.27	5.39	0.37	3.27	-5.39	3.27	13.89	23.09	3.27	13.89	-23.09	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.37	3.09	5.08	0.37	3.09	-5.08	3.27	12.71	21.06	3.27	12.71	-21.06	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.37	3.09	5.08	0.37	0.14	0.00	3.27	12.71	21.06	3.27	0.46	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.41	1.40	0.25	1.63	2.85	-4.83	13.01	6.40	1.12	4.12	12.86	-21.70	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.18	1.59	2.73	0.18	1.59	-2.73	1.85	7.17	12.32	1.85	7.17	-12.32	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.17	3.18	5.47	2.17	3.18	-5.47	5.50	14.33	24.65	5.50	14.33	-24.65	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.18	2.38	4.09	0.18	2.38	-4.09	1.85	11.11	19.11	1.85	11.11	-19.11	0.00	90.00	1.00

- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 60° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTABLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTABLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
 

**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  13. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  16. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  17. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

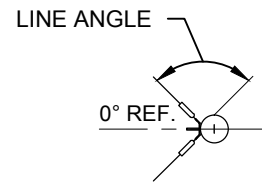
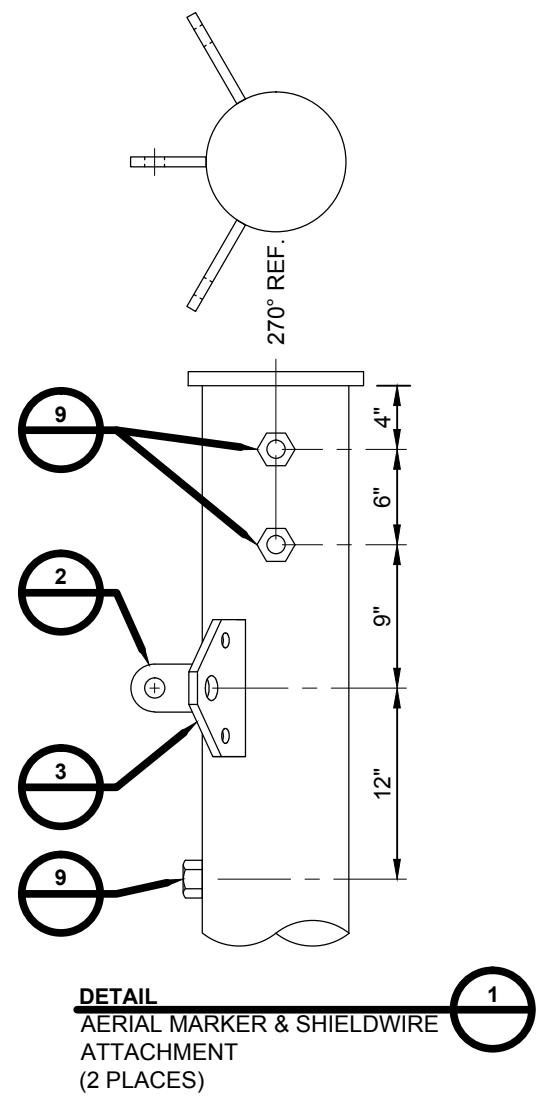
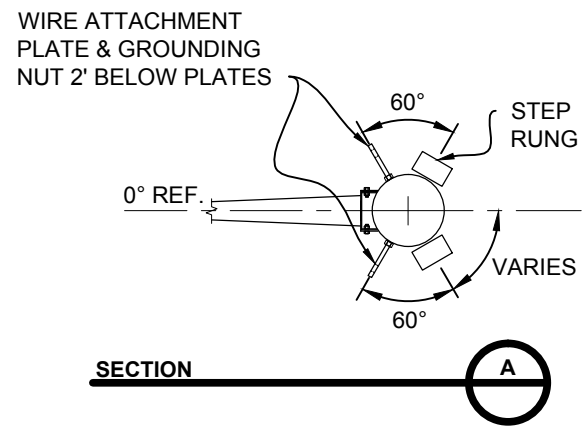
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APPR												APPROVED	
C						MISC. REVISIONS						DATE 5/1/15	
B						MISC. REVISIONS							
A						RELEASE FOR RFP BID							
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CONT/PE#						DATE						DRAWING NO. TSP-08-001	
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APPR													

345kV AC MEDIUM DEADEND 45-65°  
 30-SCHSP-MDW-065  
 LOAD & DESIGN DRAWING

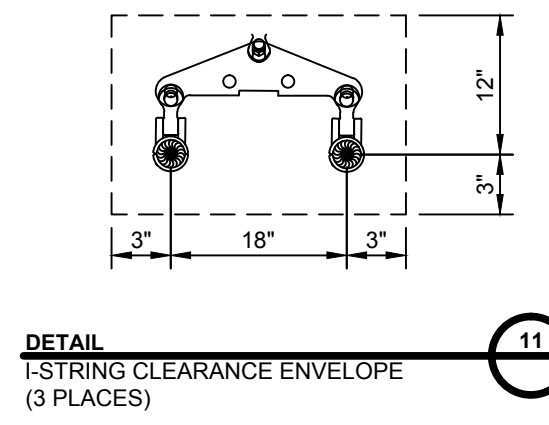
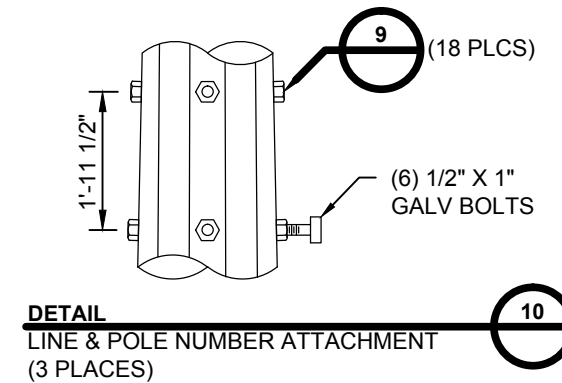
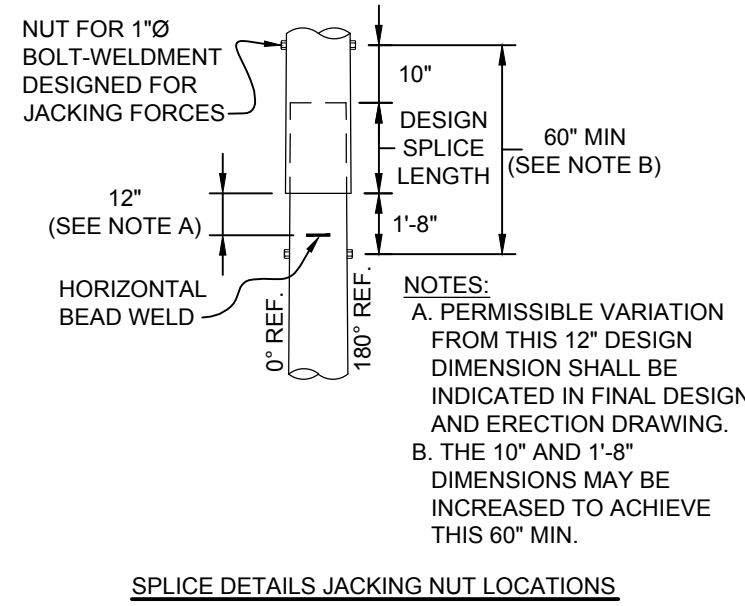
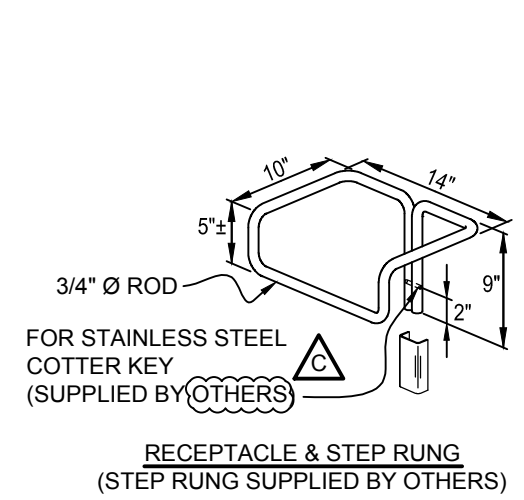
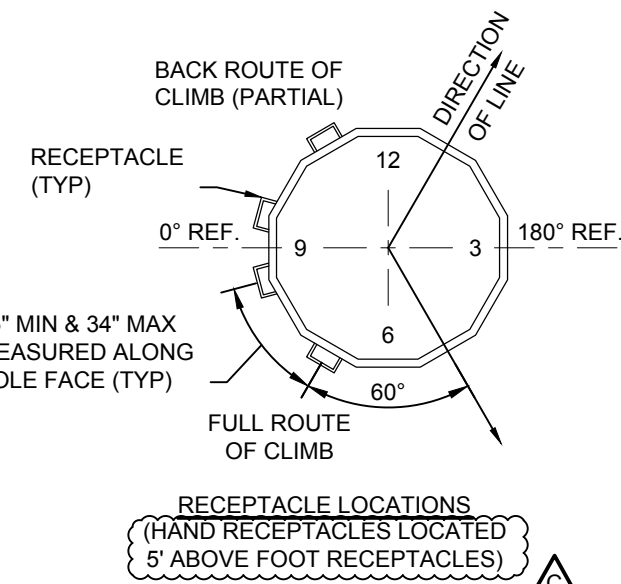
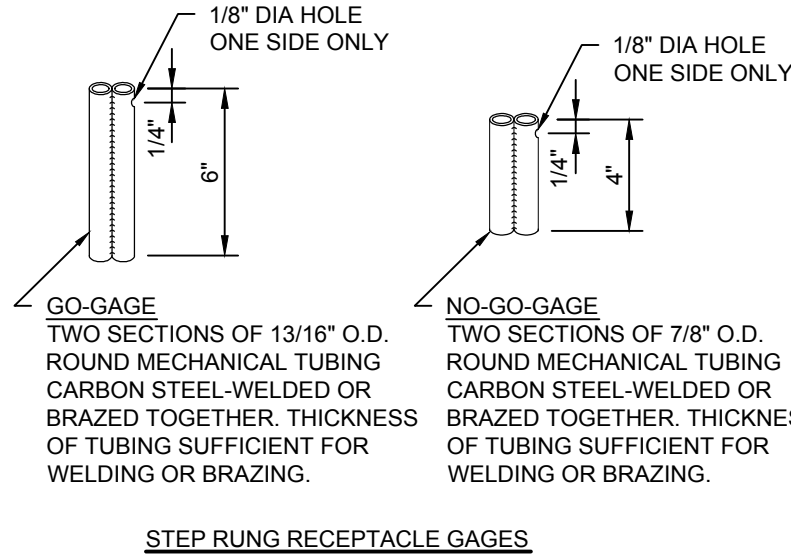
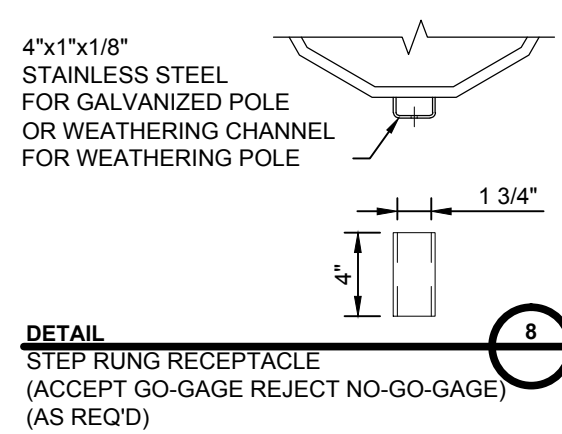
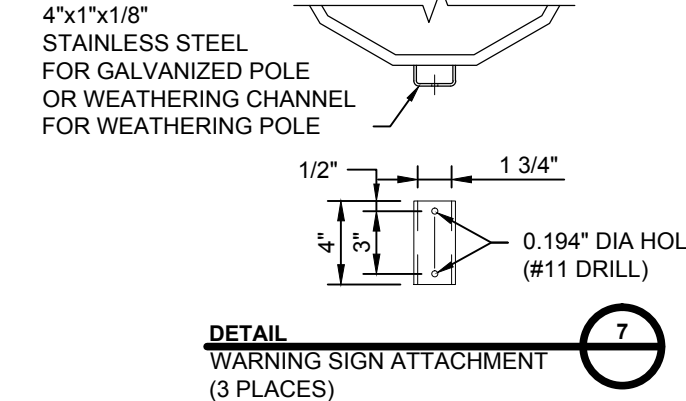
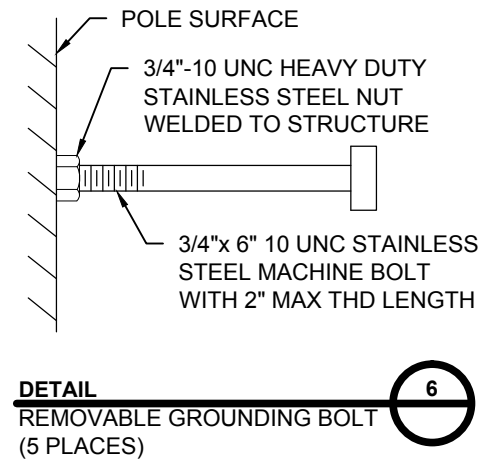
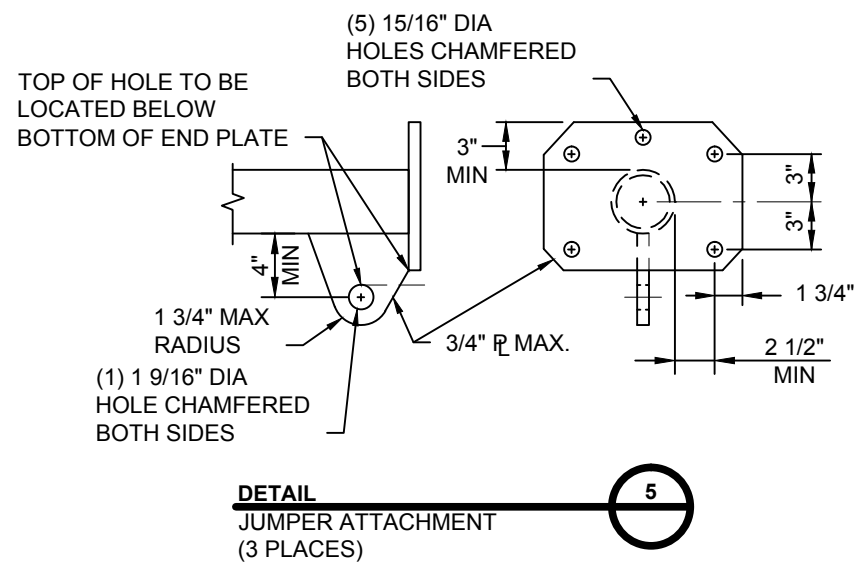
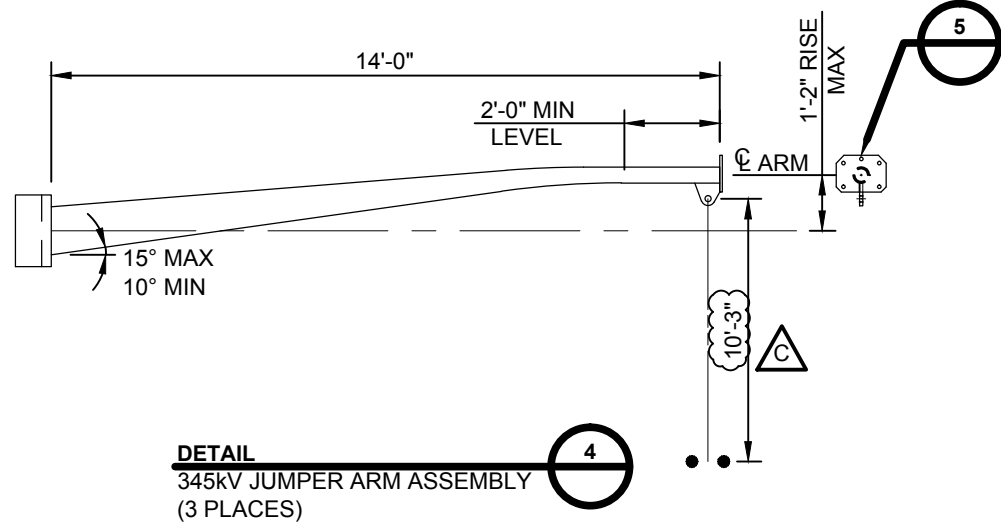
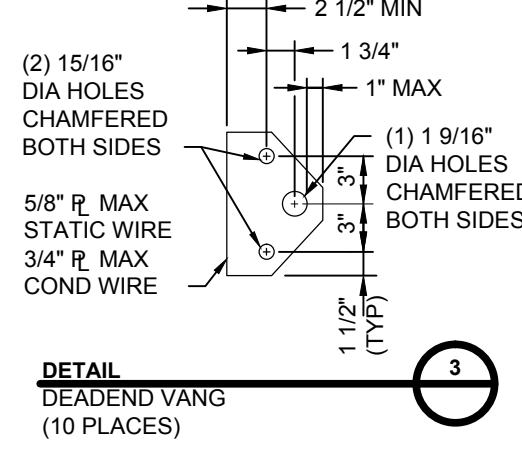
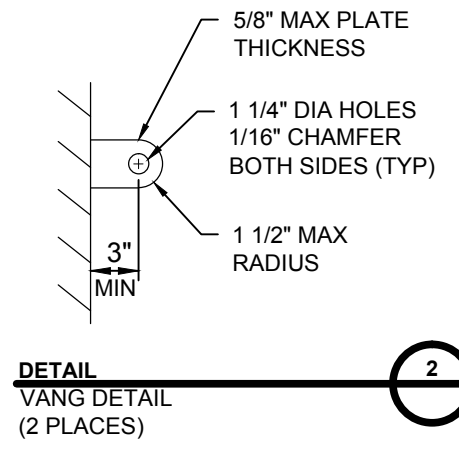
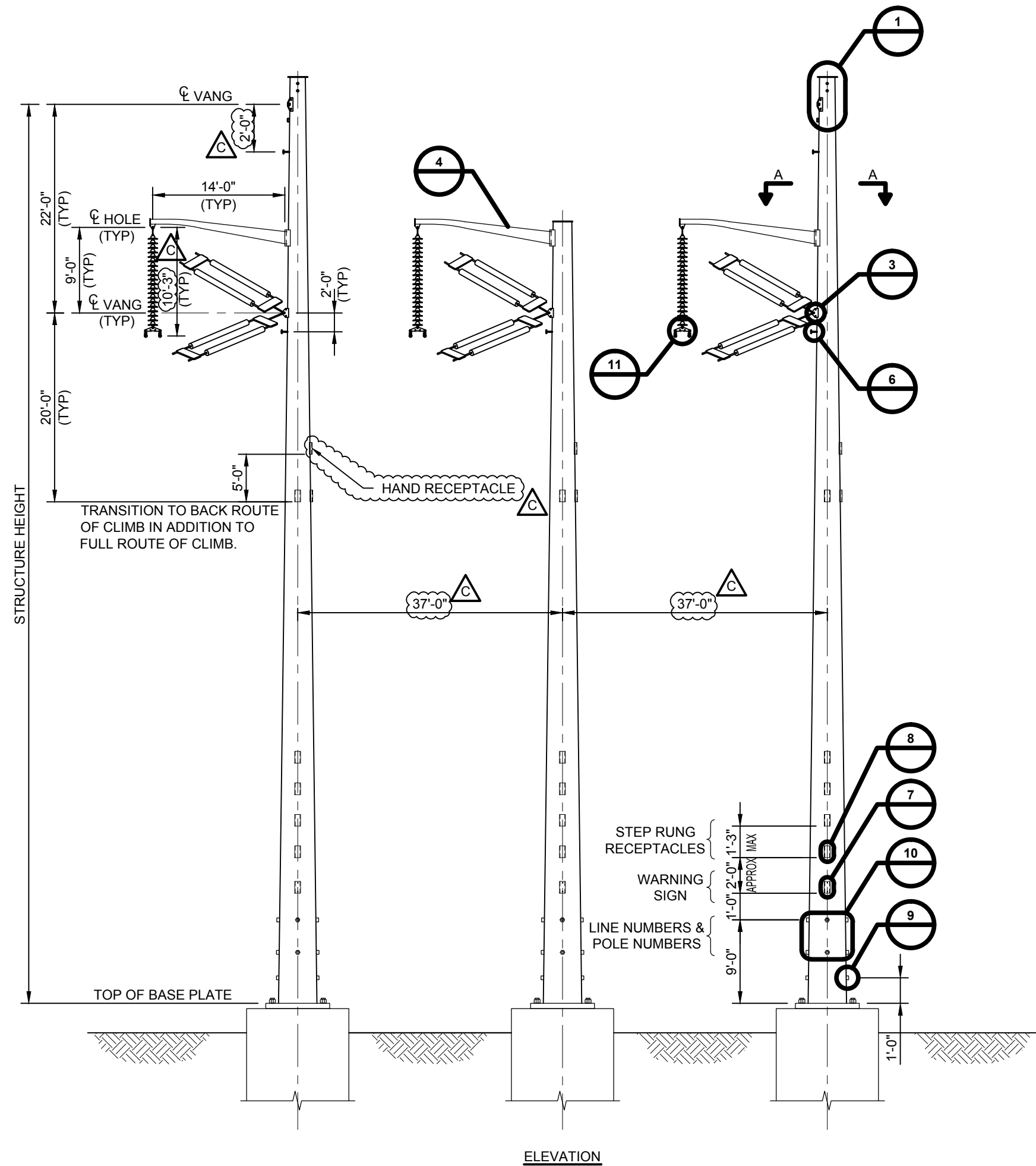
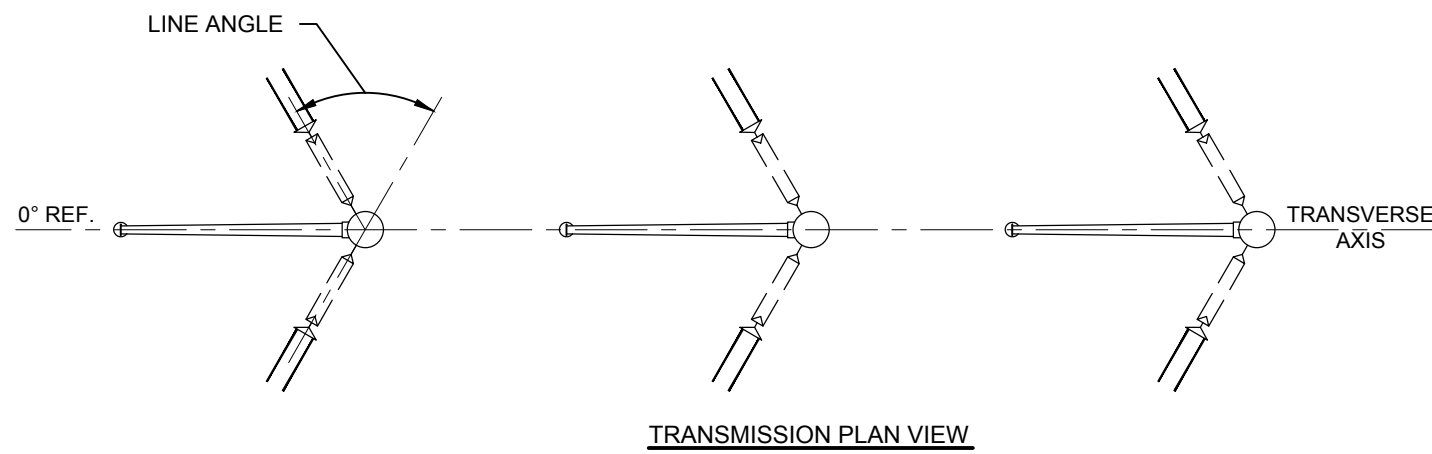
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**PRELIMINARY - NOT FOR CONSTRUCTION**





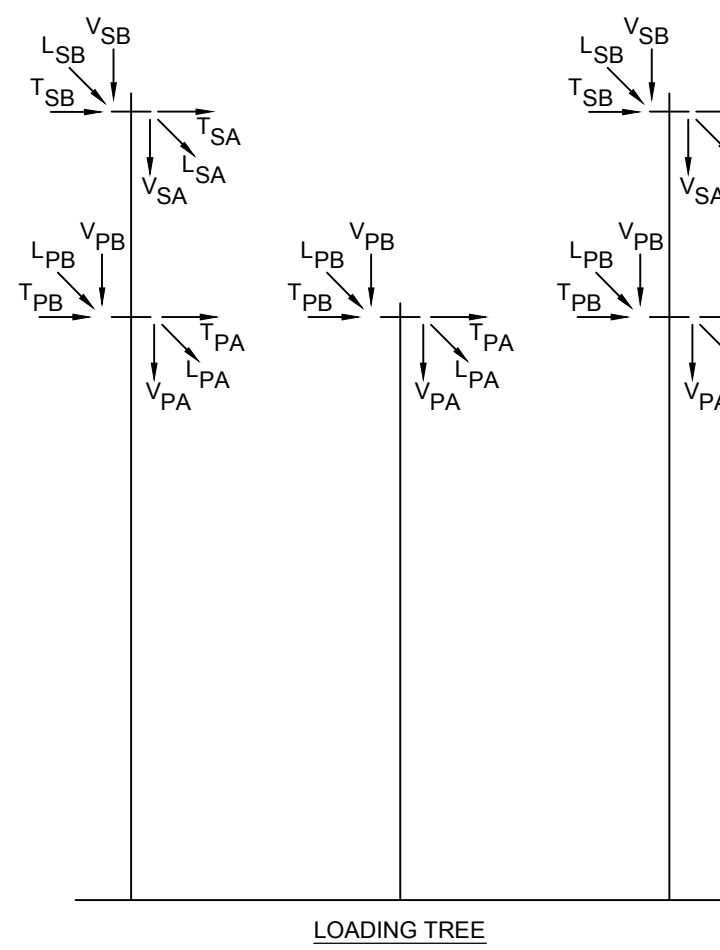
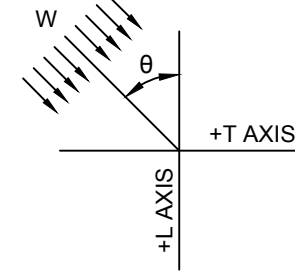
SHIELDWIRE PLAN VIEW



STRUCTURE NAME: 30-SCHSP-HDW-090  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 325 WIND SPAN BACK (FT): 325  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 65 - 90 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	7.21	8.12	0.84	7.21	-8.12	6.50	30.52	34.78	6.50	30.52	-34.78	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	3.54	3.81	0.26	3.54	-3.81	2.48	18.43	19.49	2.48	18.43	-19.49	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	5.94	6.76	1.15	5.94	-6.76	6.11	23.05	26.59	6.11	23.05	-26.59	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	7.34	8.37	1.56	7.34	-8.37	7.22	27.01	31.19	7.22	27.01	-31.19	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	4.29	4.92	0.56	4.29	-4.92	4.33	18.21	21.08	4.33	18.21	-21.08	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	4.05	4.64	0.56	4.05	-4.64	4.33	16.66	19.23	4.33	16.66	-19.23	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	4.05	4.64	0.56	4.05	4.33	16.66	19.23	4.33	0.54	0.00	4.00	90.00	1.00	
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.32	0.23	1.74	3.74	-4.41	14.89	6.03	1.02	5.06	16.89	-19.81	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.26	2.09	2.49	0.26	2.09	-2.49	2.48	9.43	11.25	2.48	9.43	-11.25	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.33	4.18	4.99	2.33	4.18	-4.99	6.75	18.86	22.50	6.75	18.86	-22.50	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.26	3.13	3.74	0.26	3.13	-3.74	2.48	14.63	17.45	2.48	14.63	-17.45	0.00	90.00	1.00

- REFERENCES:
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH H
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

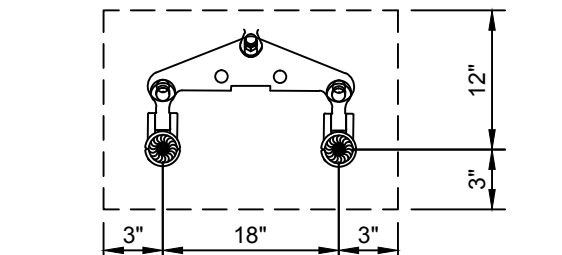
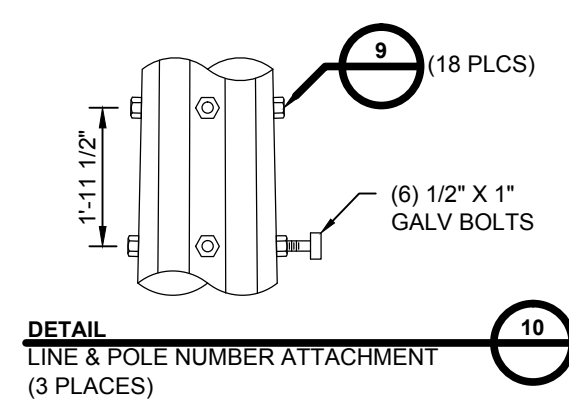
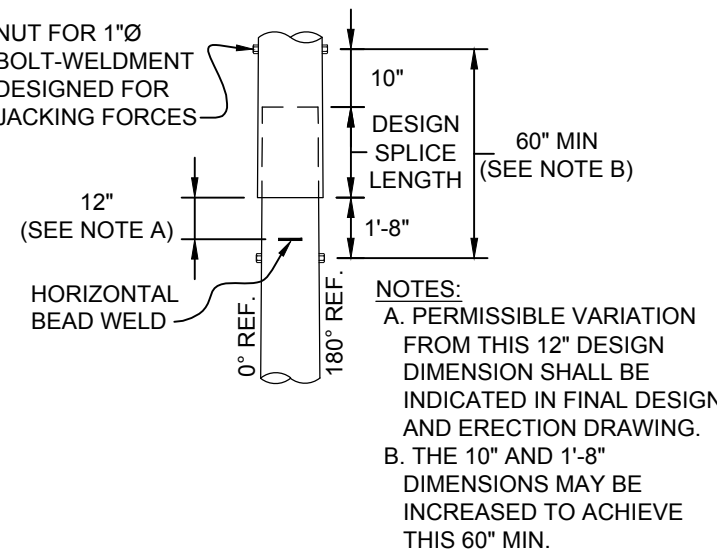
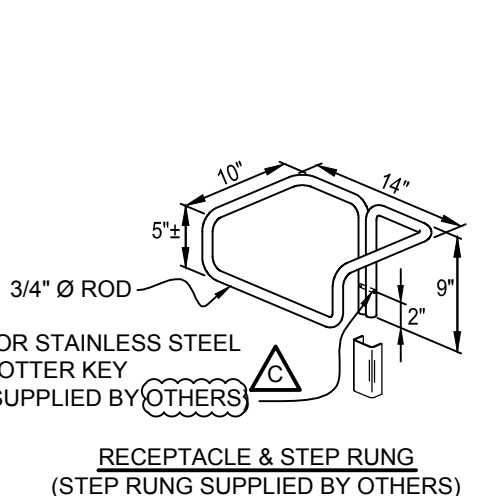
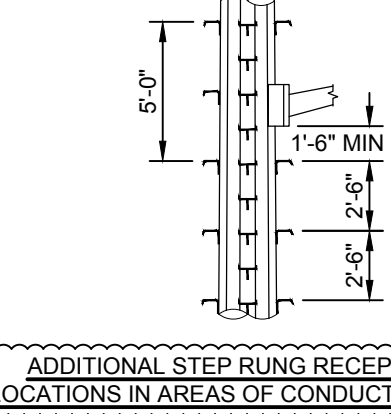
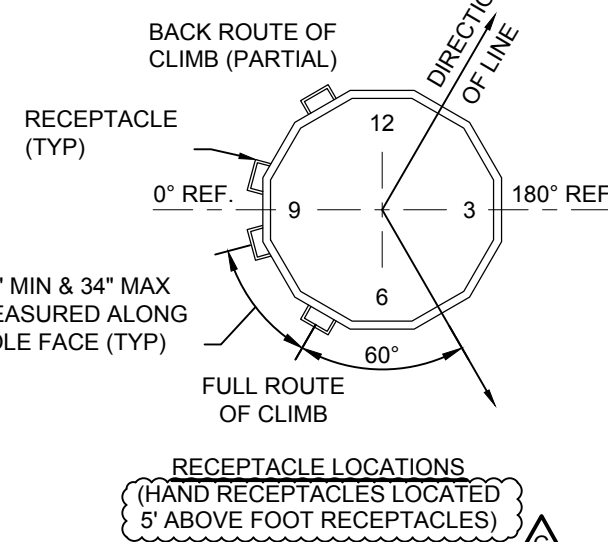
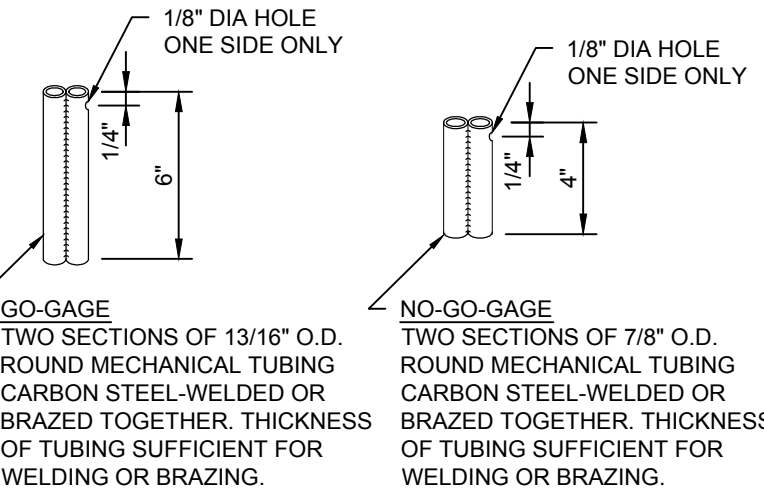
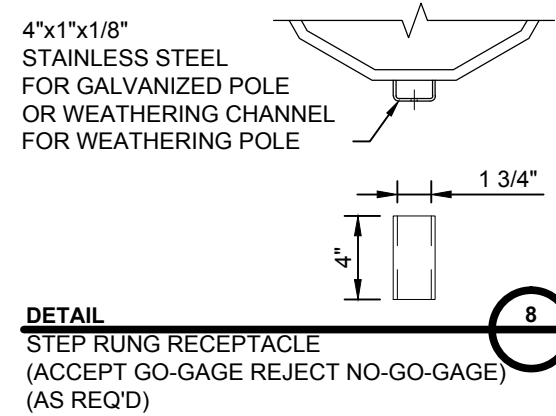
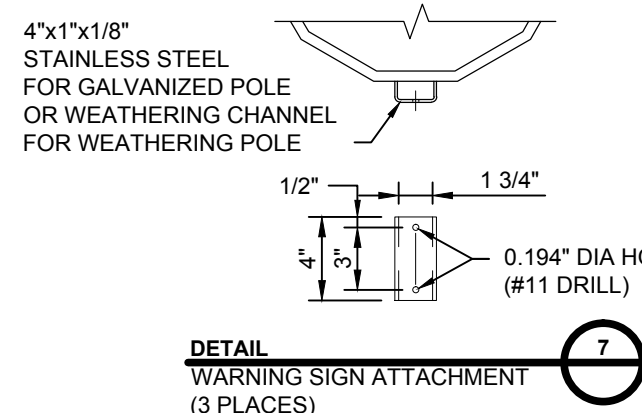
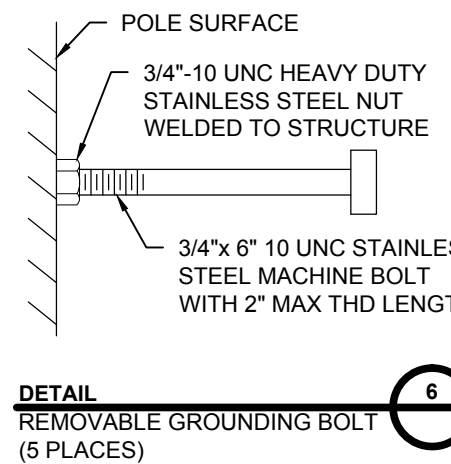
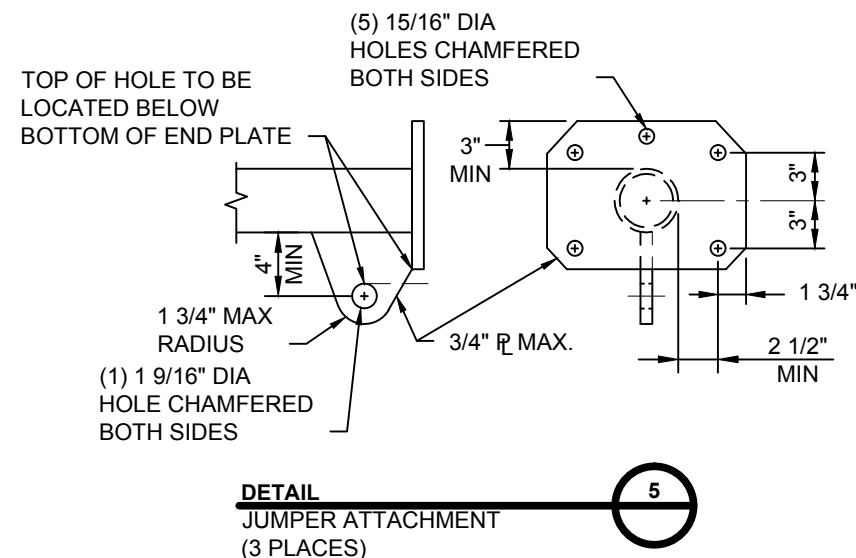
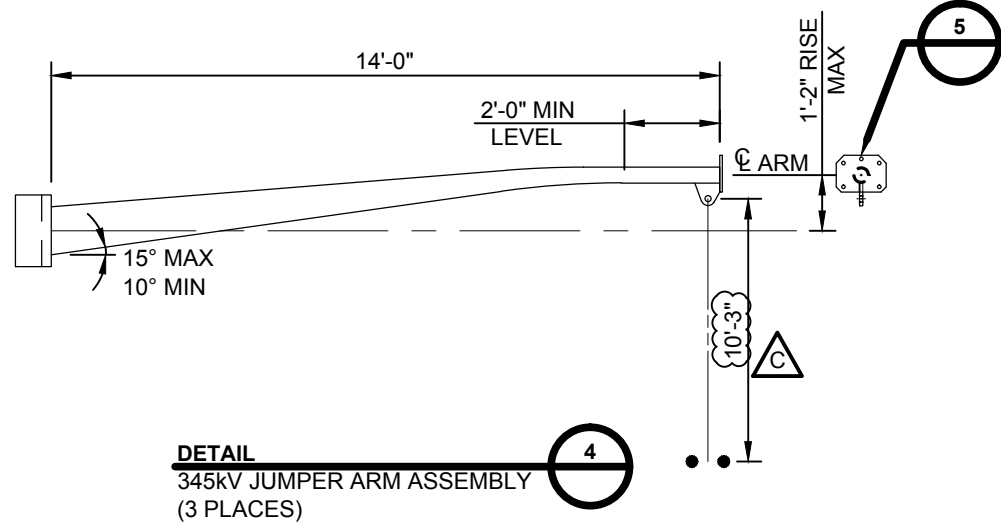
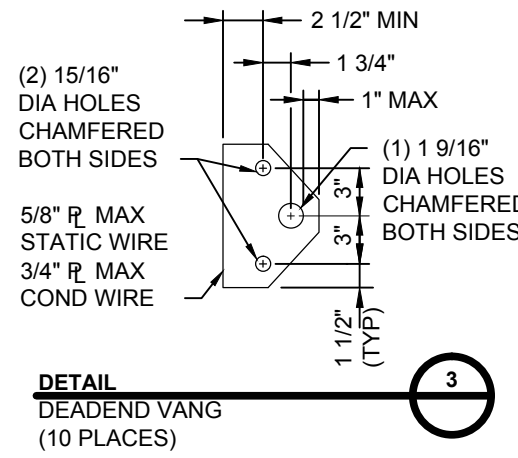
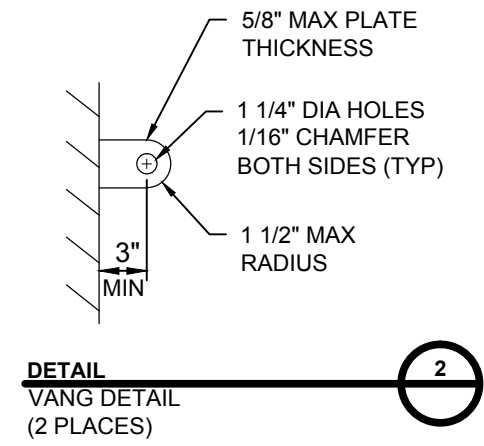
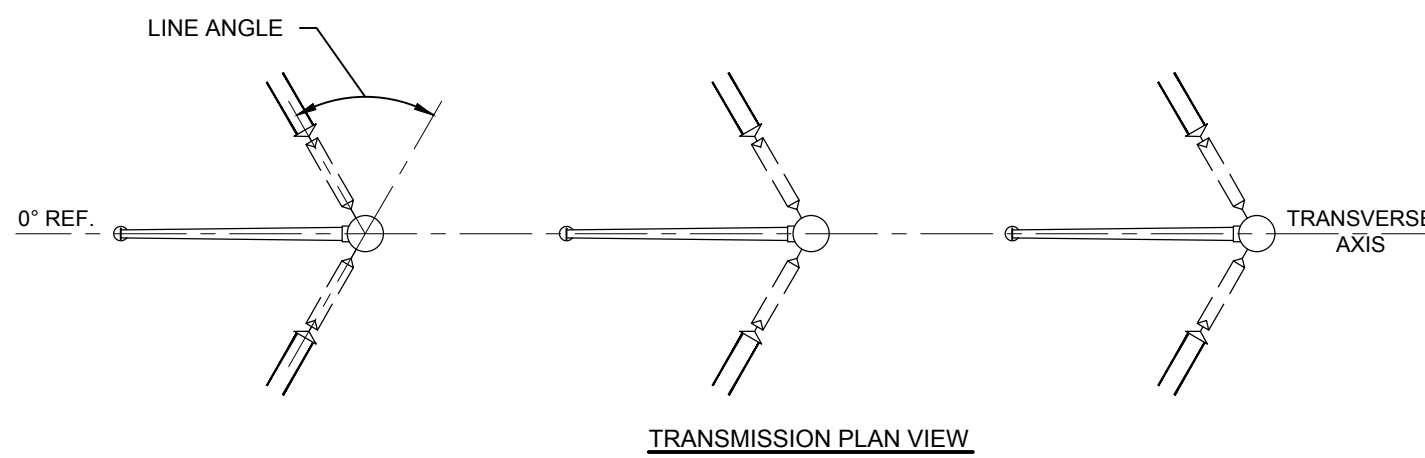
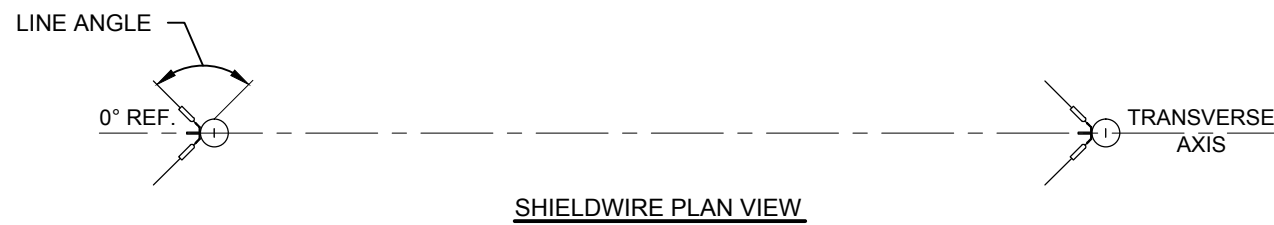
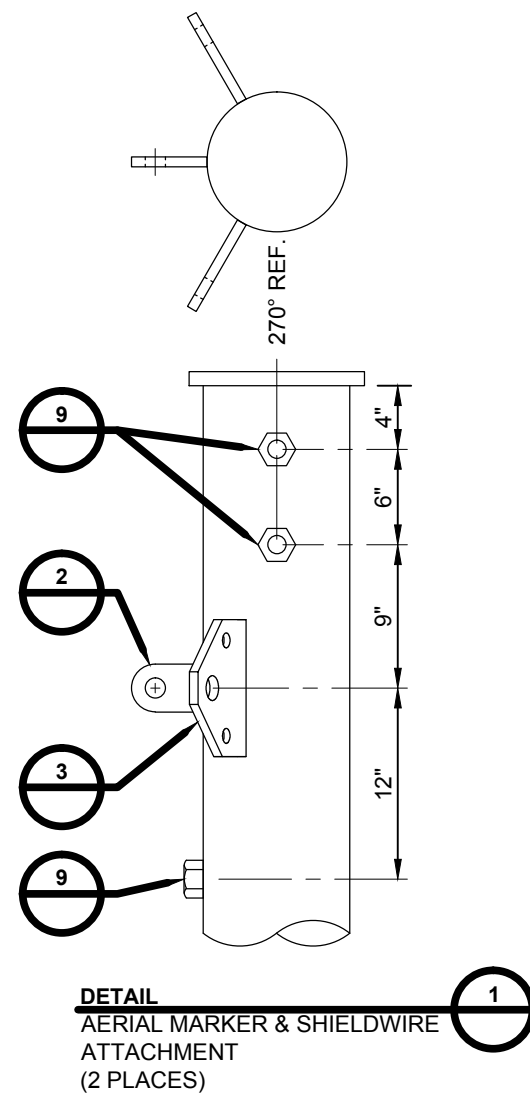
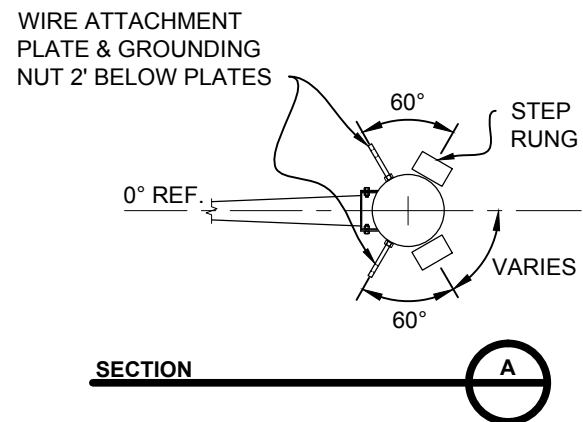


- NOTES:
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  - SNUB ANGLES SHALL BE LIMITED TO A 6° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTABLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTABLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

CONTRACT SERVICES								THE NORTHERN PASS		C	
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR				DRAWN	BLH
										ENGINEER	CET
										CHECKED	TAB
										APPROVED	
										DATE	5/1/15
C	MISC. REVISIONS		5/27/15	MSP				345kV AC HEAVY DEADEND 65-90° 30-SCHSP-HDW-090 LOAD & DESIGN DRAWING			
B	MISC. REVISIONS		5/8/15	BLH							
A	RELEASE FOR RFP BID		5/1/15	BLH				SCALE	FILE: TSP-09.DWG	DRAWING NO.	
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PRELIMINARY - NOT  
FOR CONSTRUCTION

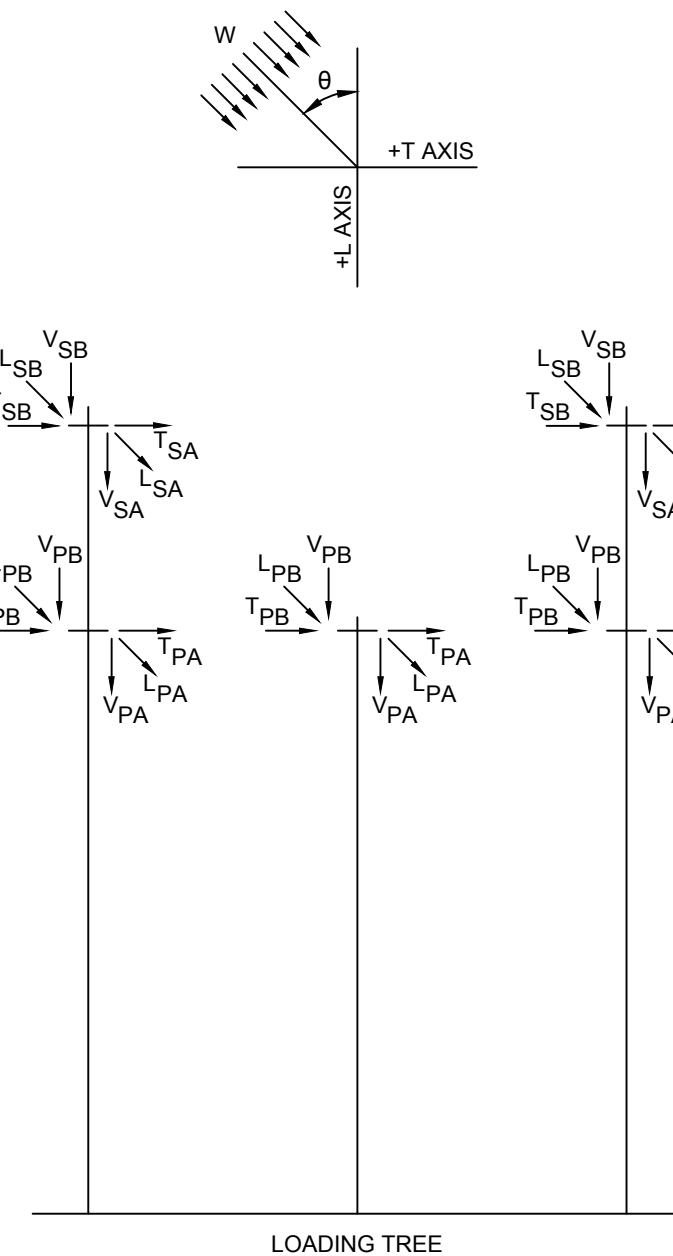




STRUCTURE NAME: 30-SCHSP-HDW-140  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 225 WIND SPAN BACK (FT): 225  
WEIGHT SPAN AHEAD (FT): 350 WEIGHT SPAN BACK (FT): 350  
LINE ANGLE: 130-140 DEGREES

LOADING CASE						DESIGN LOADS															
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K		
1	NESC 250B	0.00	0.50	39.53	0.64	9.33	4.07	0.64	9.33	-4.07	5.36	39.69	17.43	5.36	39.69	-17.43	10.00	90.00	1.50		
2	NESC 250C	60.00	0.00	100.00	0.21	4.48	1.91	0.21	4.48	-1.91	2.03	23.16	9.77	2.03	23.16	-9.77	29.00	90.00	1.00		
3	NESC 250D	15.00	1.00	39.53	0.86	7.72	3.39	0.86	7.72	-3.39	4.88	30.15	13.32	4.88	30.15	-13.32	4.00	90.00	1.00		
4	NU EXTREME ICE	15.00	1.25	39.53	1.16	9.55	4.19	1.16	9.55	-4.19	5.70	35.35	15.63	5.70	35.35	-15.63	4.00	90.00	1.00		
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.43	5.59	2.47	0.43	5.59	-2.47	3.58	23.86	10.56	3.58	23.86	-10.56	4.00	90.00	1.00		
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.43	5.28	2.32	0.43	5.28	-2.32	3.58	21.80	9.64	3.58	21.80	-9.64	4.00	90.00	1.00		
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.43	5.28	2.32	0.43	0.11	0.00	3.58	21.80	9.64	3.58	0.38	0.00	4.00	90.00	1.00		
8	CONSTRUCTION	30.00	0.00	29.97	3.48	0.92	0.12	1.66	4.94	-2.21	13.55	4.21	0.51	4.39	22.27	-9.93	3.45	90.00	1.50		
9	DEFLECTION	60.00	0.00	0.00	0.21	2.78	1.25	0.21	2.78	-1.25	2.03	12.53	5.64	2.03	12.53	-5.64	0.00	90.00	1.00		
10	MAINTENANCE	60.00	0.00	0.00	2.21	5.56	2.50	2.21	5.56	-2.50	5.86	25.07	11.27	5.86	25.07	-11.27	0.00	90.00	2.00		
11	UPLIFT	-20.00	0.00	0.00	0.21	4.16	1.87	0.21	4.16	-1.87	2.03	19.44	8.74	2.03	19.44	-8.74	0.00	90.00	1.00		

- REFERENCES:
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I

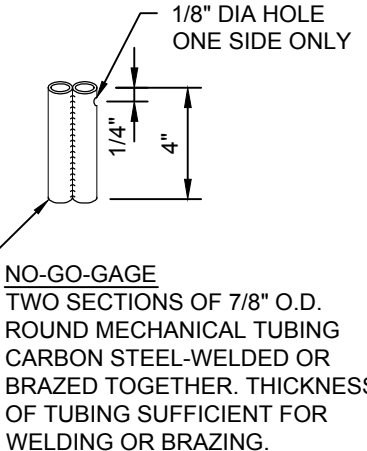
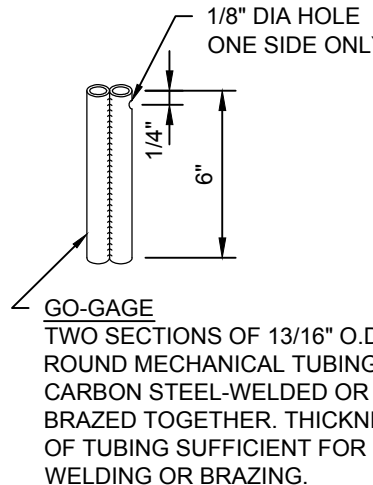
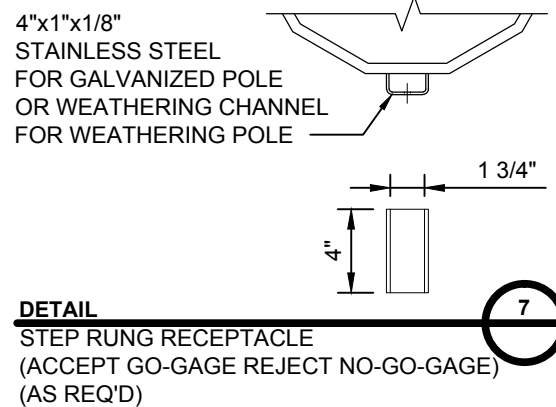
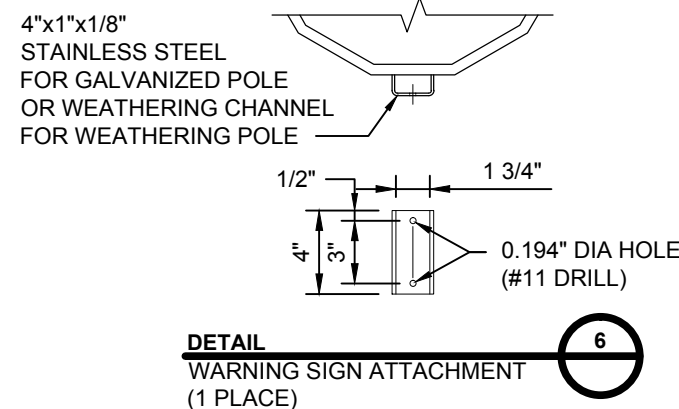
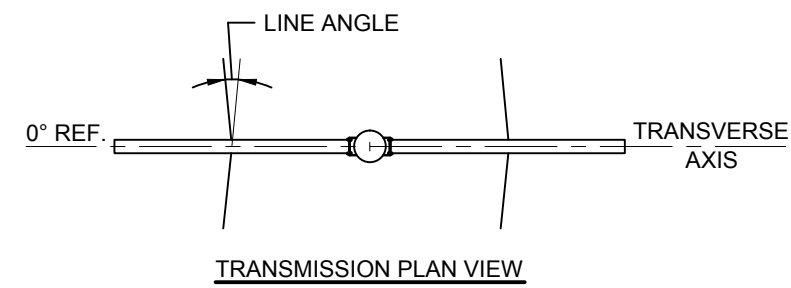
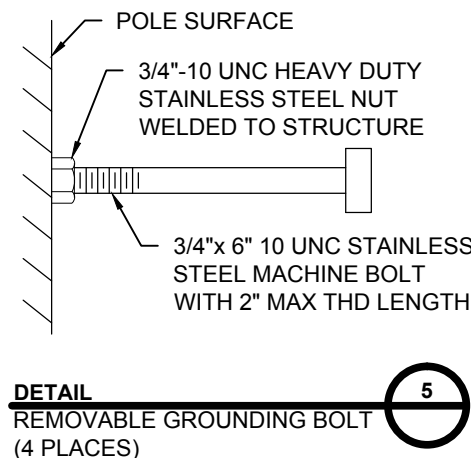
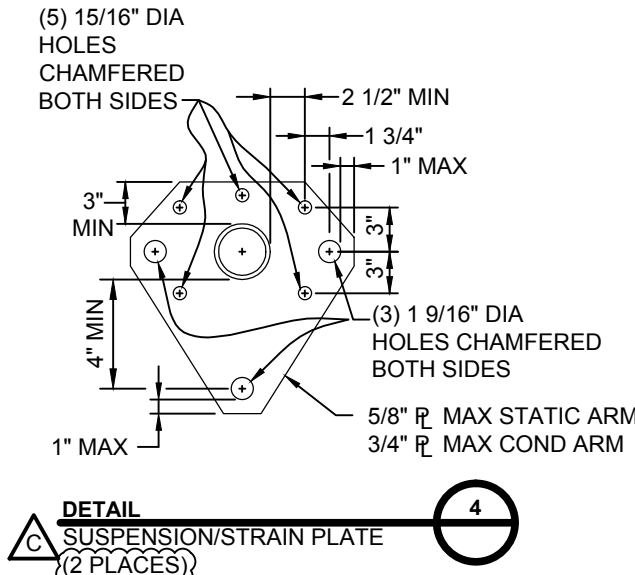
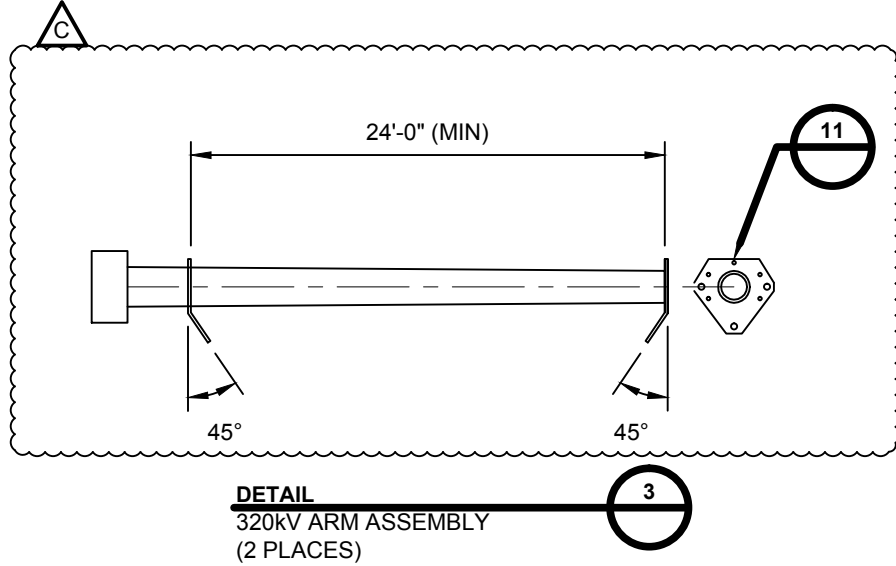
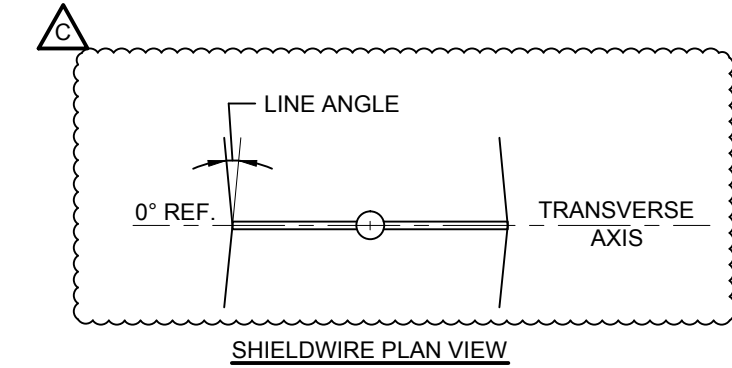
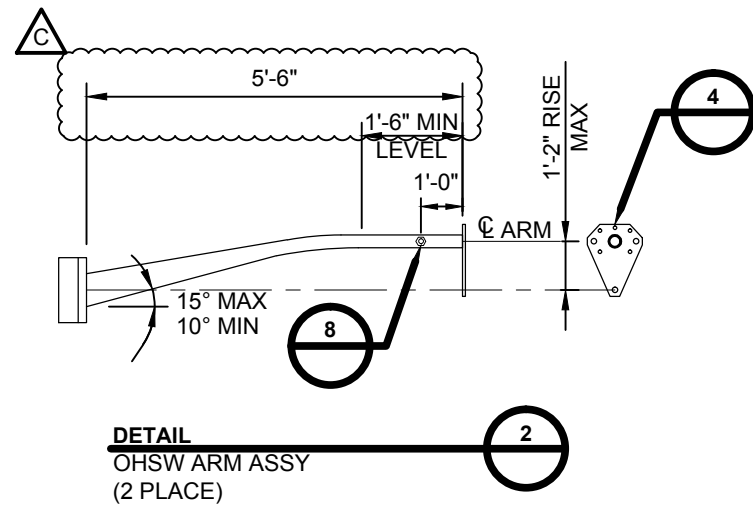
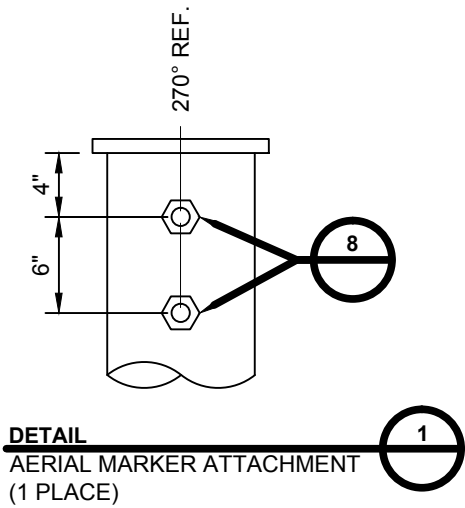
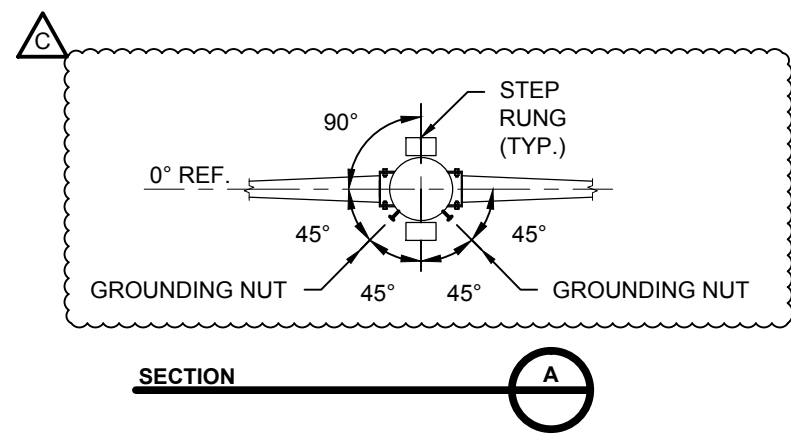


- NOTES:
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  15. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  16. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  17. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  18. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

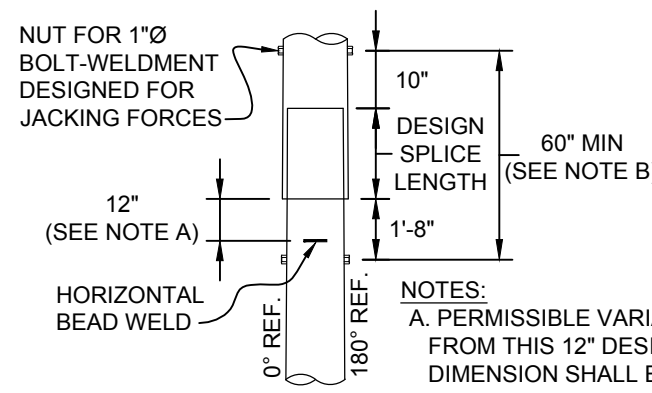
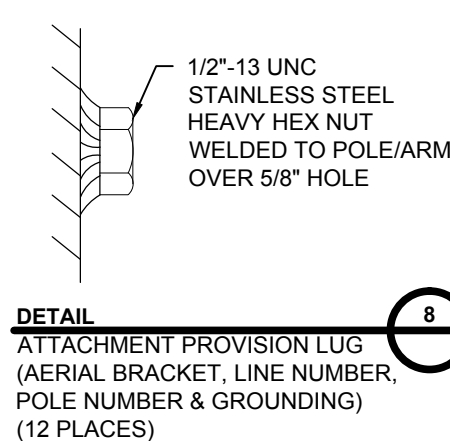
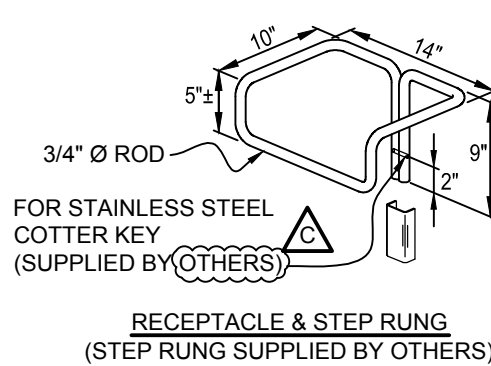
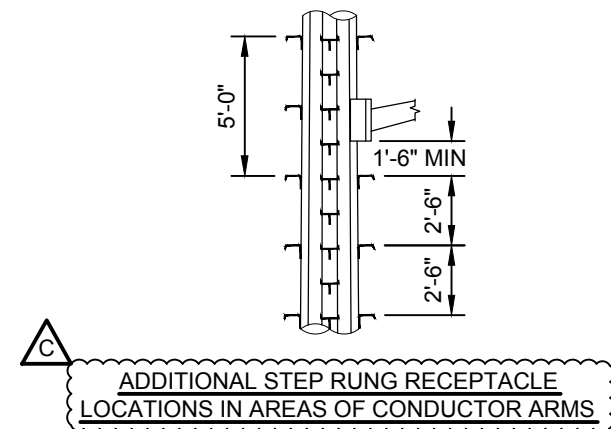
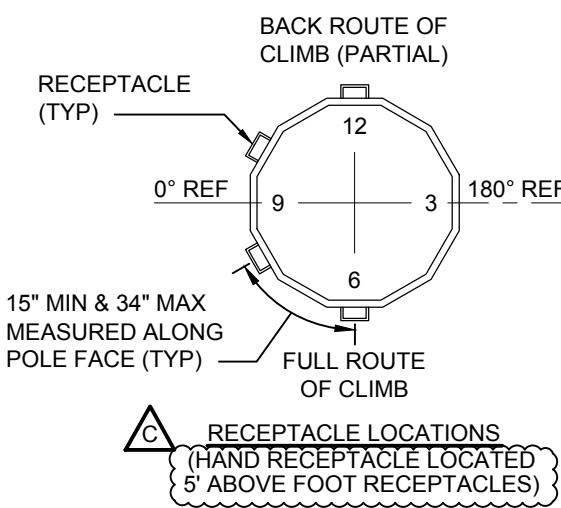
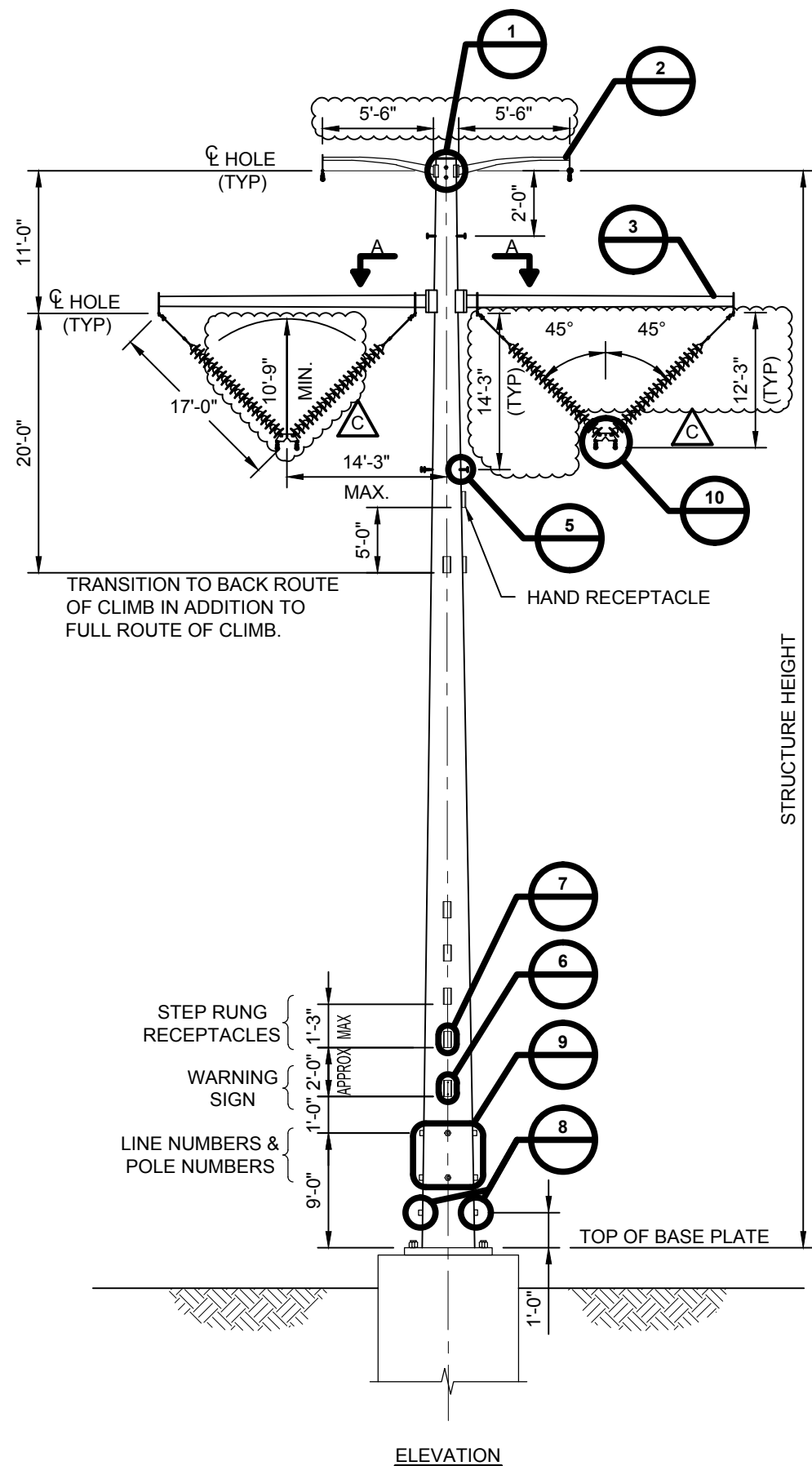
CONTRACT SERVICES							THE NORTHERN PASS		C	
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR			DRAWN	BLH
							345kV AC HEAVY DEADEND 130-140° 30-SCHSP-HDW-140 LOAD & DESIGN DRAWING		ENGINEER	CET
									CHECKED	TAB
									APPROVED	
									DATE	5/1/15
C	MISC. REVISIONS		5/27/15	MSP			SCALE: NTS		DRAWING NO. TSP-10-001	
B	MISC. REVISIONS		5/8/15	BLH						
A	RELEASE FOR RFP BID		5/1/15	BLH			FILE: TSP-10.DWG			
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	IMAGE:			

PRELIMINARY - NOT  
FOR CONSTRUCTION



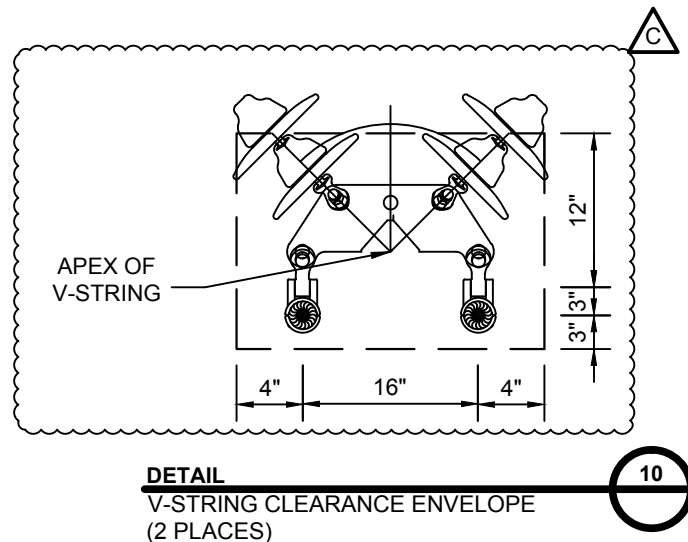
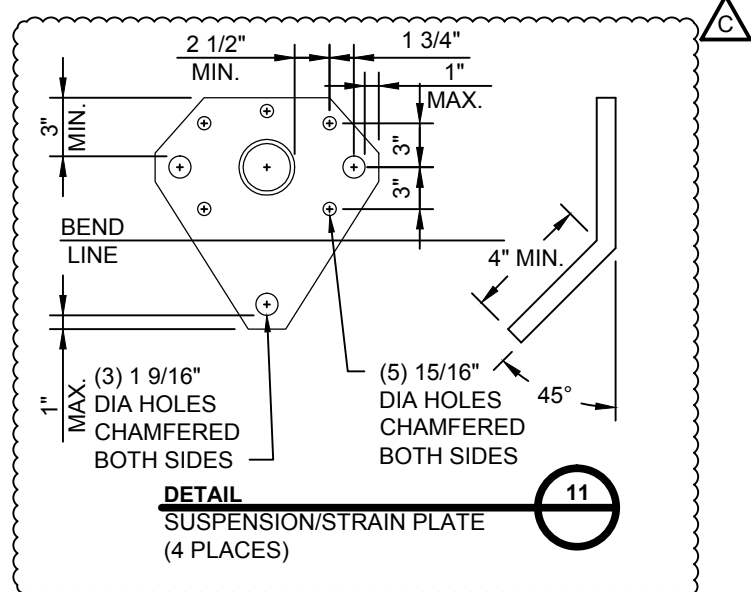
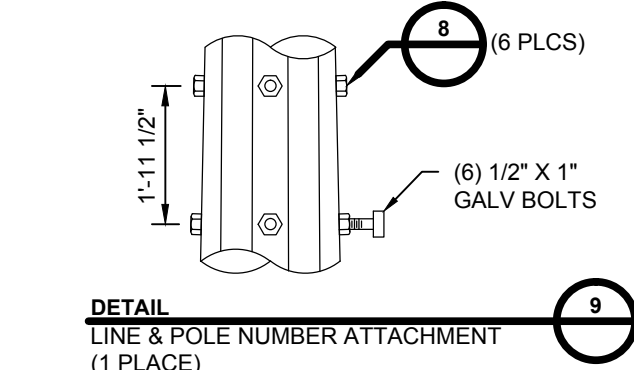


STEP RUNG RECEPTACLE GAGES



NOTES:  
A. PERMISSIBLE VARIATION FROM THIS 12" DESIGN DIMENSION SHALL BE INDICATED IN FINAL DESIGN AND ERECTION DRAWING.  
B. THE 10" AND 1'-8" DIMENSIONS MAY BE INCREASED TO ACHIEVE THIS 60" MIN.

SPLICE DETAILS JACKING NUT LOCATIONS

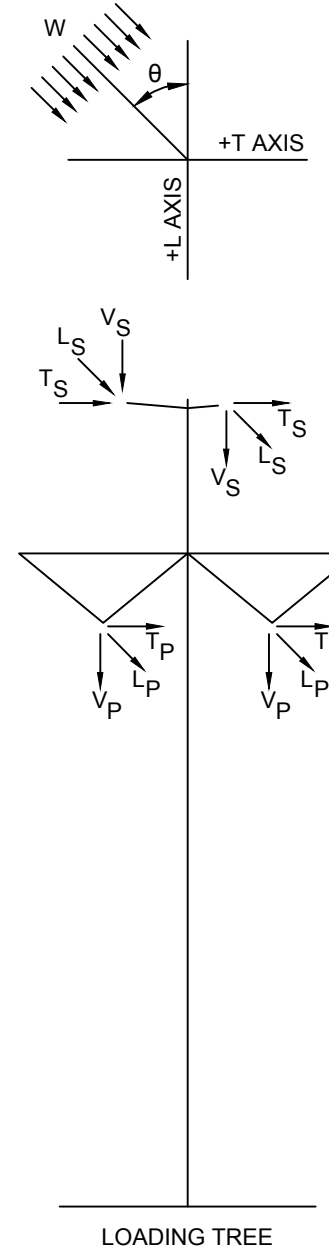


**PRELIMINARY - NOT FOR CONSTRUCTION**

STRUCTURE NAME: 32-SCHSP-LTW-002  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 550  
WEIGHT SPAN (FT): 850  
WEIGHT SPAN (FT): 850

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.45	1.03	0.00	13.54	5.30	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.43	0.75	0.00	5.61	5.98	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.03	0.74	0.00	12.70	3.28	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.62	1.06	0.00	17.43	4.15	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.96	0.48	0.00	9.02	2.65	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.96	0.47	0.00	9.02	2.49	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.96	0.37	5.50	9.02	1.51	24.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.58	0.27	0.27	23.61	2.17	2.27	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.43	0.10	0.00	5.61	0.83	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.66	0.21	0.00	13.01	1.66	0.00	0.00	90.00	2.00

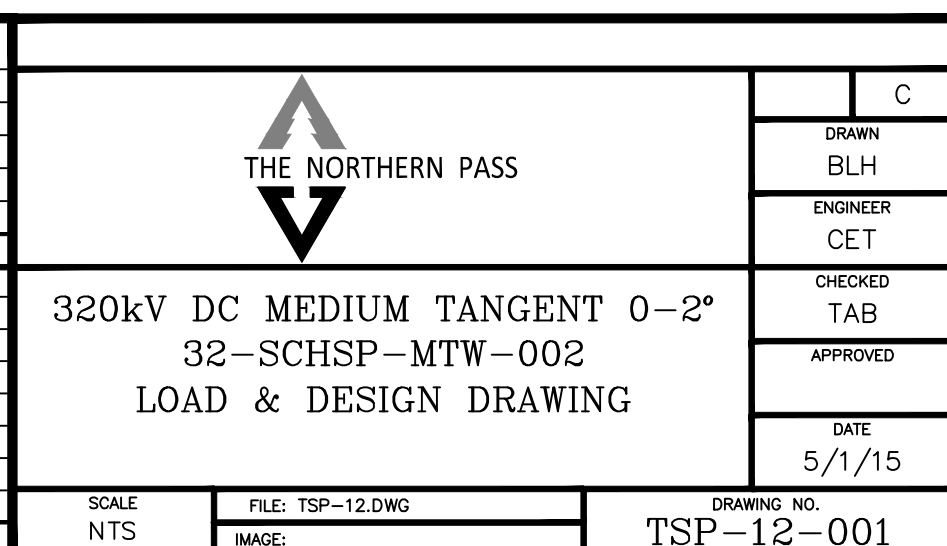
- REFERENCES:**
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
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  - SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 60°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
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  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD TO DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

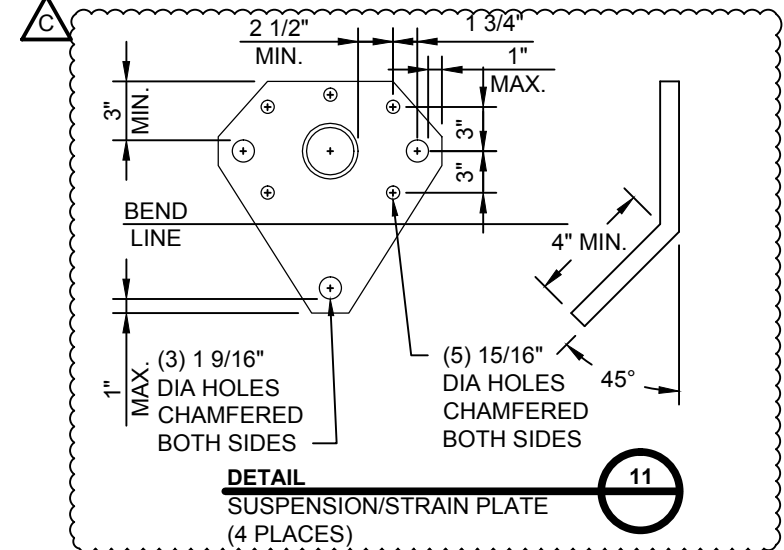
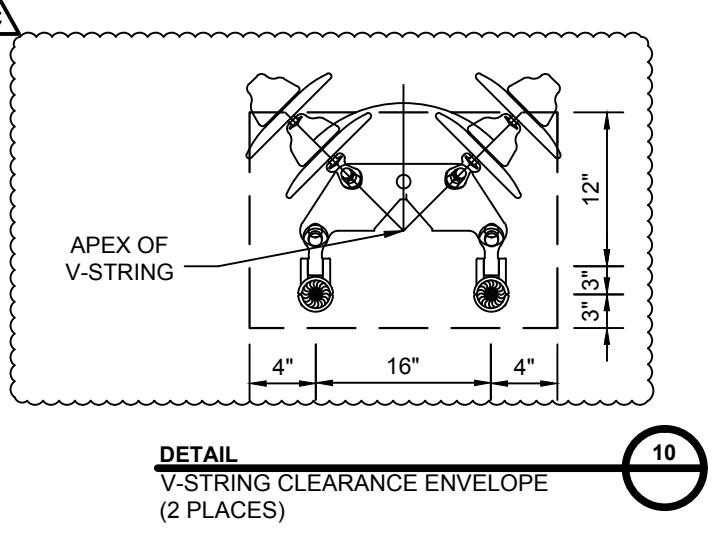
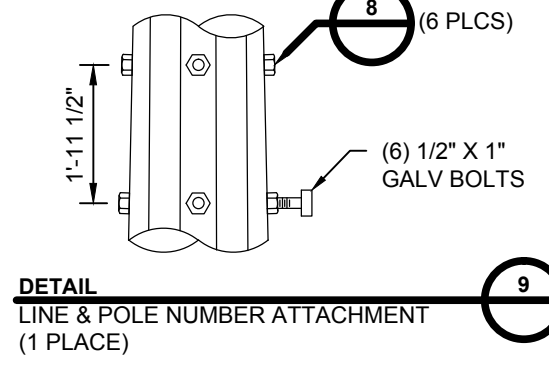
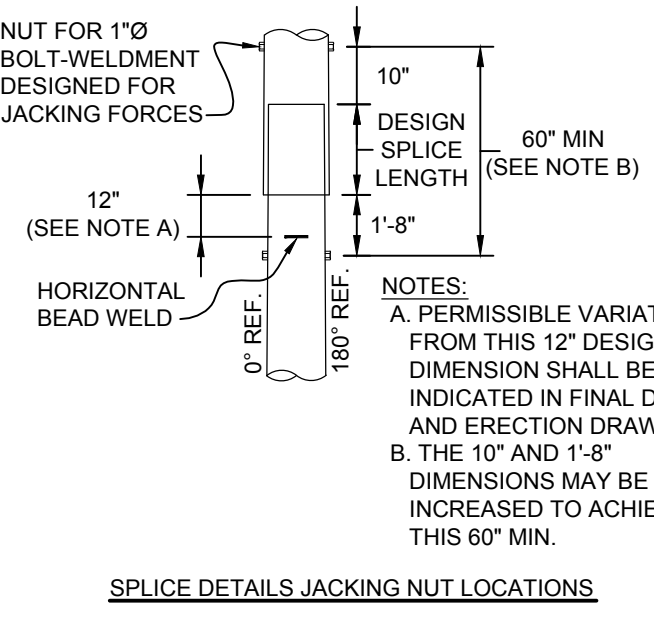
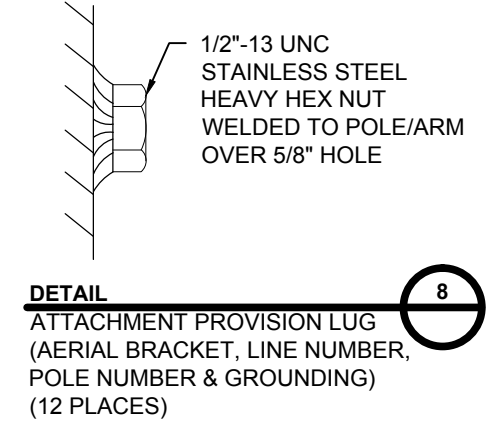
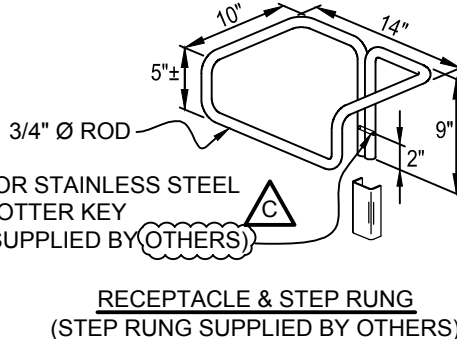
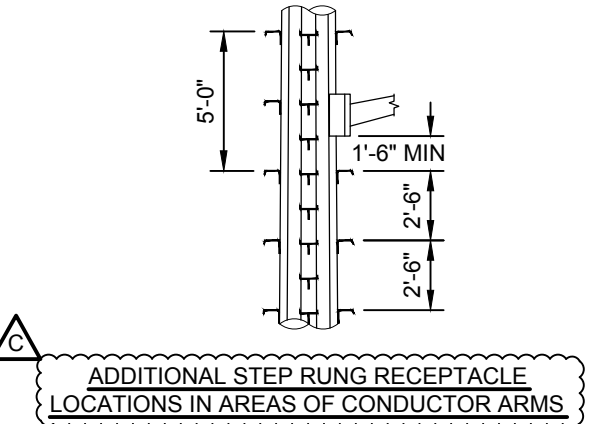
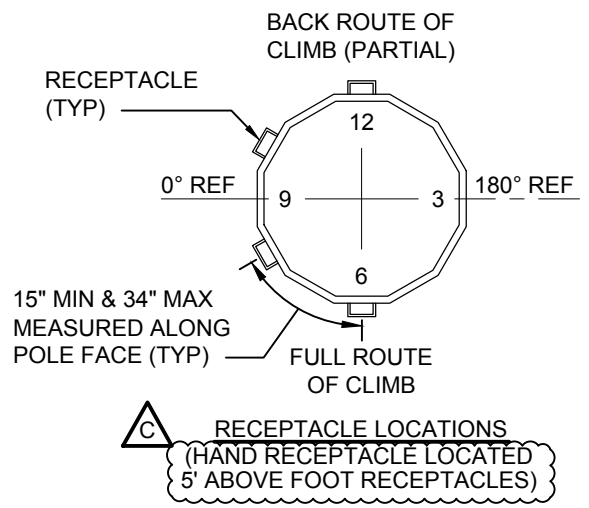
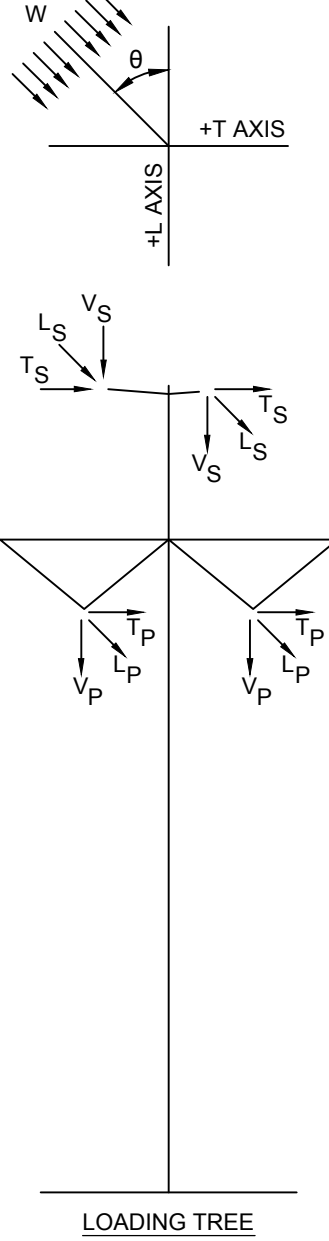
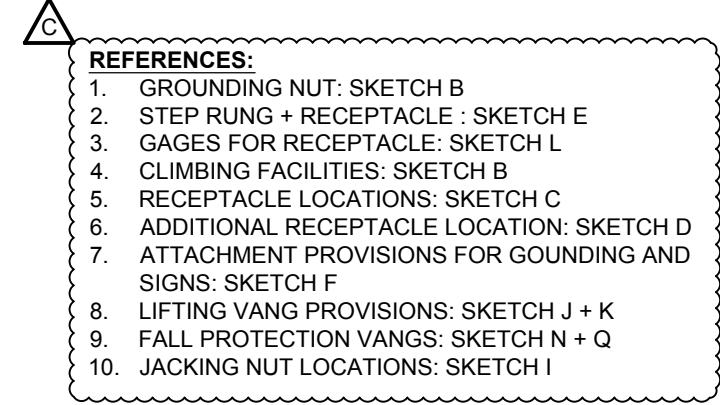
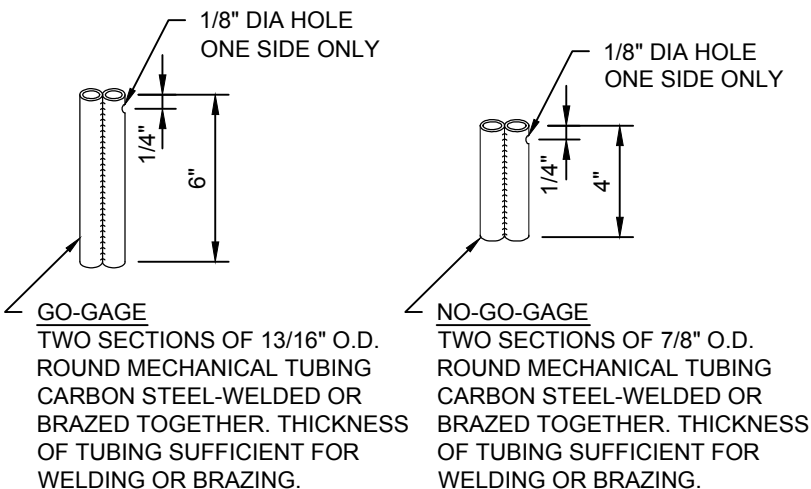
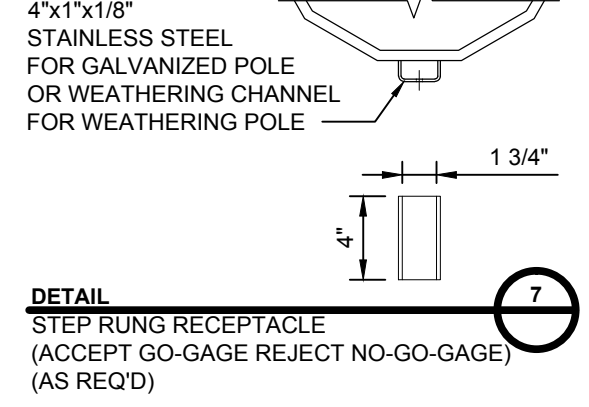
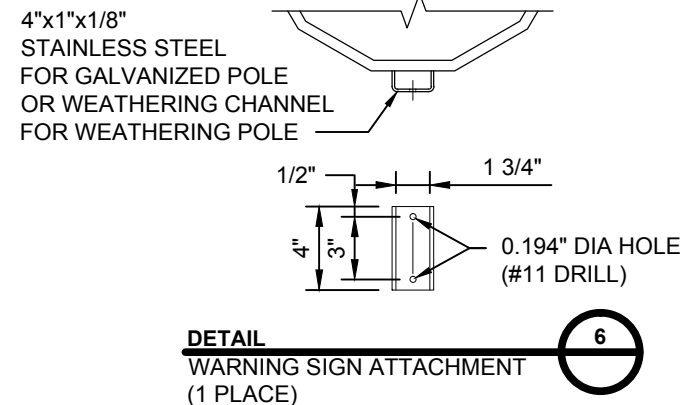
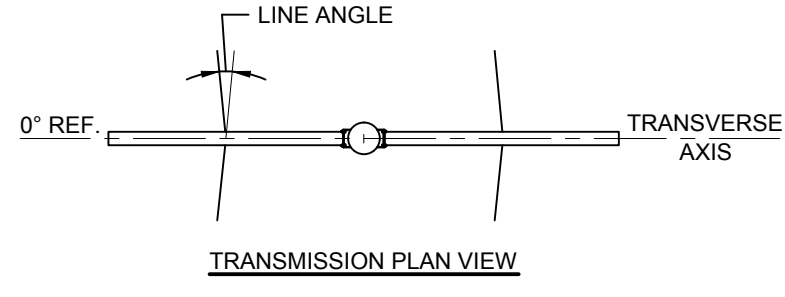
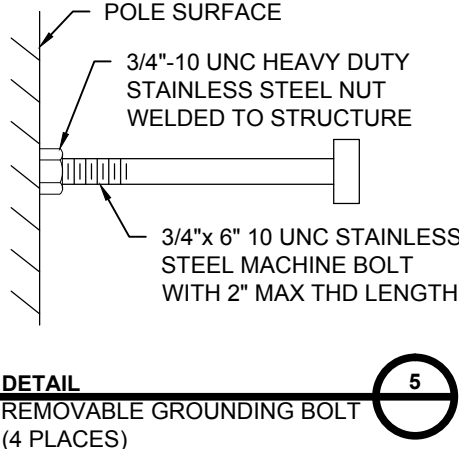
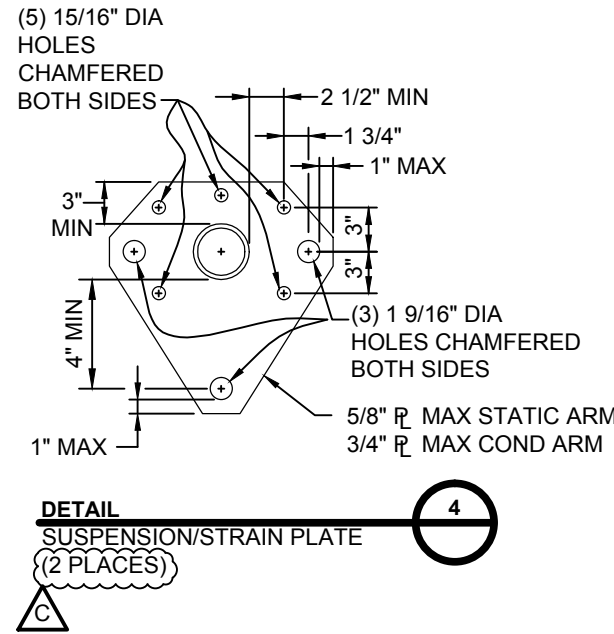
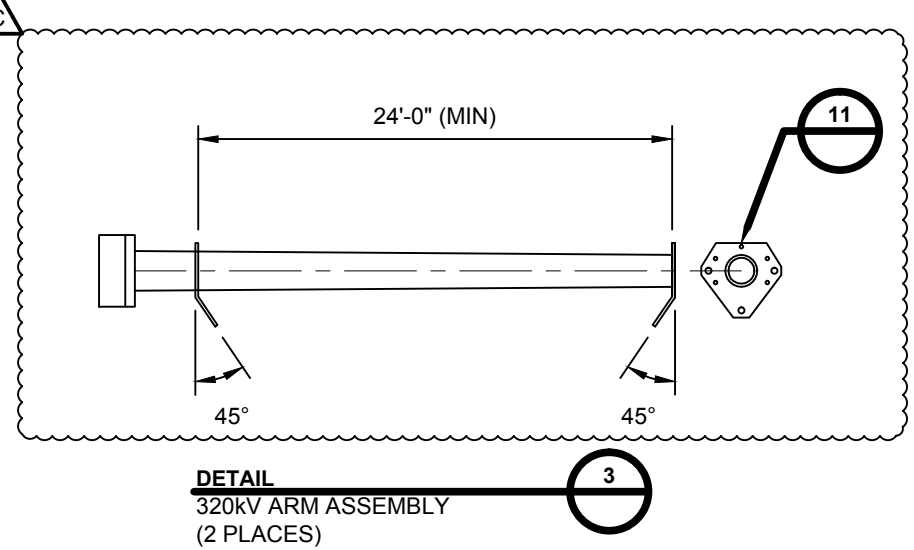
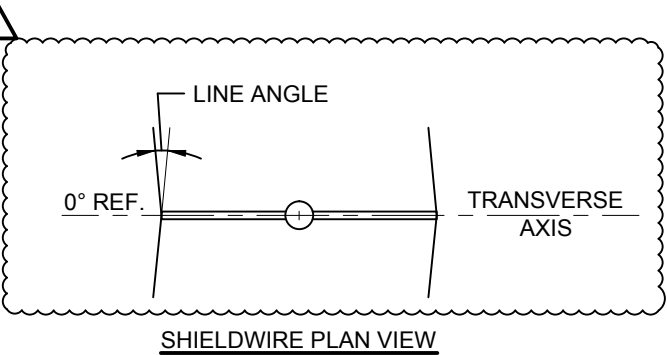
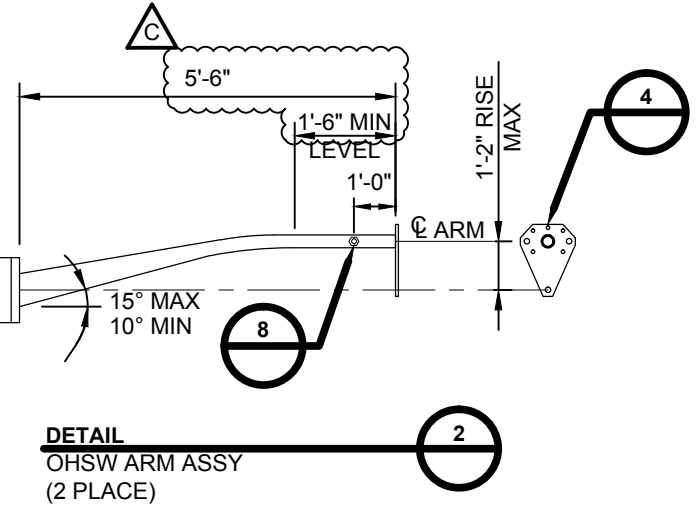
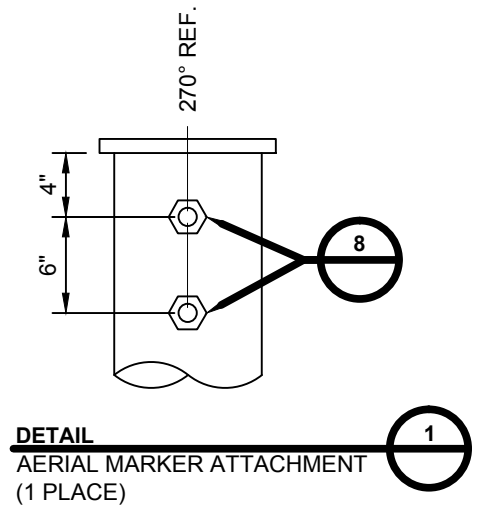
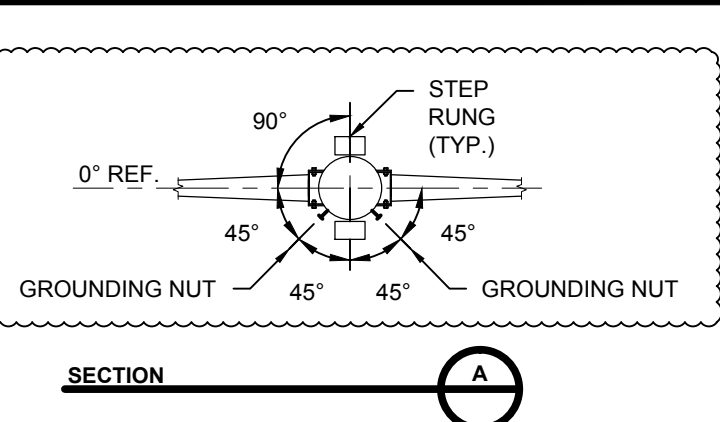
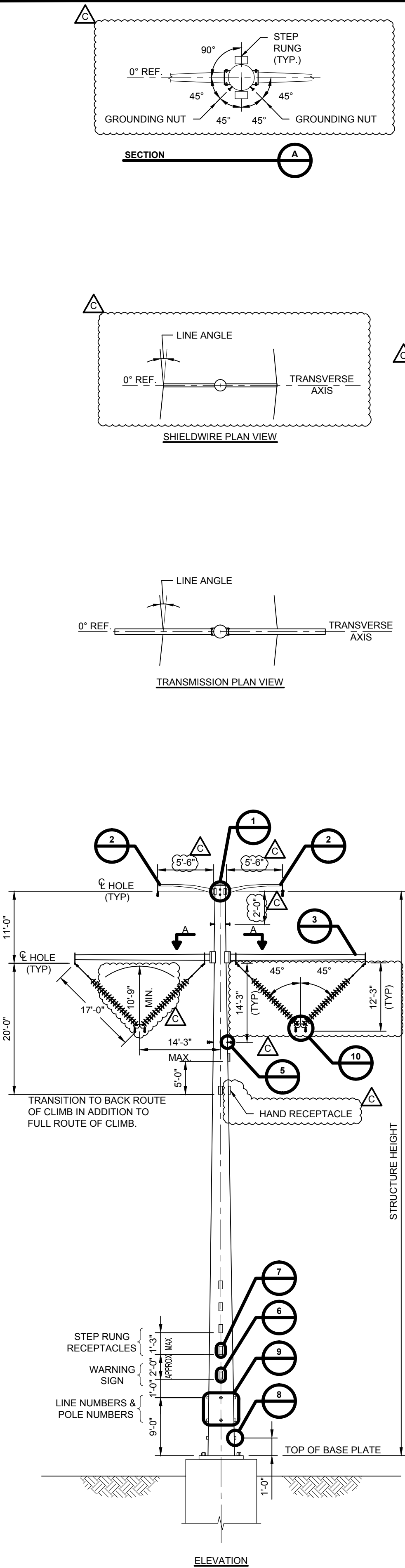
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**PRELIMINARY - NOT  
FOR CONSTRUCTION**





- NOTES:**
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25°.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

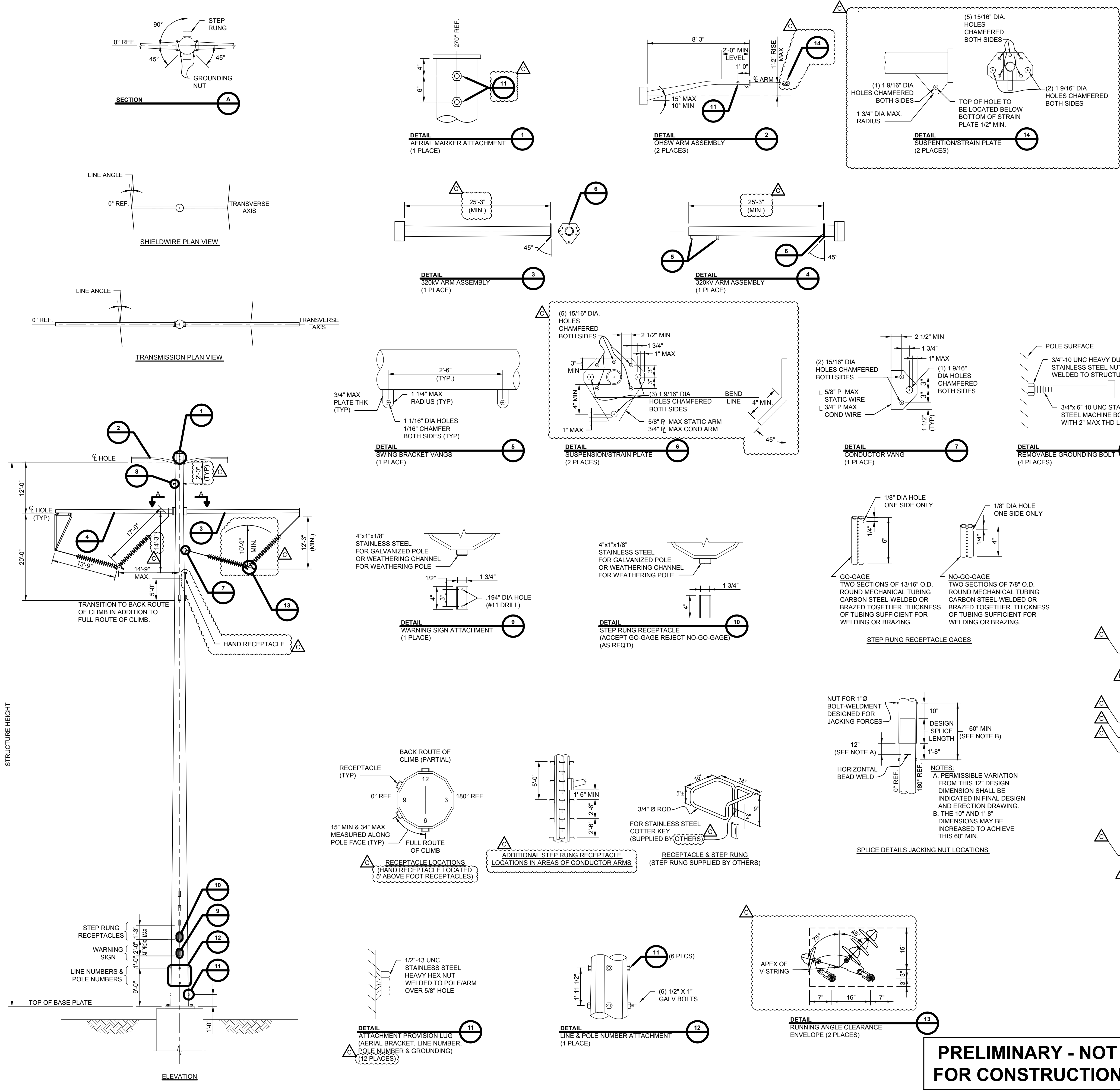
STRUCTURE NAME: 32-SCHSP-HTW-002  
 320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
 OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
 WIND SPAN (FT): 950  
 WEIGHT SPAN (FT): 1850  
 LINE ANGLE: 0 - 2 DEGREES

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	3.06	1.53	0.00	26.46	7.28	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.88	1.19	0.00	11.15	9.36	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	4.35	1.07	0.00	25.63	4.34	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	7.81	1.53	0.00	35.93	5.48	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	2.04	0.68	0.00	17.64	3.44	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	2.04	0.67	0.00	17.64	3.28	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	2.04	0.57	5.50	17.64	2.58	40.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.25	0.33	0.27	31.91	2.63	2.27	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.88	0.10	0.00	11.15	0.83	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	3.56	0.21	0.00	24.09	1.66	0.00	0.00	90.00	2.00

**PRELIMINARY - NOT FOR CONSTRUCTION**

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	<p>320kV DC HEAVY TANGENT 0-2°                  32-SCHSP-HTW-002                  LOAD &amp; DESIGN DRAWING</p>	C DRAWN BLH ENGINEER CET CHECKED TAB APPROVED DATE 5/1/15
	C	MISC. REVISIONS		5/27/15	KAK				
	B	MISC. REVISIONS		5/8/15	BLH				
	A	RELEASE FOR RFP BID		5/1/15	BLH				
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	SCALE NTS	FILE: TSP-13.DWG IMAGE:	DRAWING NO. TSP-13-001

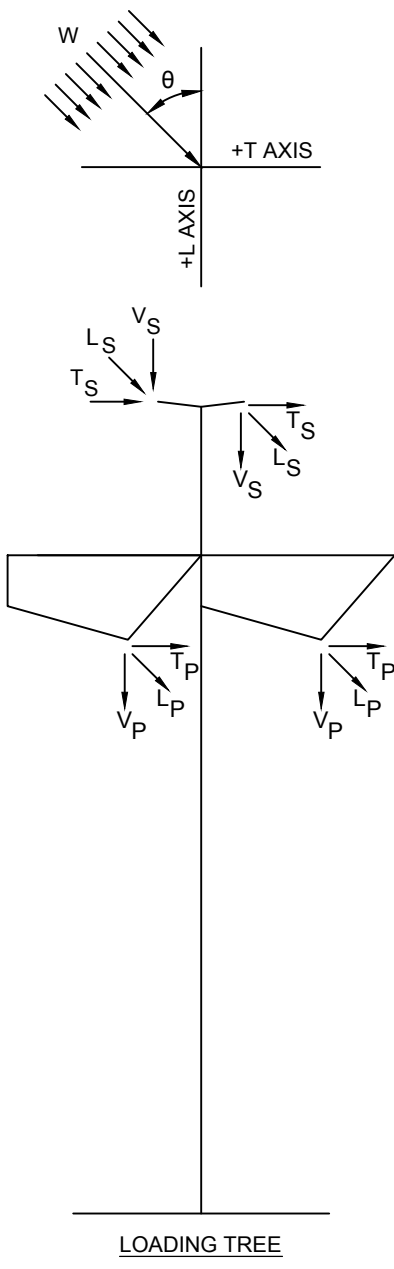




STRUCTURE NAME: 32-SCHSP-LAW-010  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 900  
WEIGHT SPAN (FT): 1250  
LINE ANGLE: 2 - 10 DEGREES

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	2.09	2.81	0.00	18.70	17.29	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.61	1.76	0.00	7.82	14.32	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.96	2.15	0.00	17.87	11.47	0.00	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	5.30	3.15	0.00	24.83	14.60	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.40	1.47	0.00	12.47	9.56	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.40	1.41	0.00	12.47	8.76	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.40	0.93	5.50	12.47	3.88	24.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.85	1.05	0.27	26.93	8.74	2.27	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.61	0.52	0.00	7.82	4.14	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	3.02	1.03	0.00	17.45	8.27	0.00	0.00	90.00	2.00

- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I



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  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 0.8 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
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  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
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    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
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  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 13.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
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  14. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  15. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD TO DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  16. 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE
  17. 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS
  18. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

**PRELIMINARY - NOT FOR CONSTRUCTION**

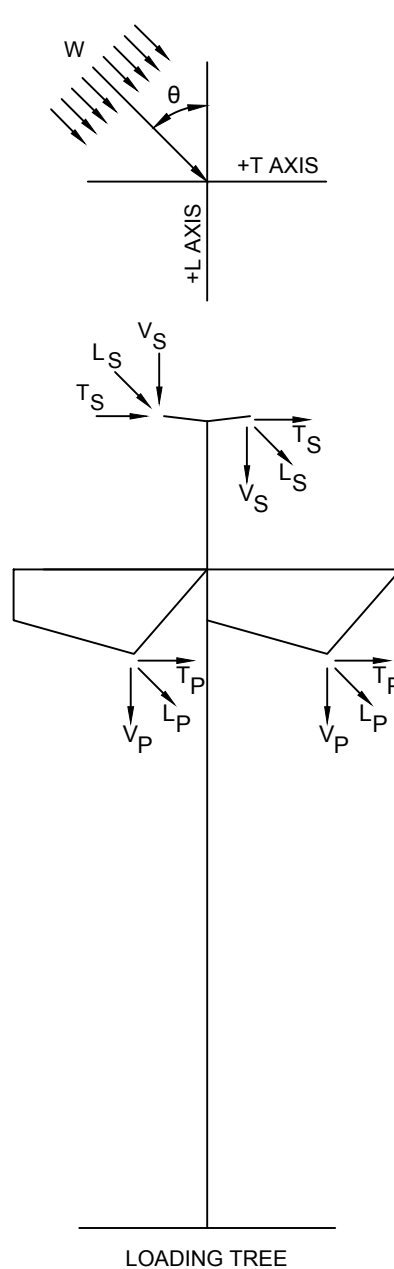
CONTRACT SERVICES						THE NORTHERN PASS				C	
										DRAWN	BLH
REV						320kv DC LIGHT ANGLE 2-10° 32-SCHSP-LAW-010 LOAD & DESIGN DRAWING				ENGINEER	
										CET	
C						SCALE: NTS				CHECKED	
										TAB	
B						FILE: TSP-14.DWG				APPROVED	
										DATE	
A						IMAGE:				5/1/15	
										DRAWING NO.	
DWG REV						TSP-14-001					





**REFERENCES:**

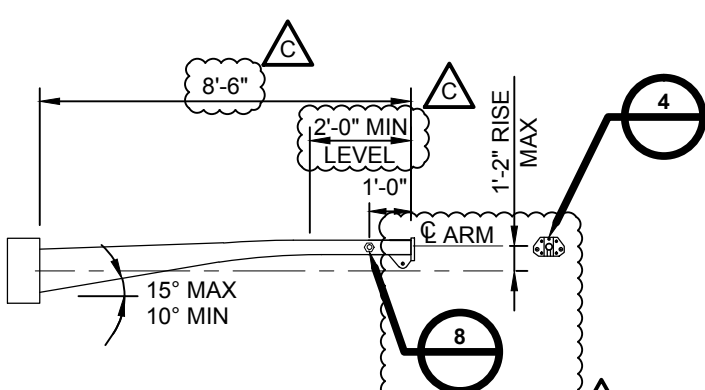
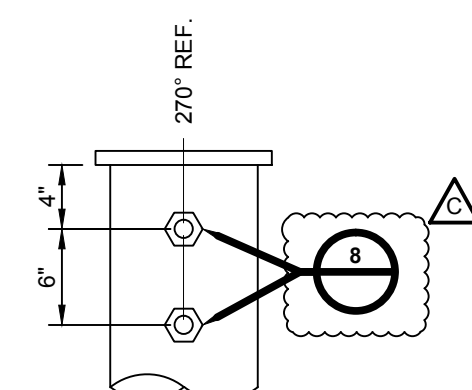
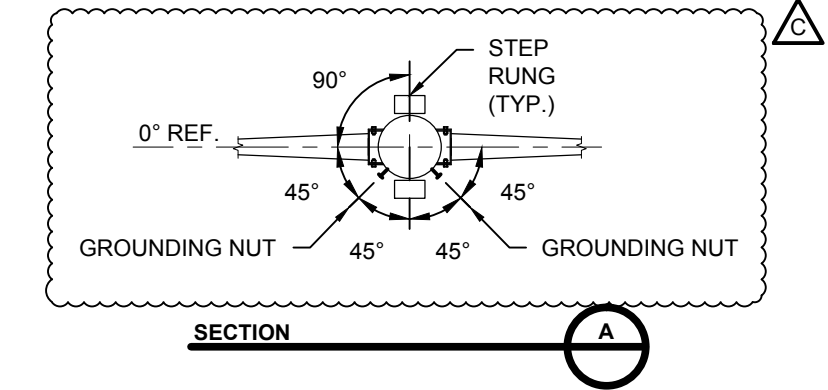
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2. STEP RUNG + RECEPTACLE : SKETCH E
3. GAGES FOR RECEPTACLE: SKETCH L
4. CLIMBING FACILITIES: SKETCH B
5. RECEPTACLE LOCATIONS: SKETCH C
6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
8. LIFTING VANG PROVISIONS: SKETCH J + K
9. FLYING PROTECTOR: SKETCH N + Q
10. JACKING NUT LOCATIONS: SKETCH I
11. JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
1. ALL INSTALLED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, L & R ARE IN DEGREES AND ARE IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE UNLESS OTHERWISE SPECIFIED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A (15) DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (25°).
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 3.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE LIFTING. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. **CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.)
  16. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  17. 5'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  18. 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  19. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

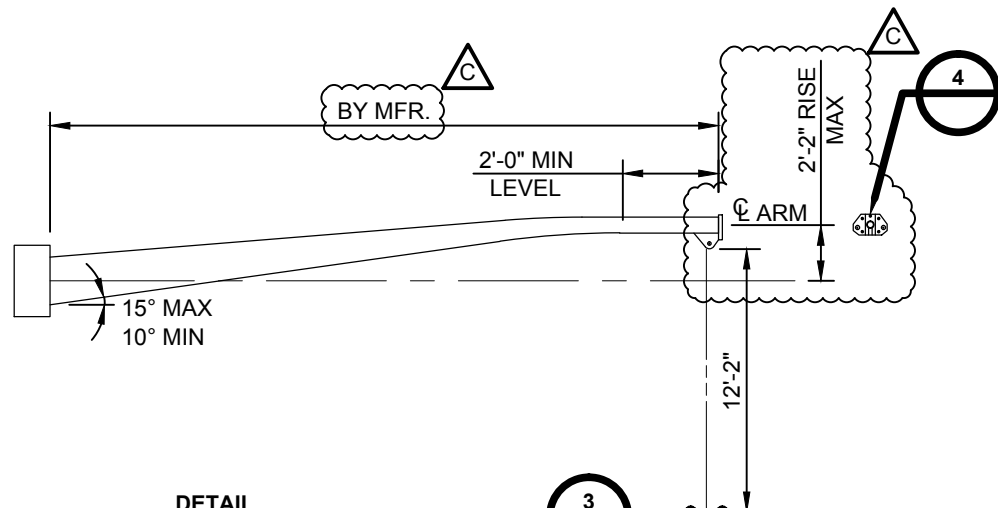
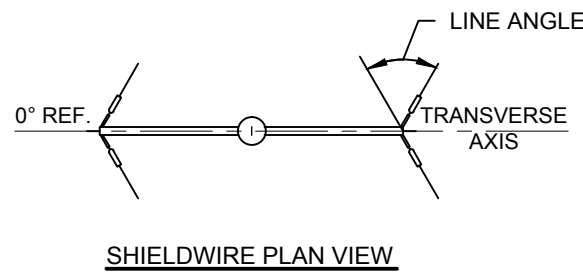
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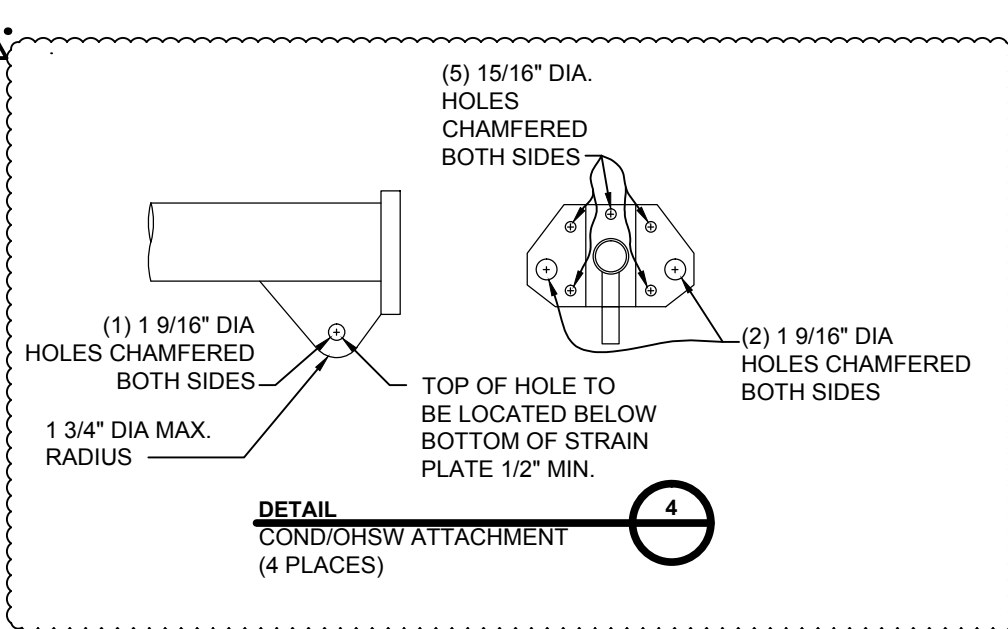


DETAIL  
AERIAL MARKER ATTACHMENT  
(1 PLACE)

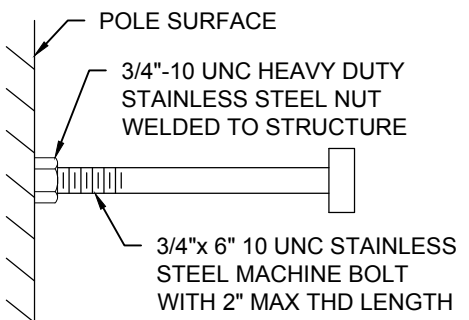
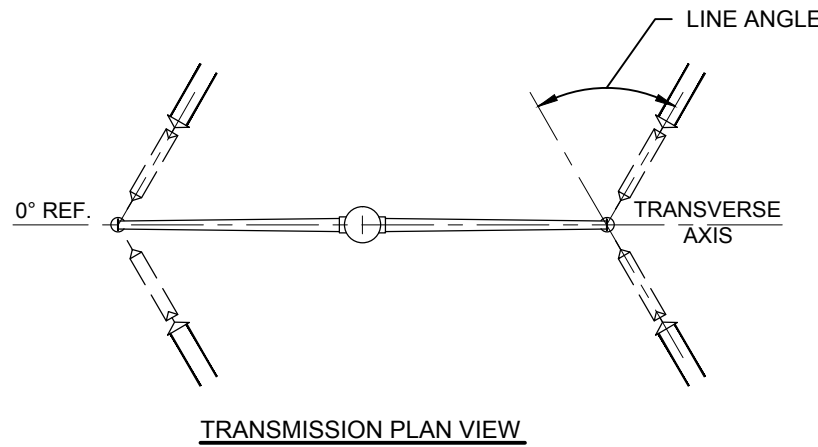
DETAIL  
OHSW ARM ASSEMBLY  
(2 PLACES)



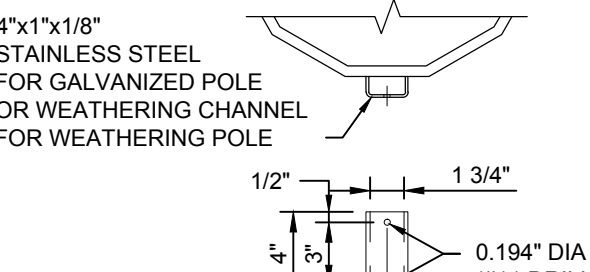
DETAIL  
320KV ARM ASSEMBLY  
(2 PLACES)



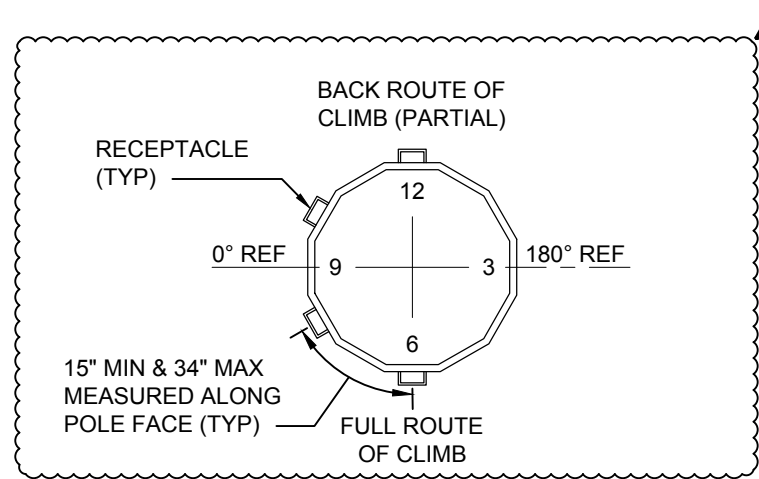
DETAIL  
COND/OHSW ATTACHMENT  
(4 PLACES)



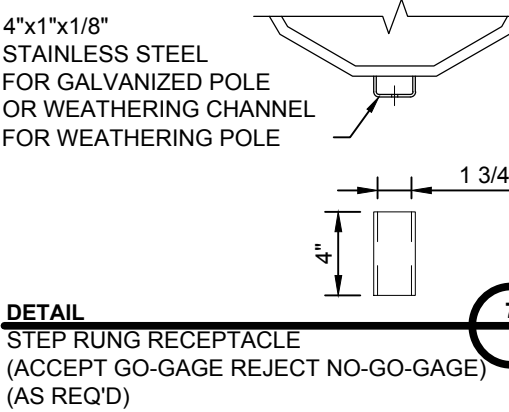
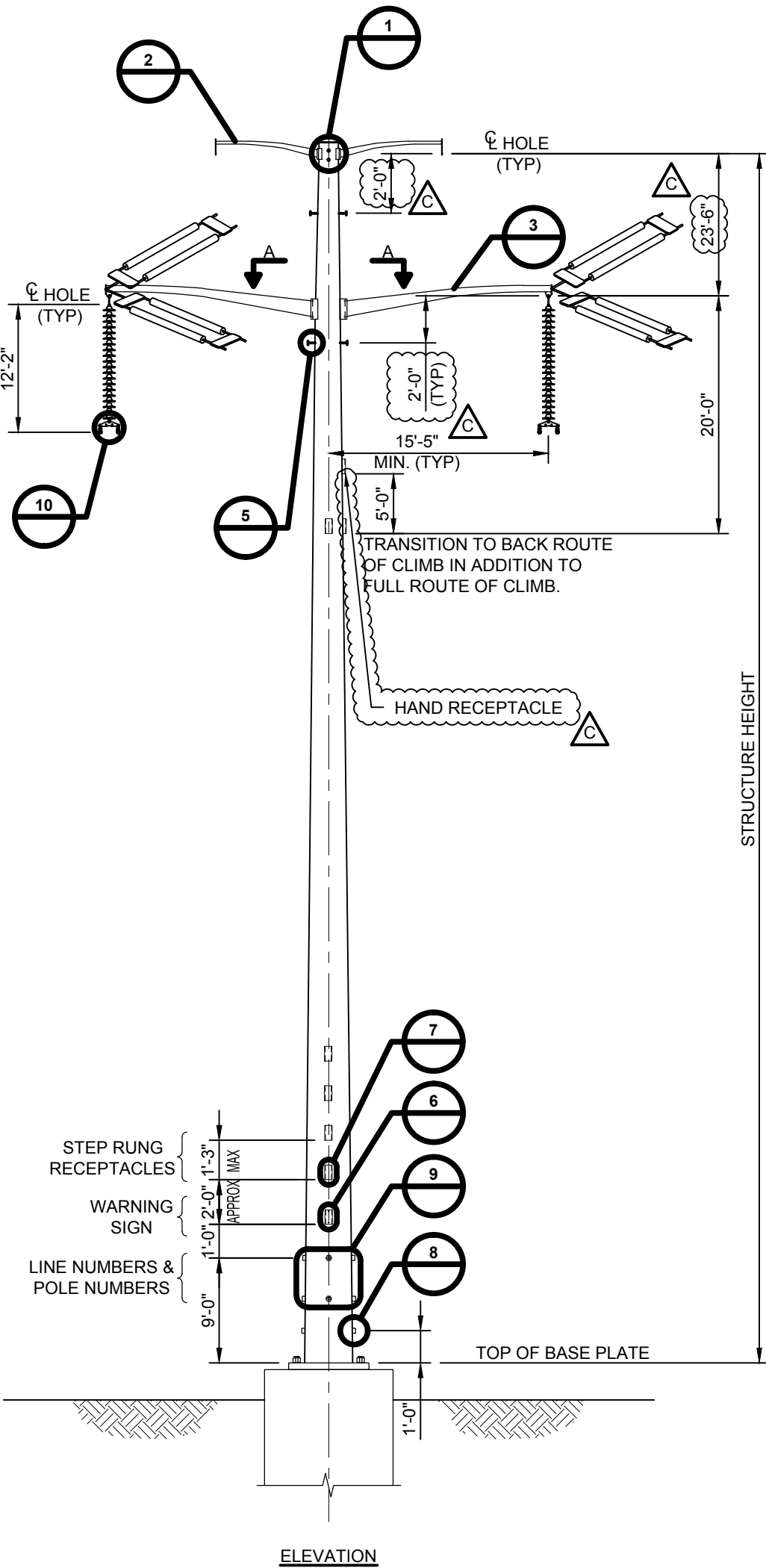
DETAIL  
REMOVABLE GROUNDING BOLT  
(4 PLACES)



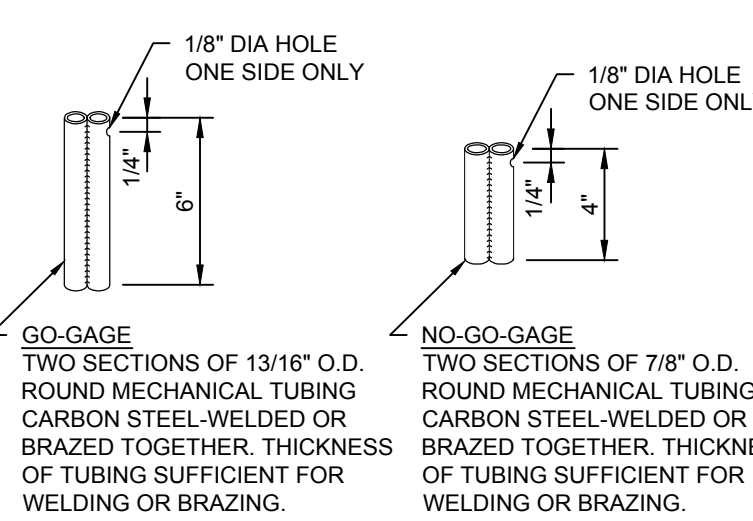
DETAIL  
WARNING SIGN ATTACHMENT  
(1 PLACE)



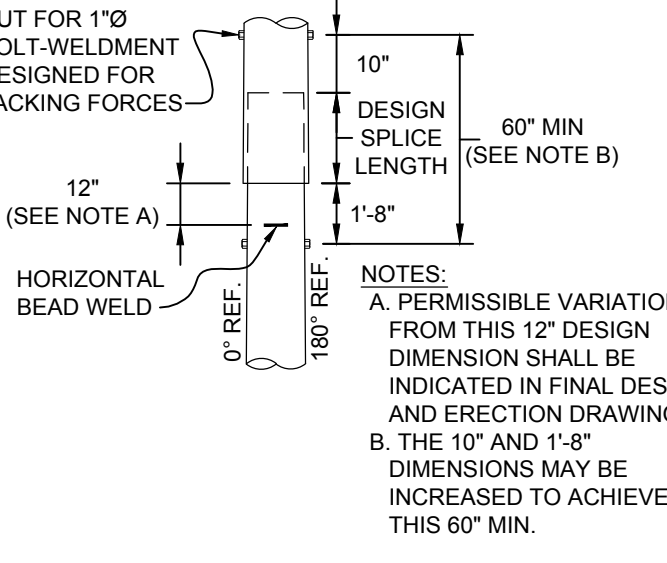
RECEPTACLE LOCATIONS  
(HAND RECEPTACLE LOCATED  
5' ABOVE FOOT RECEPTABLES)



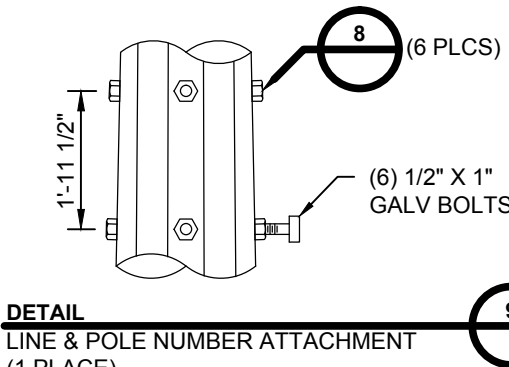
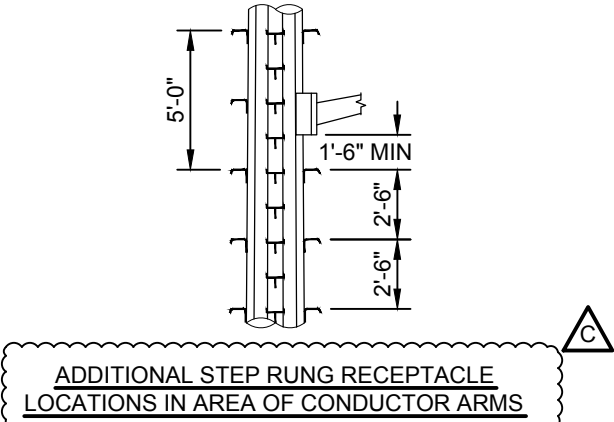
DETAIL  
STEP RUNG RECEPTACLE  
(ACCEPT GO-GAGE REJECT NO-GO-GAGE)  
(AS REQ'D)



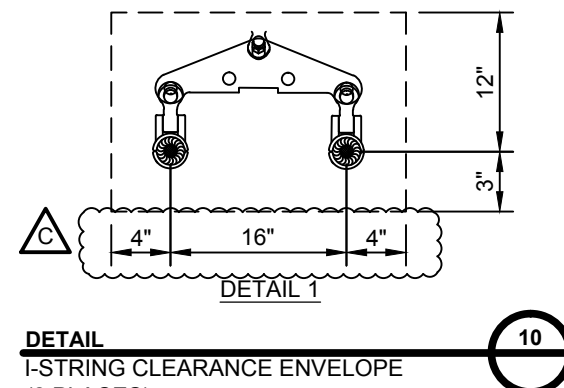
STEP RUNG RECEPTACLE GAGES



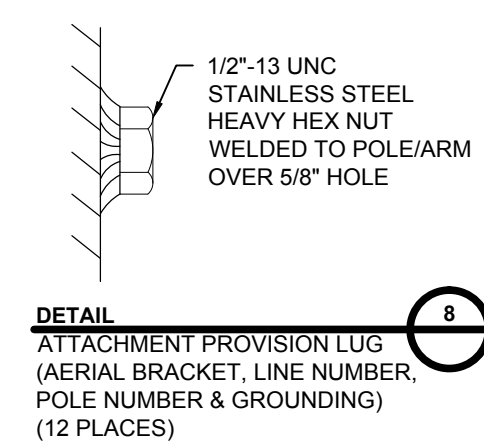
SPICE DETAILS, JACKING NUT LOCATIONS



DETAIL  
LINE & POLE NUMBER ATTACHMENT  
(1 PLACE)



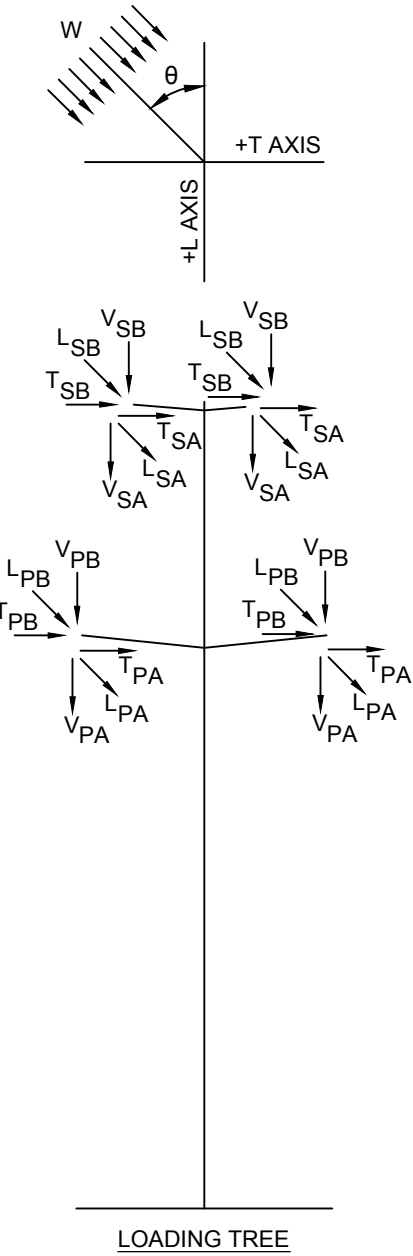
DETAIL  
T-STRING CLEARANCE ENVELOPE  
(2 PLACES)



DETAIL  
ATTACHMENT PROVISION LUG  
(AERIAL BRACKET, LINE NUMBER,  
POLE NUMBER & GROUNDING)  
(12 PLACES)

STRUCTURE NAME: 32-SCHSP-LDW-045  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 550 WIND SPAN BACK (FT): 550  
WEIGHT SPAN AHEAD (FT): 825 WEIGHT SPAN BACK (FT): 825  
INE ANGLE: 0 - 45 DEGREES

NO.	DESCRIPTION	LOADING CASE					DESIGN LOADS												
		TEMP (°F)	ICE (in)	WIND (mph)	VSA (lb)	TSA (lb)	LVA (lb)	VSB (lb)	TSB (lb)	LSB (lb)	VPA (lb)	TSA (lb)	LPA (lb)	VPB (lb)	TPB (lb)	LPB (lb)	W (lb/ft)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.41	4.37	9.62	1.41	4.37	-9.62	13.36	30.89	73.59	13.36	30.89	-73.59	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.42	2.32	4.51	0.42	2.32	-4.51	5.52	19.43	38.67	5.52	19.43	-38.67	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.97	3.53	8.01	1.97	3.53	-8.01	12.47	21.41	52.13	12.47	21.41	-52.13	4.00	90.00	1.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	5.25	12.04	3.51	5.25	-12.04	16.96	27.33	66.65	16.96	27.33	-66.65	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	2.51	5.83	0.94	2.51	-5.83	8.91	18.16	44.60	8.91	18.16	-44.60	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	2.38	-5.50	8.91	16.40	40.00	8.91	16.40	-40.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	2.38	5.50	0.94	2.38	0.00	8.91	16.40	40.00	8.91	1.09	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.52	0.27	1.98	2.08	-5.23	30.33	12.71	2.27	9.63	17.56	-44.25	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.42	1.13	2.96	0.42	1.13	-2.96	5.52	9.08	23.72	5.52	9.08	-23.72	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.64	2.26	5.92	2.64	2.26	-5.92	12.84	18.16	47.44	12.84	18.16	-47.44	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.42	1.70	4.43	0.42	1.70	-4.43	5.52	16.59	43.34	5.52	16.59	-43.34	0.00	90.00	1.00



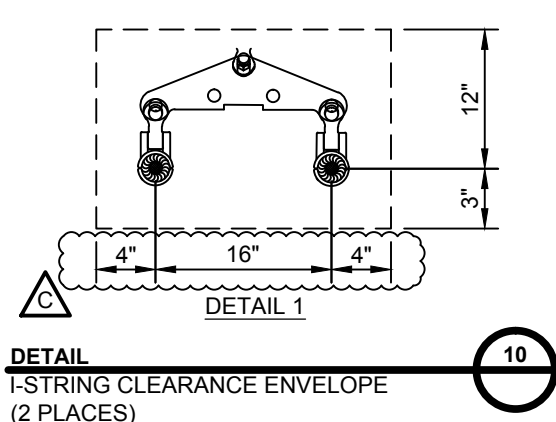
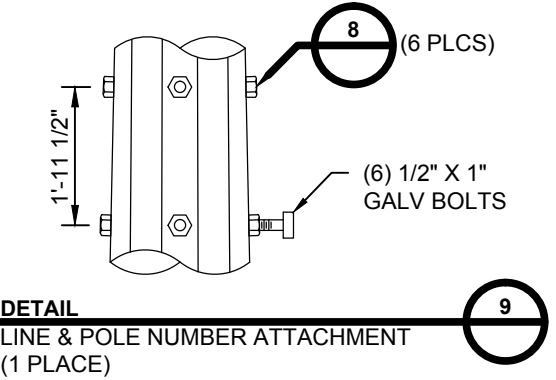
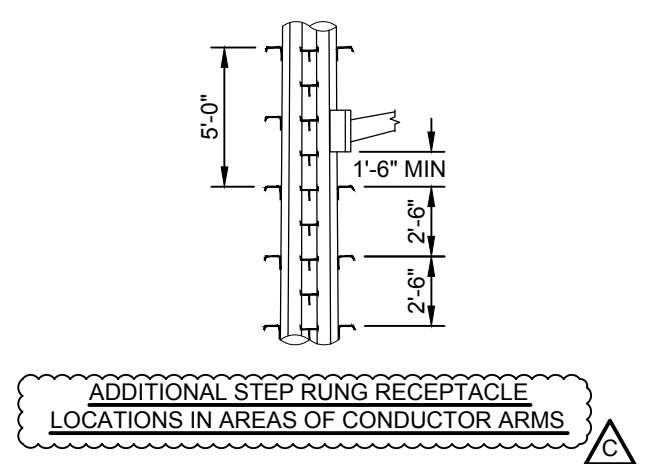
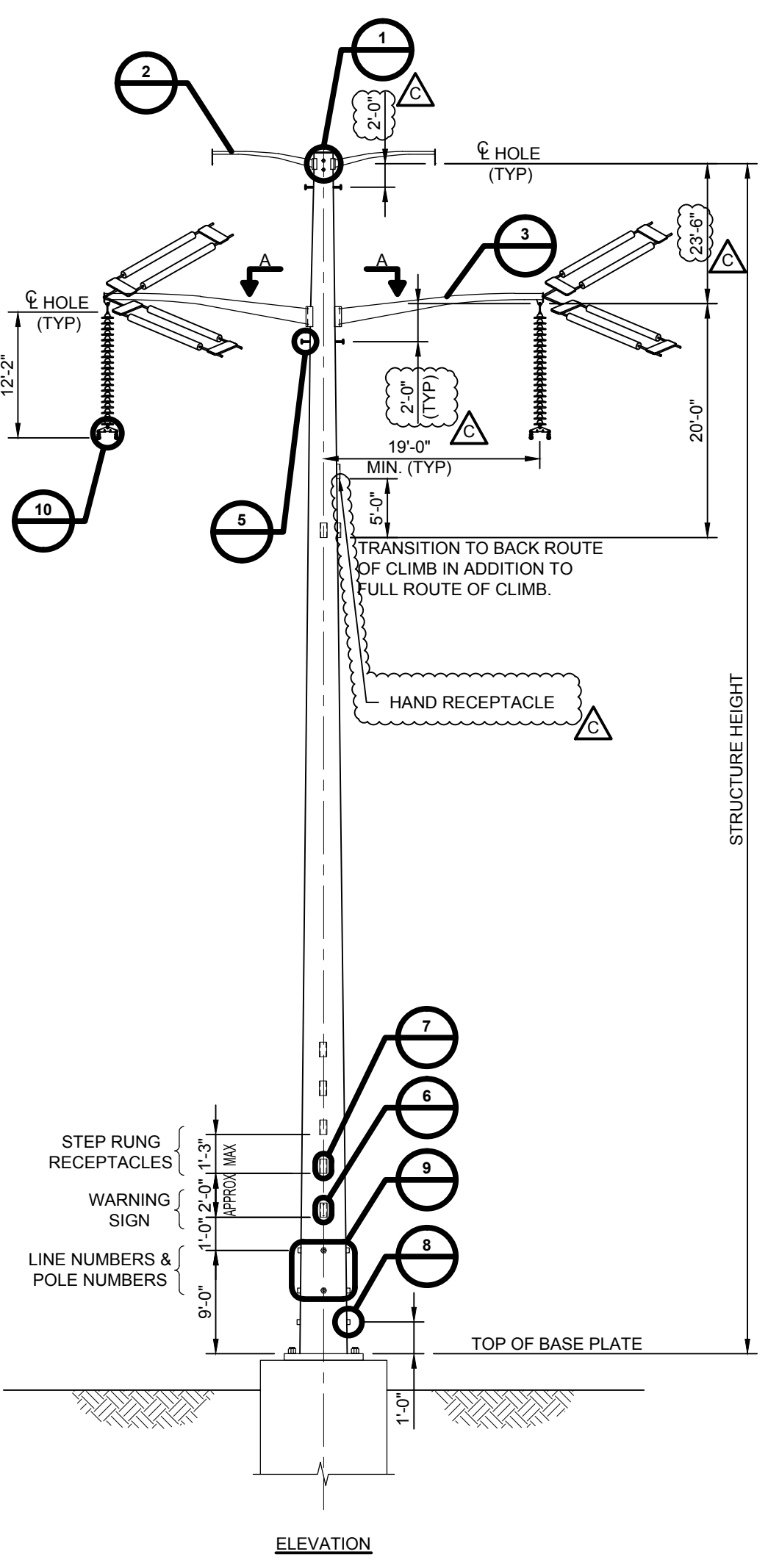
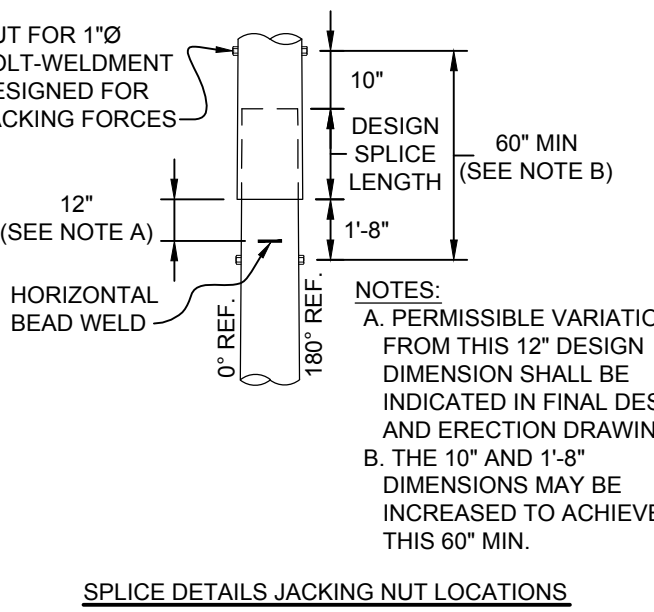
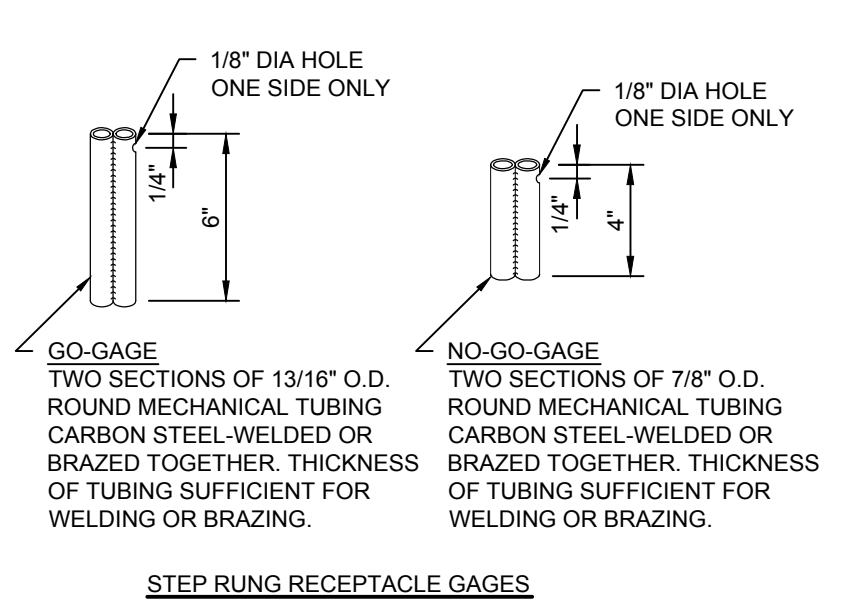
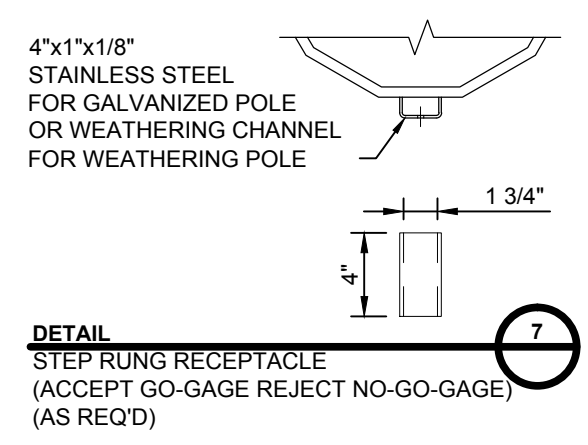
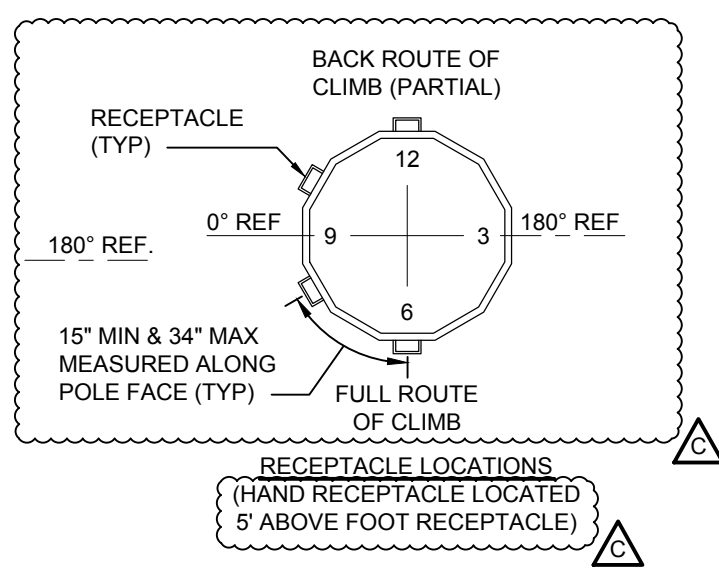
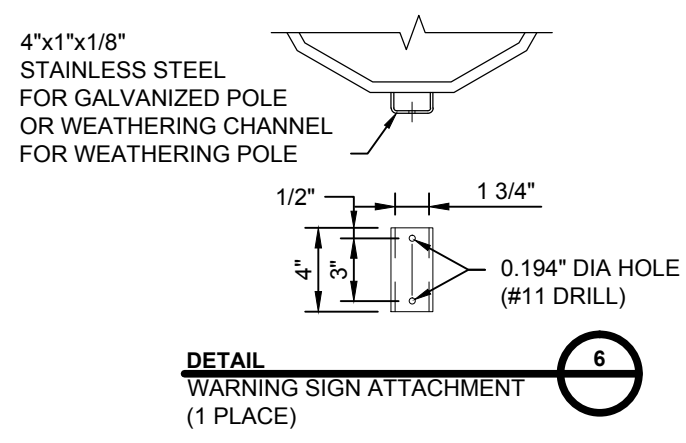
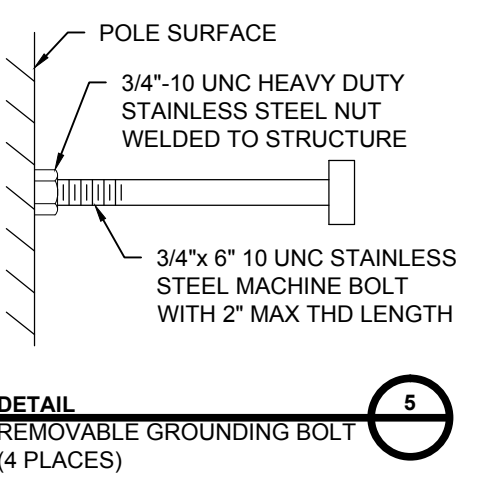
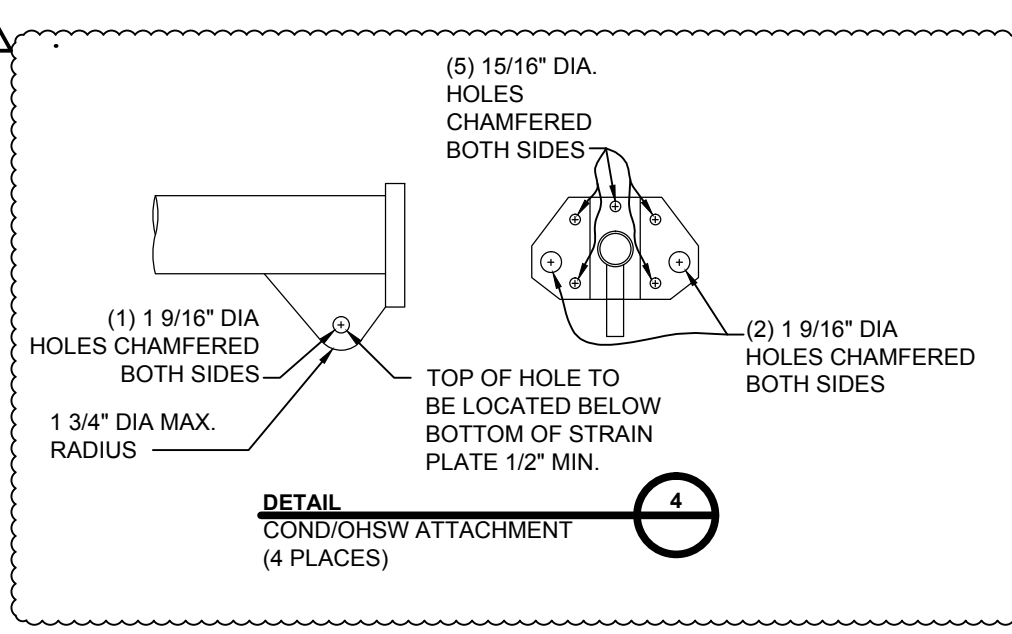
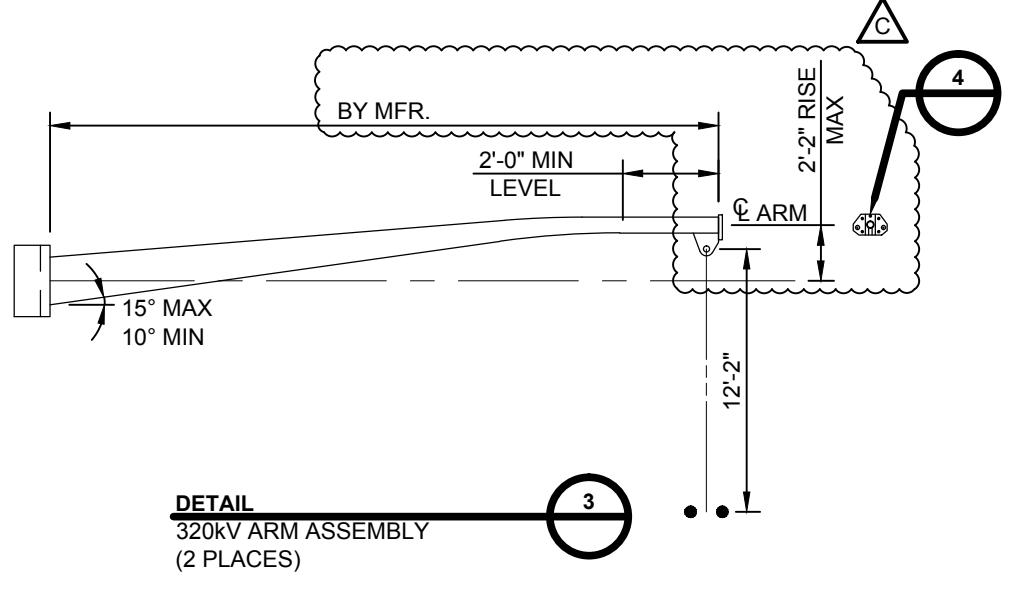
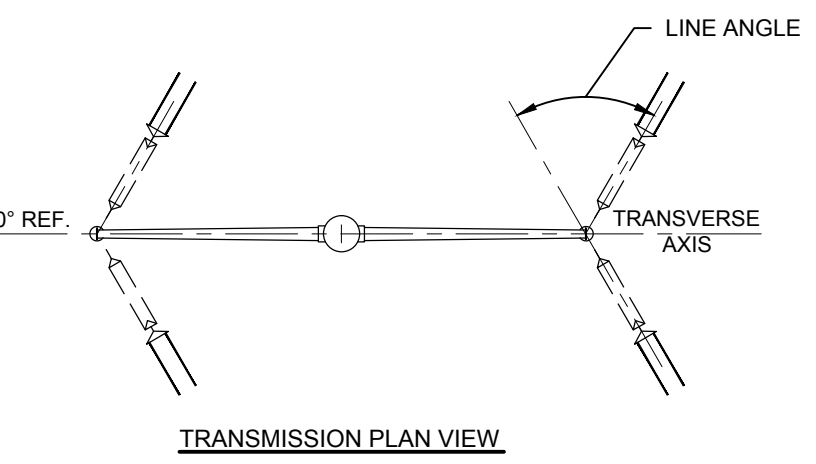
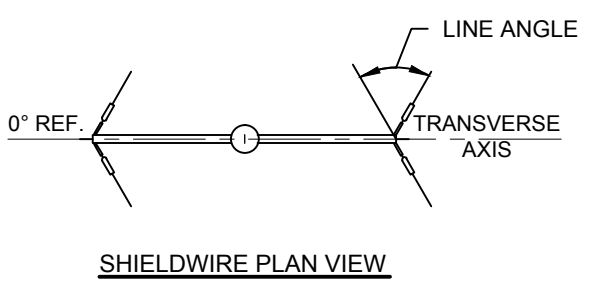
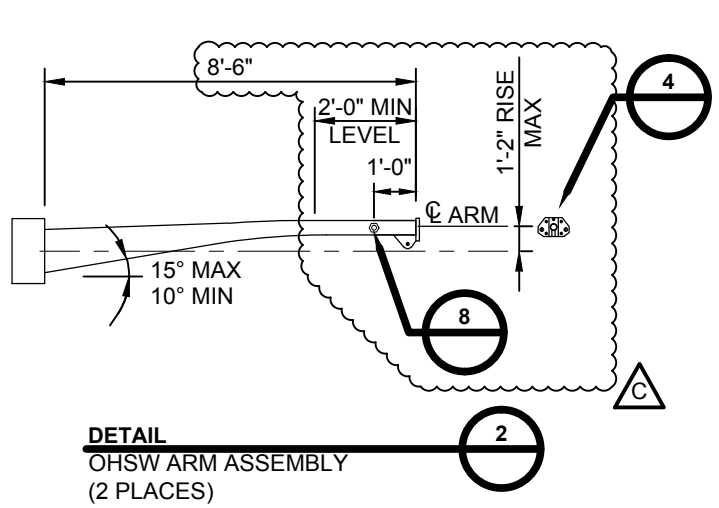
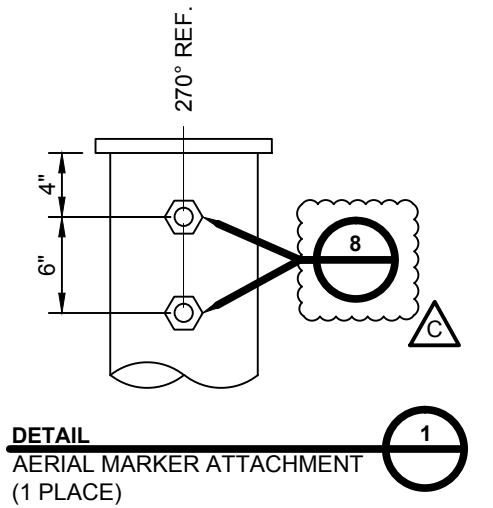
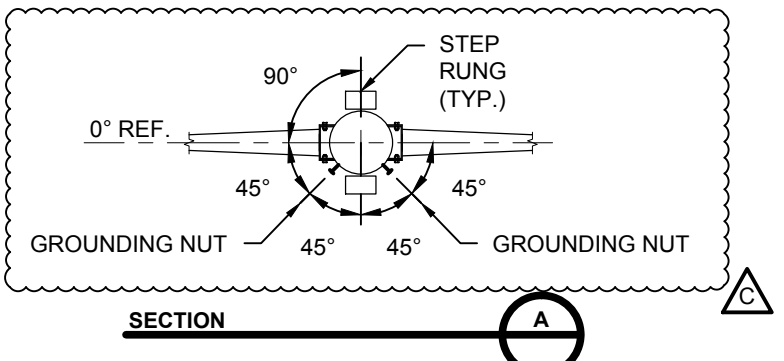
- REFERENCES:**
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

- NOTES:**
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
  - SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25.
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTABLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTABLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - 10'-9" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  - 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  - FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

**PRELIMINARY - NOT  
FOR CONSTRUCTION**

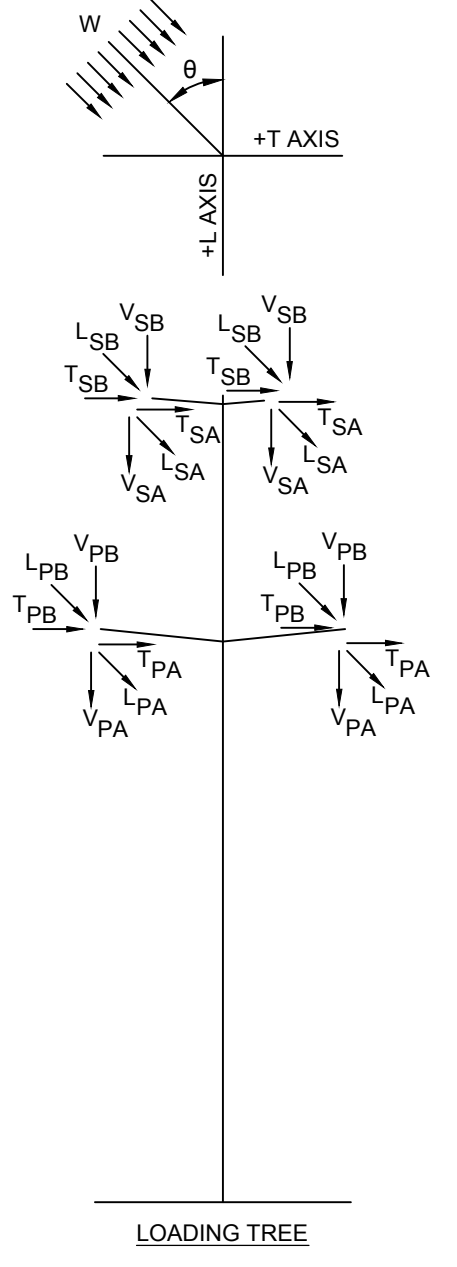
CONTRACT SERVICES							THE NORTHERN PASS			C	
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR				DRAWN	BLH
C	MISC. REVISIONS		5/27/15	MSP			320kV DC LIGHT DEADEND 0-45° 32-SCHSP-LDW-045 LOAD & DESIGN DRAWING			ENGINEER	CET
B	MISC. REVISIONS		5/8/15	BLH						CHECKED	TAB
A	RELEASE FOR RFP BID		5/1/15	BLH						APPROVED	
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR				DATE	5/1/15
SCALE NTS							FILE: TSP-16.DWG	DRAWING NO. TSP-16-001			
							IMAGE:				





STRUCTURE NAME: 32-SCHSP-HDW-090  
320-KV DC CONDUCTOR: 2 - 2933 KCMIL 91 STRAND AAAC PER PHASE (20000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 550 WIND SPAN BACK (FT): 550  
WEIGHT SPAN AHEAD (FT): 825 WEIGHT SPAN BACK (FT): 825  
LINE ANGLE: 45 - 90 DEGREES

LOADING CASE		DESIGN LOADS															
		TEMP (°F)	ICE (in)	WIND (mph)	VSA (lb)	TSA (lb)	LSA (lb)	VSB (lb)	TSB (lb)	LSB (lb)	VPA (lb)	TSA (lb)	LPA (lb)	VPB (lb)	TPB (lb)	LPB (lb)	W (lb/ft)
1	NESC 250B	0.00	0.50	39.53	1.41	7.50	8.89	1.41	7.50	-8.89	13.36	54.76	67.99	13.36	54.76	-67.99	10.00
2	NESC 250C	60.00	0.00	100.00	0.42	3.79	4.17	0.42	3.79	-4.17	5.52	31.98	35.73	5.52	31.98	-35.73	29.00
3	NESC 250D	15.00	1.00	39.53	1.97	6.12	7.40	1.97	6.12	-7.40	12.47	38.32	48.17	12.47	38.32	-48.17	4.00
4	HQ EXTREME ICE	15.00	1.50	39.53	3.51	9.16	11.13	3.51	9.16	-11.13	16.96	48.95	61.57	16.96	48.95	-61.57	4.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.94	4.40	5.39	0.94	4.40	-5.39	8.91	32.63	41.21	8.91	32.63	-41.21	4.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	4.17	-5.08	8.91	29.38	36.96	8.91	29.38	-36.96	4.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.94	4.17	5.08	0.94	4.17	-5.08	8.91	29.38	36.96	8.91	29.38	-36.96	4.00
8	CONSTRUCTION	30.00	0.00	29.97	4.12	1.38	0.25	1.98	3.78	-4.83	30.33	11.55	2.10	9.63	31.91	-40.88	3.45
9	DEFLECTION	60.00	0.00	0.00	0.42	2.09	2.73	0.42	2.09	-2.73	5.52	16.77	21.92	5.52	16.77	-21.92	0.00
10	MAINTENANCE	60.00	0.00	0.00	2.64	4.18	5.47	2.64	4.18	-5.47	12.84	33.55	43.83	12.84	33.55	-43.83	0.00
11	UPLIFT	-20.00	0.00	0.00	0.42	3.13	4.09	0.42	3.13	-4.09	5.52	30.65	40.04	5.52	30.65	-40.04	0.00



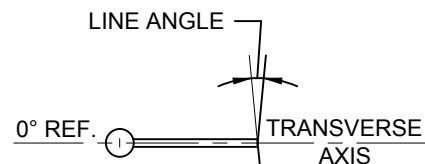
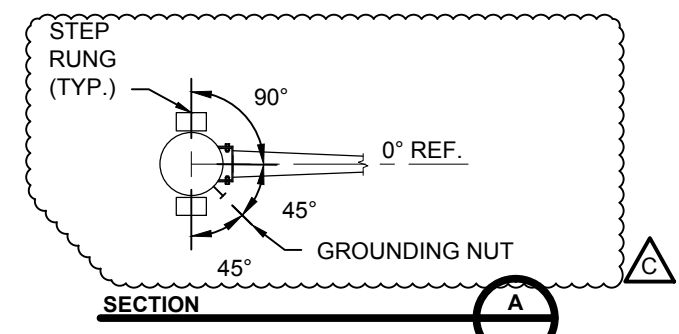
- REFERENCES:
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I

- NOTES:
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
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  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
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    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15° DEFLECTION LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 25°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  16. 3'-5" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING CLEARANCE.
  17. 10'-9" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.
  18. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

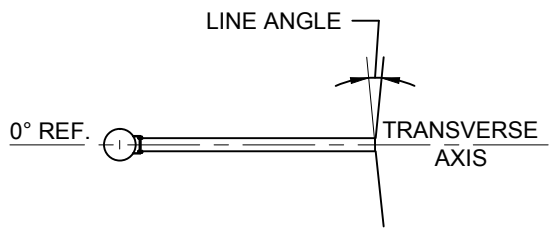
PRELIMINARY - NOT FOR CONSTRUCTION

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR		320kV DC LIGHT DEADEND 45-90° 32-SCHSP-HDW-090 LOAD & DESIGN DRAWING	SCALE NTS	FILE: TSP-17.DWG IMAGE:	DRAWING NO. TSP-17-001
C		MISC. REVISIONS		5/27/15	KAK							
B		MISC. REVISIONS		5/8/15	BLH							
A		RELEASE FOR RFP BID		5/1/15	BLH							
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR					

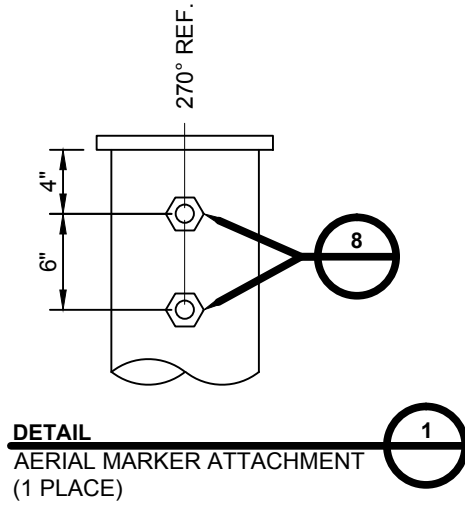




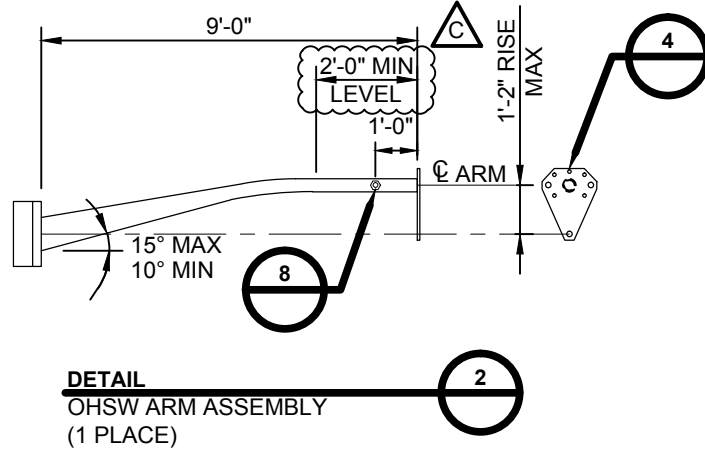
SHIELDWIRE PLAN VIEW



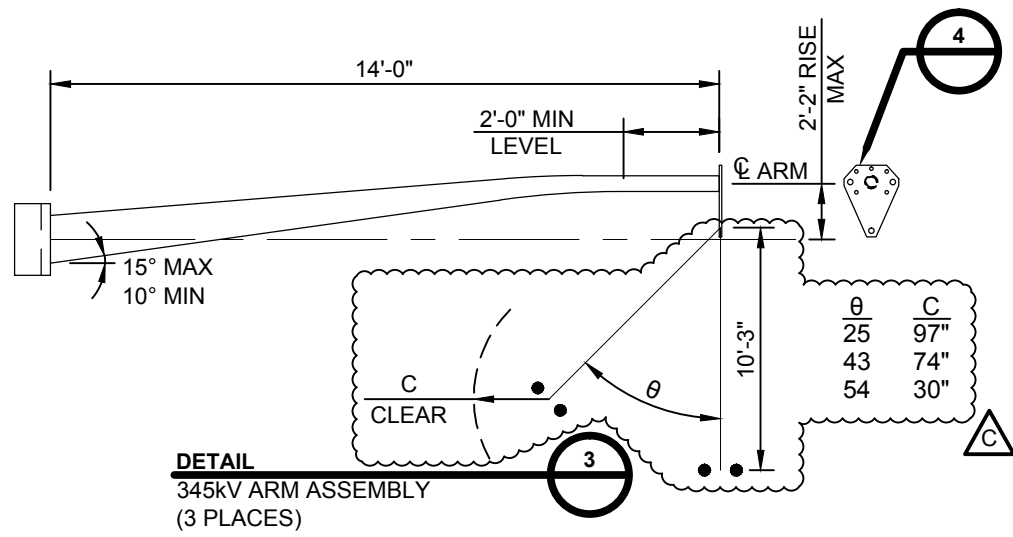
TRANSMISSION PLAN VIEW



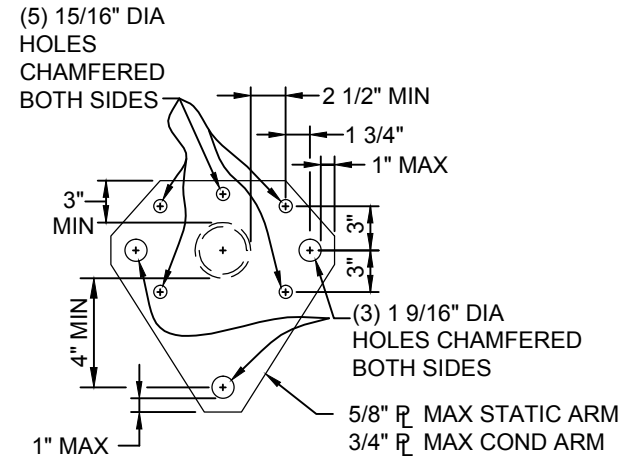
DETAIL  
AERIAL MARKER ATTACHMENT  
(1 PLACE)



DETAIL  
OHSW ARM ASSEMBLY  
(1 PLACE)

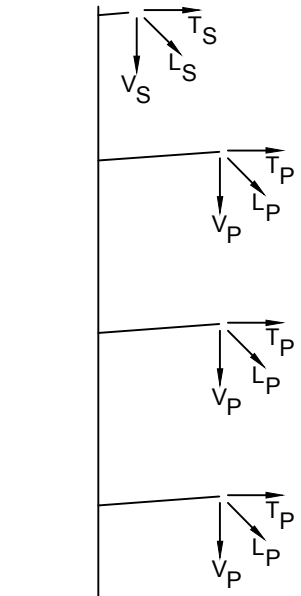
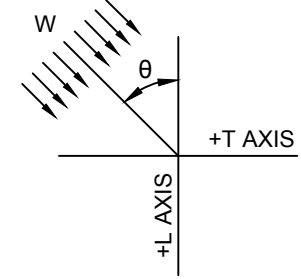


DETAIL  
345KV ARM ASSEMBLY  
(3 PLACES)

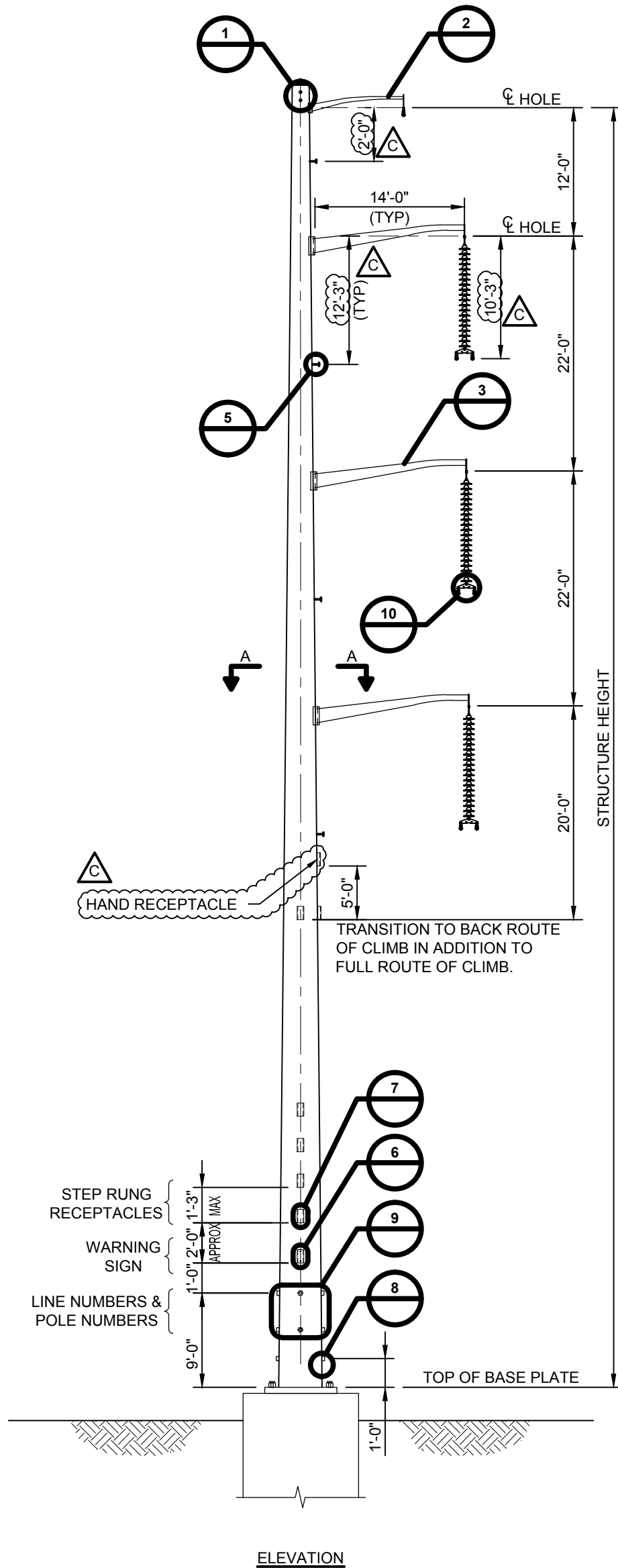


DETAIL  
SUSPENSION/STRAIN PLATE  
(4 PLACES)

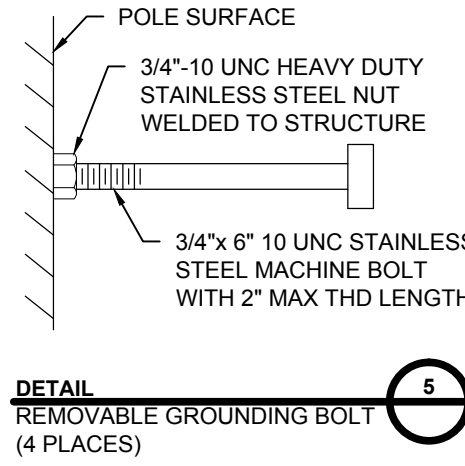
- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I



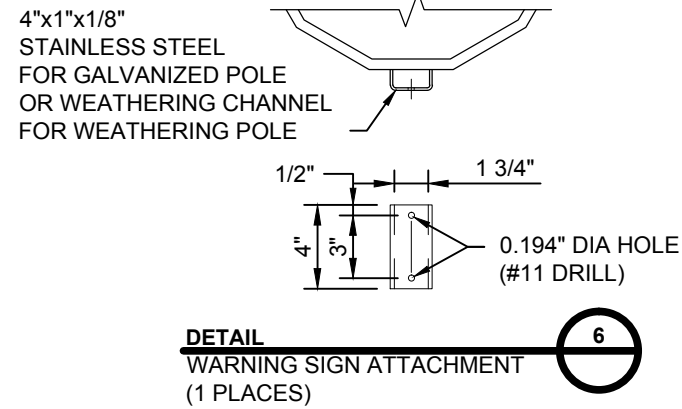
LOADING TREE



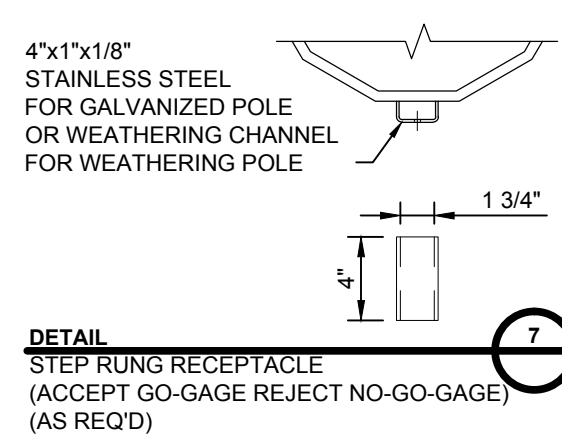
ELEVATION



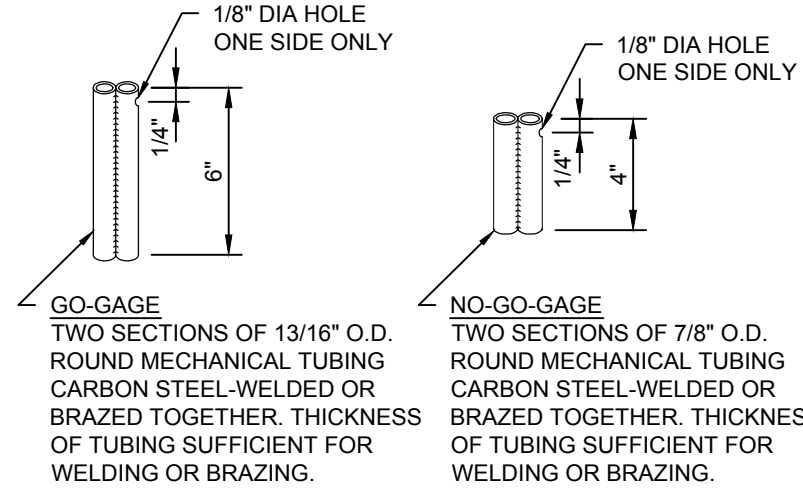
DETAIL  
REMOVABLE GROUNDING BOLT  
(4 PLACES)



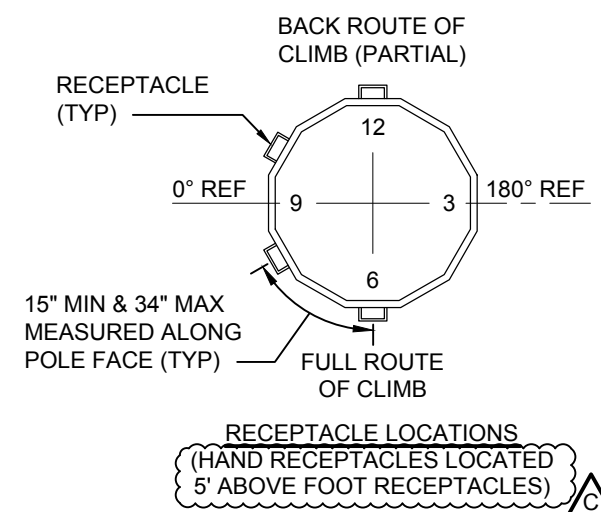
DETAIL  
WARNING SIGN ATTACHMENT  
(1 PLACES)



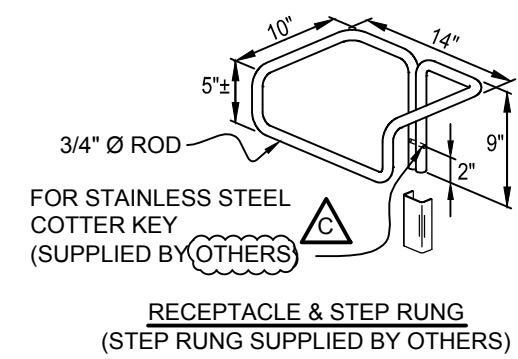
DETAIL  
STEP RUNG RECEPTACLE  
(ACCEPT GO-GAGE REJECT NO-GO-GAGE)  
(AS REQ'D)



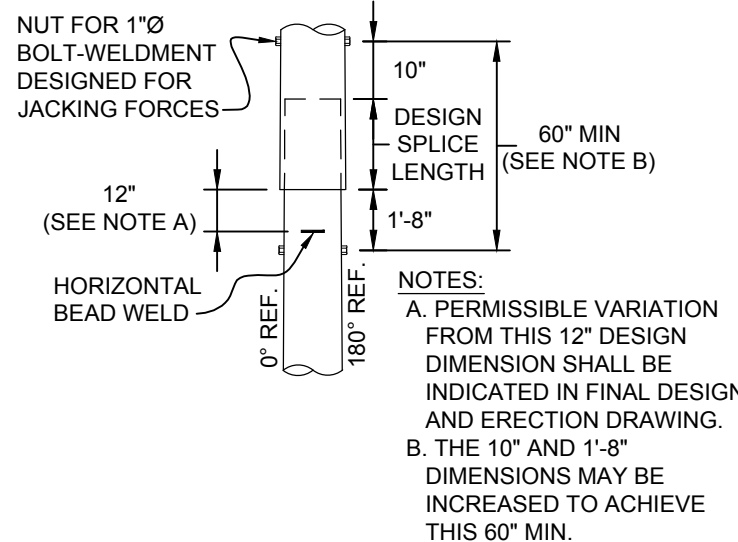
STEP RUNG RECEPTACLE GAGES



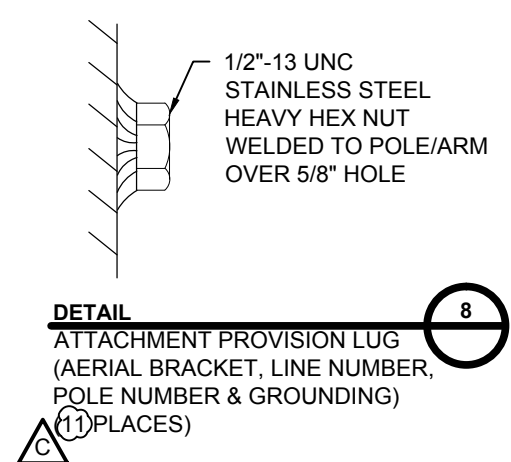
ADDITIONAL STEP RUNG  
RECEPTACLE LOCATIONS IN  
AREA OF CONDUCTOR ARMS



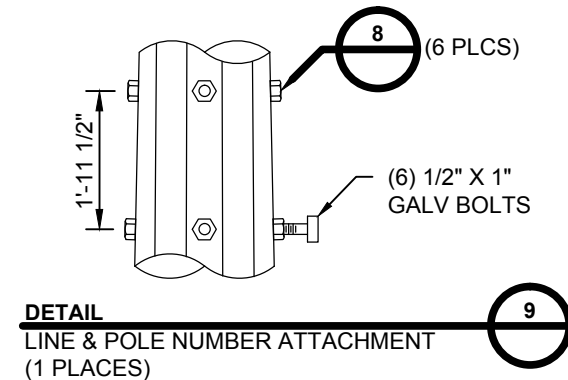
RECEPTACLE & STEP RUNG  
(STEP RUNG SUPPLIED BY OTHERS)



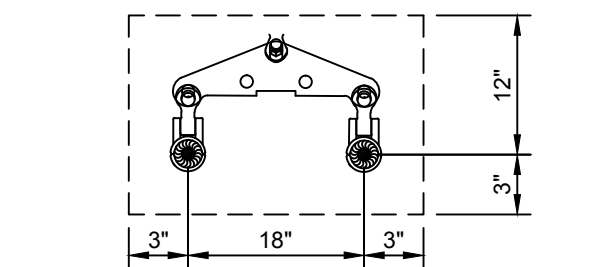
SPLICE DETAILS JACKING NUT LOCATIONS



DETAIL  
ATTACHMENT PROVISION LUG  
(AERIAL BRACKET, LINE NUMBER,  
POLE NUMBER & GROUNDING)  
(11 PLACES)




DETAIL  
LINE & POLE NUMBER ATTACHMENT  
(1 PLACES)



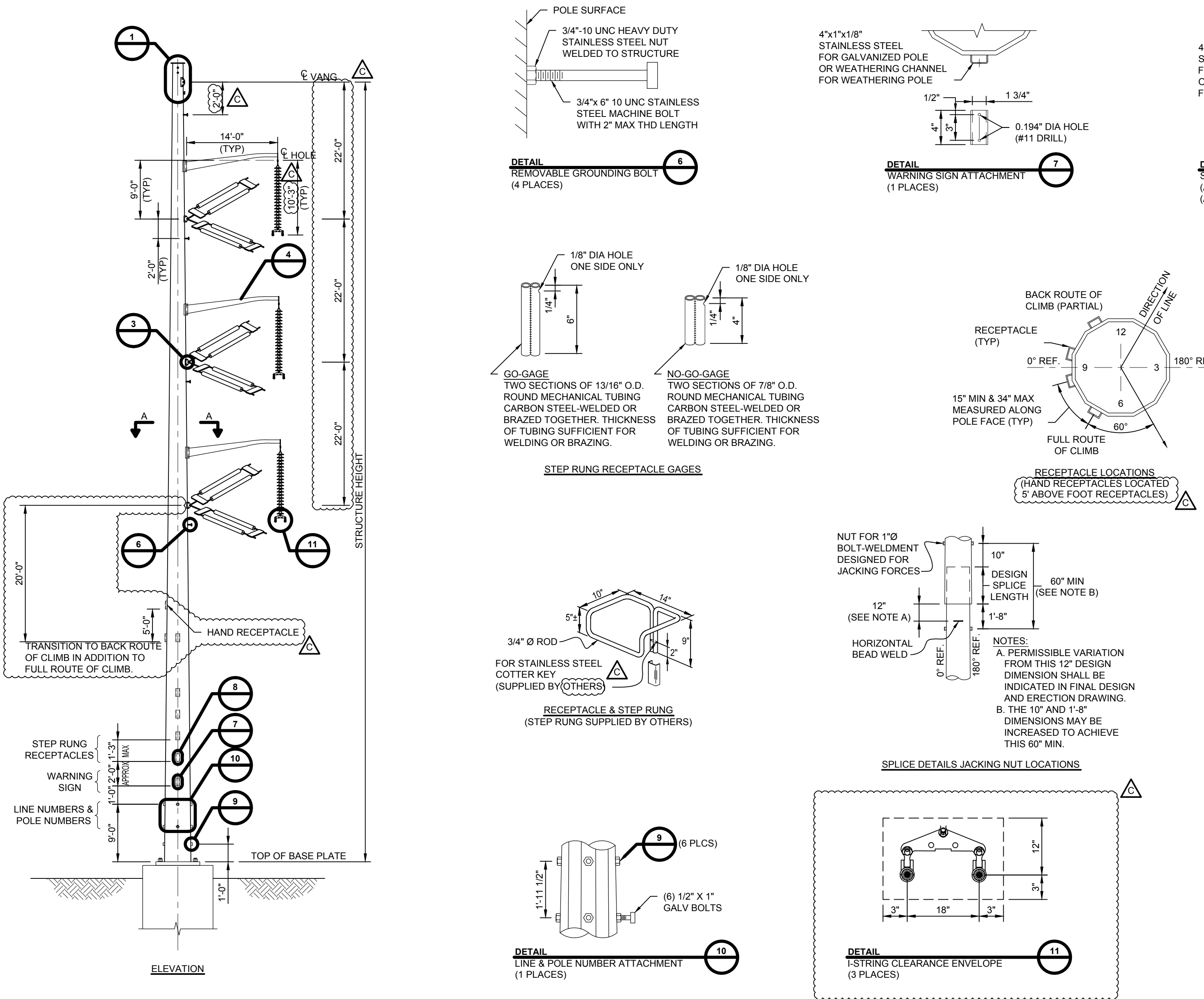
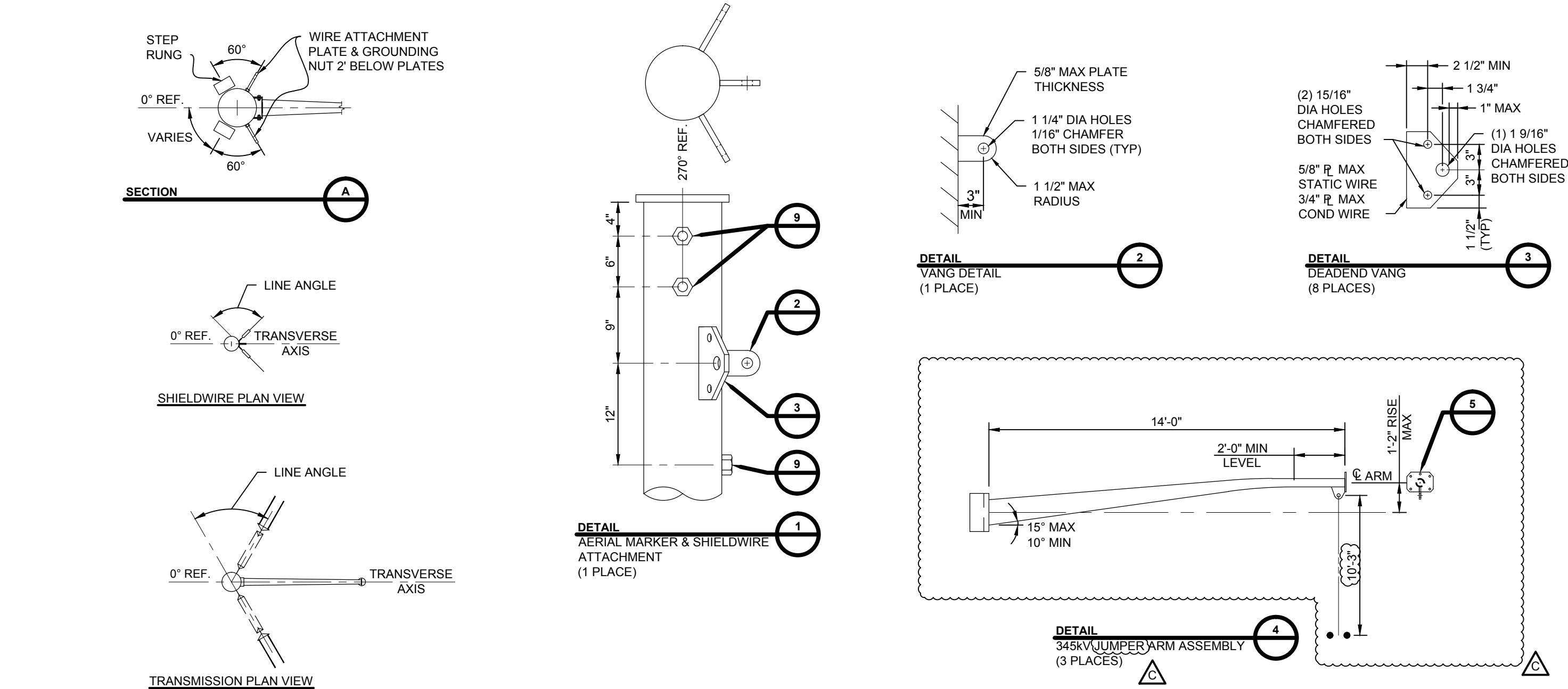
DETAIL  
1-STRING CLEARANCE ENVELOPE  
(3 PLACES)

- NOTES:**
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  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 10.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.  
**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  12. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  13. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  14. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL POINTS OF THE CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNS TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  15. VANGS AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  16. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

CONTRACT SERVICES								 THE NORTHERN PASS	C	
									DRAWN BLH	
									ENGINEER CET	
									CHECKED TAB	
									APPROVED	
									DATE 5/1/15	
	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR			
	C	MISC. UPDATES		5/22/15	MSP					
	B	MISC. REVISIONS		5/5/15	BLH					
		RELEASE FOR RFP BID		5/1/15	BLH					
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	SCALE NTS	FILE: TSP-18.DWG IMAGE:	DRAWING NO. TSP-18-001

**PRELIMINARY - NOT  
FOR CONSTRUCTION**





STRUCTURE NAME: 30-SCVSP-LDW-060  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 400 WIND SPAN BACK (FT): 400  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 0 - 60 DEGREES

LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	5.32	9.62	0.84	5.32	-9.62	6.50	22.29	41.24	6.50	22.29	-41.24	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	2.69	4.51	0.26	2.69	-4.51	2.48	14.12	23.11	2.48	14.12	-23.11	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	4.34	8.01	1.15	4.34	-8.01	6.11	16.70	31.53	6.11	16.70	-31.53	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	5.36	9.92	1.56	5.36	-9.92	7.22	19.56	36.98	7.22	19.56	-36.98	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	3.12	5.83	0.56	3.12	-5.83	4.33	13.16	24.99	4.33	13.16	-24.99	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	2.95	5.50	0.56	2.95	-5.50	4.33	12.07	22.80	4.33	12.07	-22.80	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	2.95	5.50	0.56	0.20	0.00	4.33	12.07	22.80	4.33	0.67	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.45	0.27	1.74	2.67	-5.23	14.89	6.67	1.21	5.06	12.09	-23.49	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.26	1.48	2.96	0.26	1.48	-2.96	2.48	6.67	13.34	2.48	6.67	-13.34	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.33	2.96	5.92	2.33	2.96	-5.92	6.75	13.34	26.68	6.75	13.34	-26.68	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.26	2.22	4.43	0.26	2.22	-4.43	2.48	10.34	20.69	2.48	10.34	-20.69	0.00	90.00	1.00

- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I

- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 1.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTABLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTABLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  15. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  16. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  17. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  18. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	C	DRAWN	BLH	ENGINEER	CET	CHECKED	TAB	APPROVED	DATE	5/1/15
C		MISC. UPDATES		5/22/15	MSP												
B		MISC. REVISIONS		5/8/15	BLH												
A		RELEASE FOR RFP BID		5/1/15	BLH												
DWG REV		EPN/DESCRIPTION		CONT/PE#	DATE	DRN	CHKD	APPR									

THE NORTHERN PASS

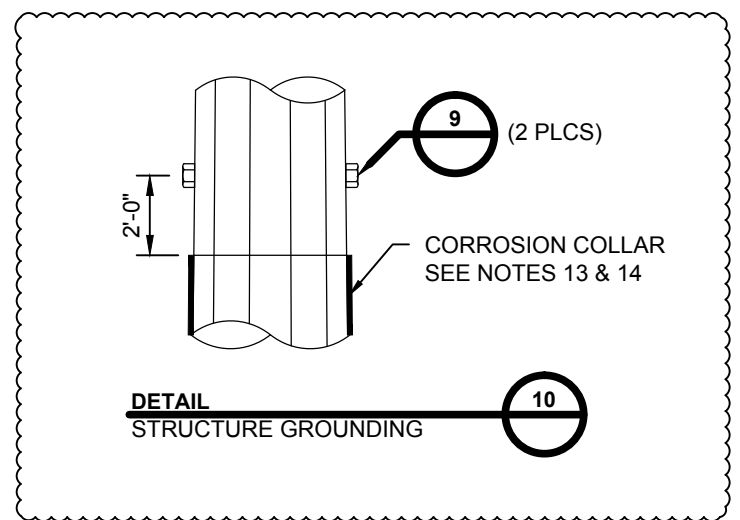
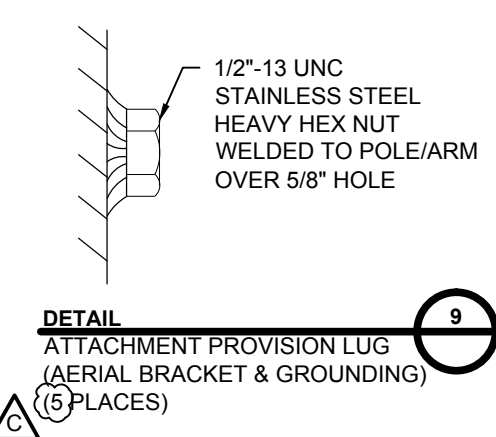
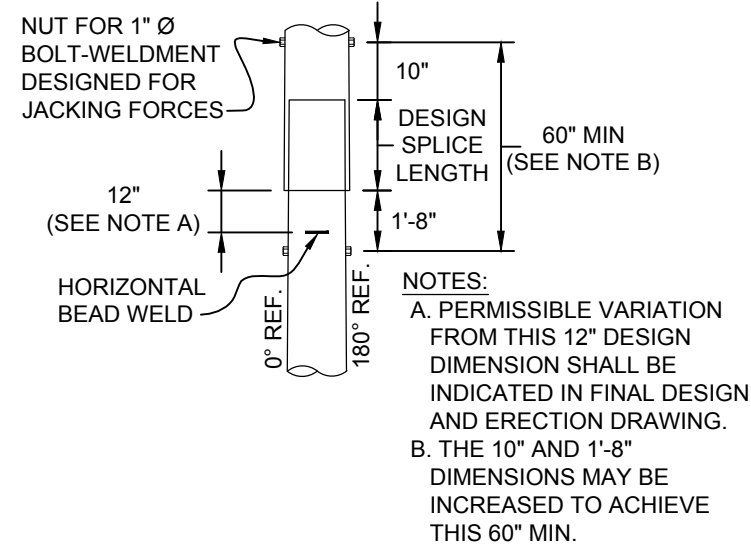
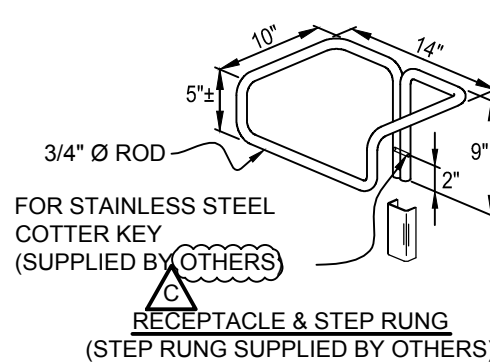
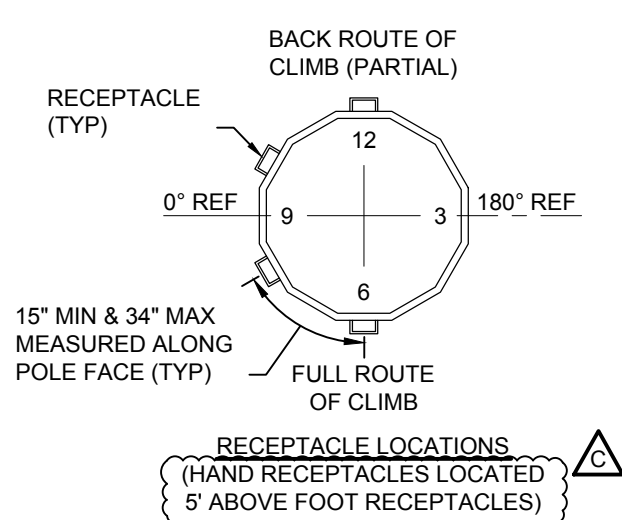
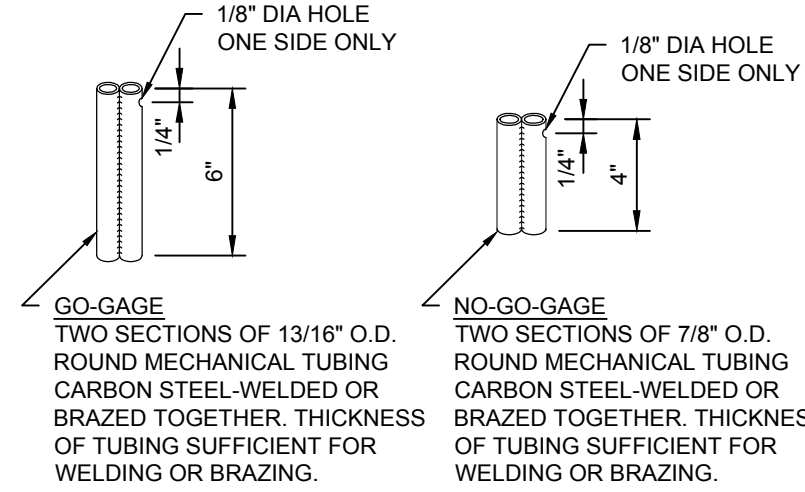
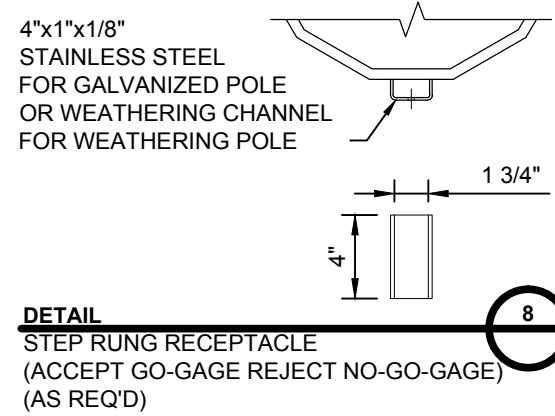
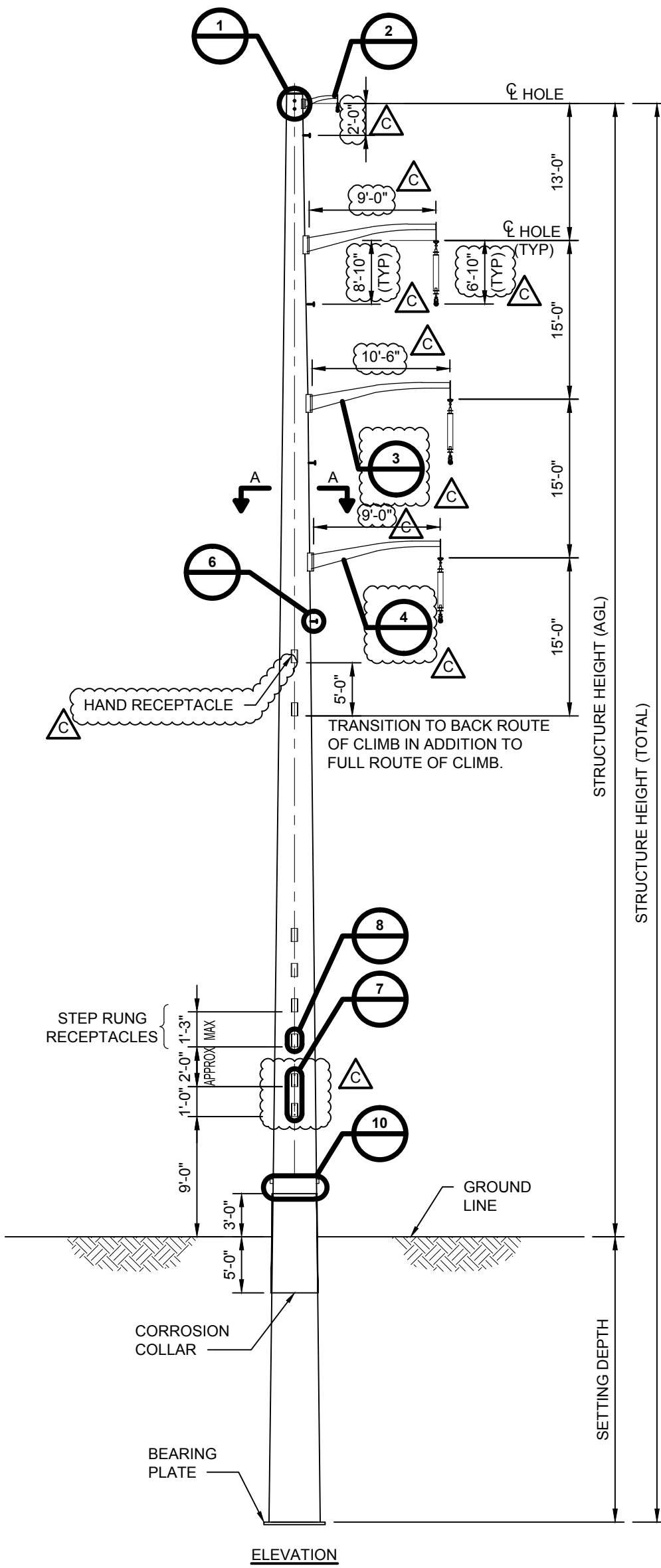
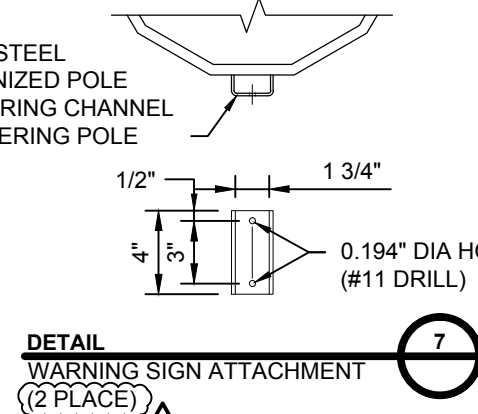
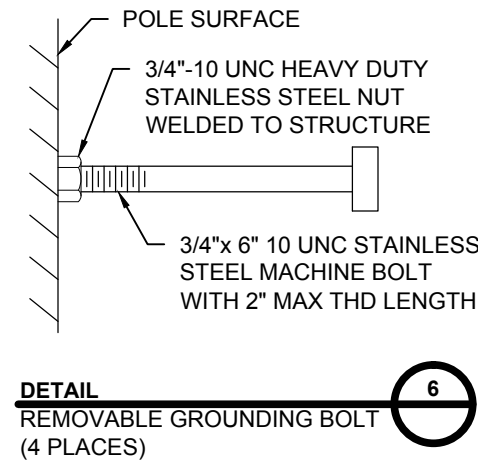
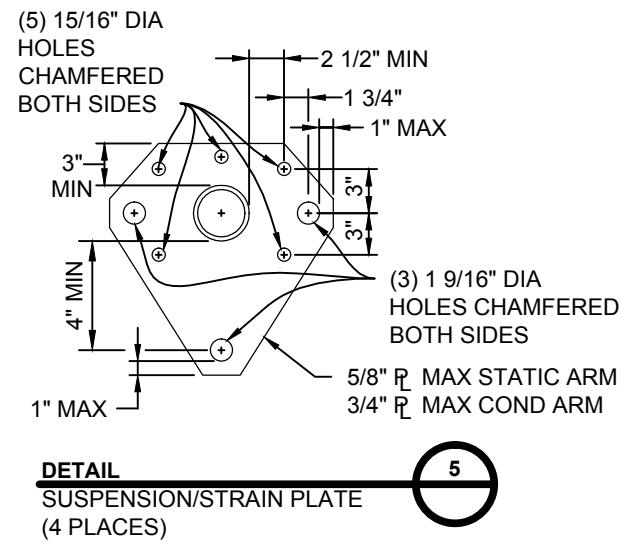
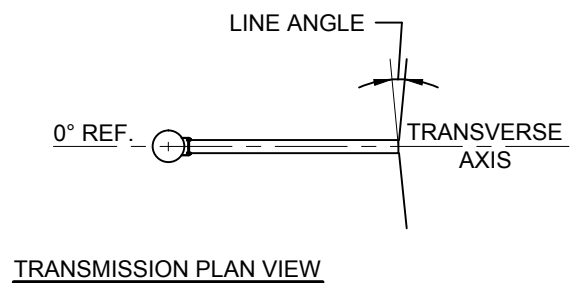
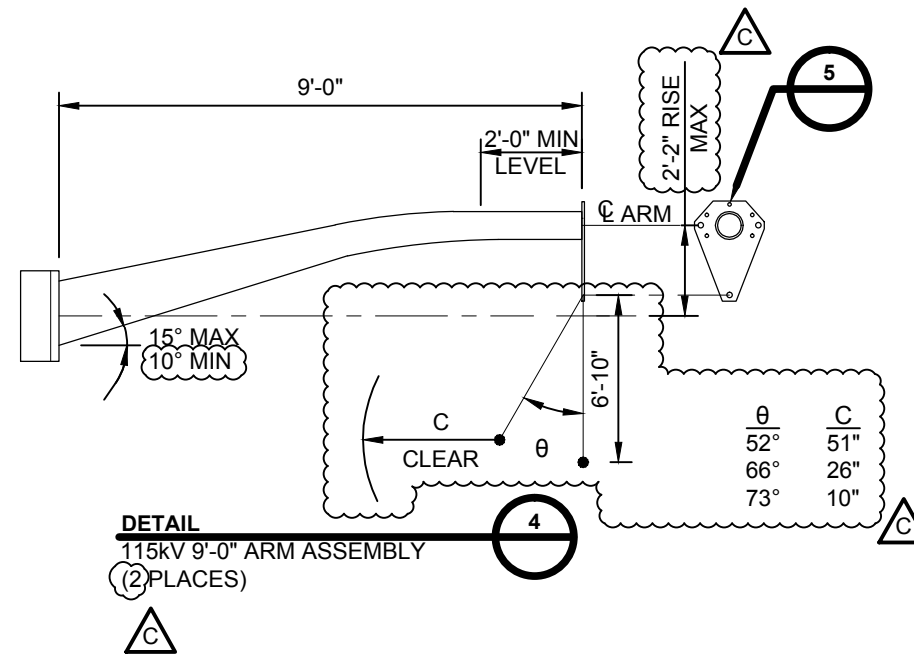
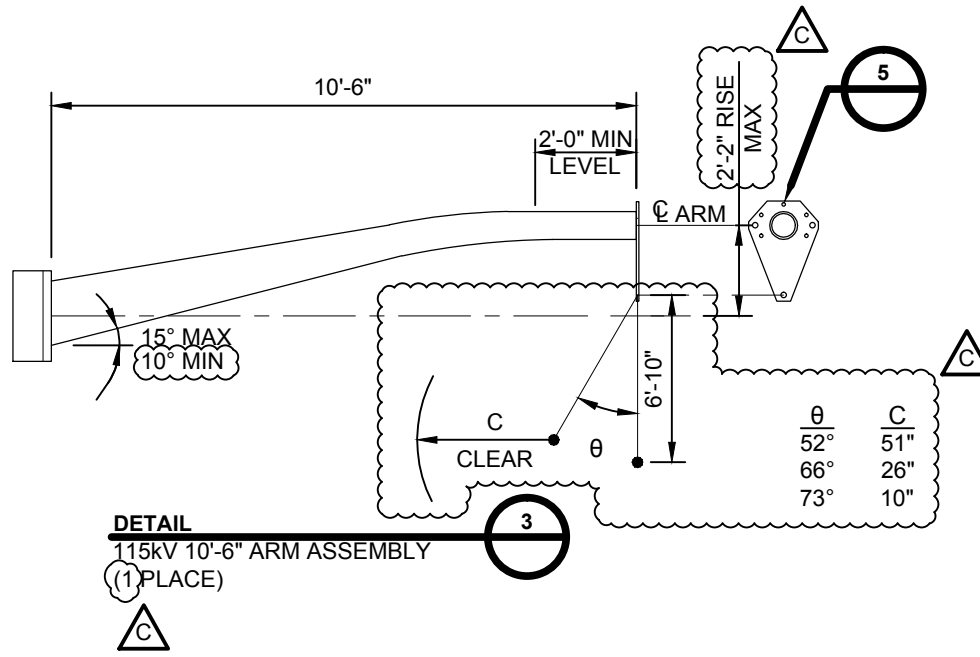
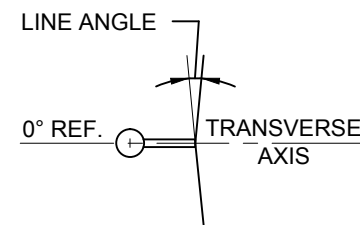
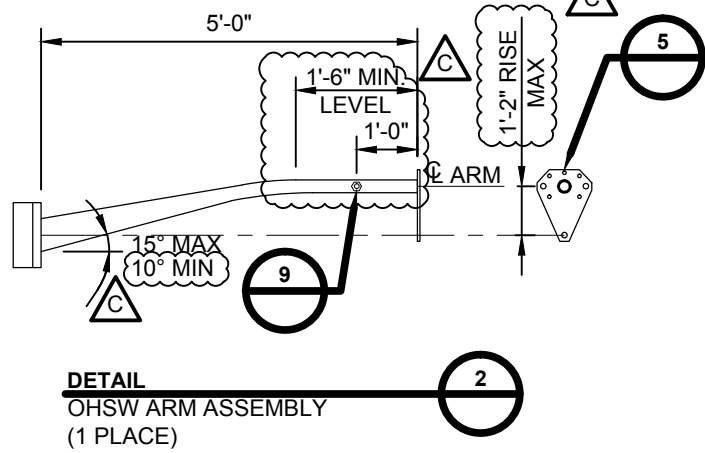
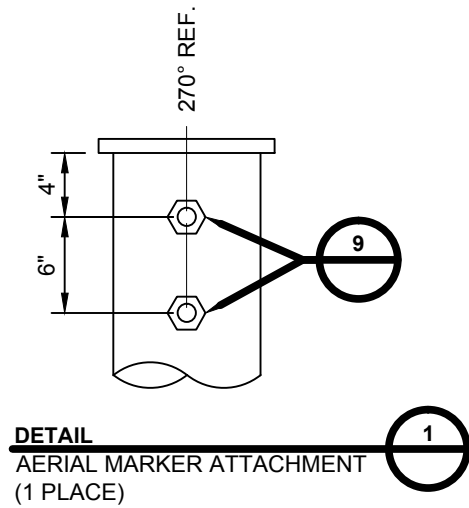
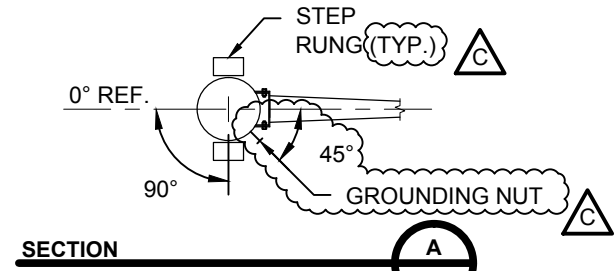
345kV AC LIGHT DEADEND 0-60°  
30-SCVSP-LDW-060  
LOAD & DESIGN DRAWING

SCALE: NTS  
FILE: TSP-19.DWG  
IMAGE:

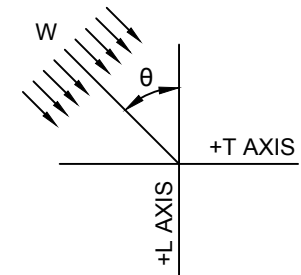
DRAWING NO.: TSP-19-001

**PRELIMINARY - NOT  
FOR CONSTRUCTION**





- REFERENCES:**
1. CLIMBING FACILITIES: SKETCH B
  2. GROUNDING NUTS: SKETCH B
  3. HAND + FOOT RECEPTACLE LOCATIONS: SKETCH C
  4. STEP RUNG: SKETCH E
  5. ATTACHMENT PROVISIONS FOR SIGNS + GROUNDING: SKETCH F
  6. JACKING NUT LOCATIONS: SKETCH I
  7. LIFTING VANGS: SKETCH J + K
  8. STEP RUNG RECEPTACLE GAGES: SKETCH L
  9. FALL PROTECTION VANGS: SKETCH N + Q



- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. STEEL PLATE, A MINIMUM OF 1/4" THICKNESS GREATER THAN THAT REQUIRED FOR COLUMN STRENGTH SHALL BE IN PLACE IN THE AREA 3'-0" ABOVE AND 5'-0" BELOW THE NOMINAL GROUND LINE.
  15. APPLY COAL TAR EPOXY ON INSIDE AND OUTSIDE OF POLE FROM BUTT OF POLE TO 12" ABOVE TOP OF CORROSION COLLAR.
  16. BELOW GROUND CORROSION PROTECTION COATING MATERIAL SHALL BE SUPPLIED (ONE QUART PER TWO STRUCTURES) TO "TOUCH UP" SCRATCHES OCCURRING IN SHIPPING AND HANDLING. A COPY OF THE MSDS SHEET SHALL BE SUPPLIED WITH THE "TOUCH UP" MATERIALS.
  17. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION & ON REFERENCE SKETCHES N + Q.
  18. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.

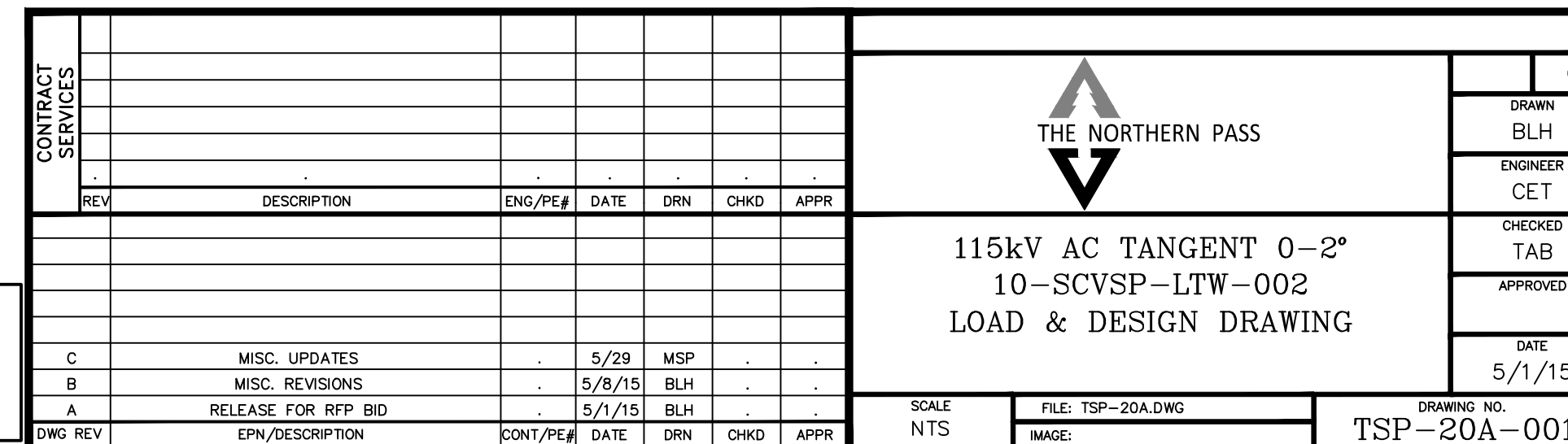
STRUCTURE NAME: 10-SCVSP-LTW-002  
115-KV AC CONDUCTOR: 1 - 795 KCMIL 26/7 "DRAKE" ACSR PER PHASE (9000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN (FT): 800  
WEIGHT SPAN (FT): 1250  
LINE ANGLE: 0 - 2 DEGREES

LOADING CASE				DESIGN LOADS									
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.50	2.09	1.34	0.00	4.52	1.96	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.61	1.03	0.00	1.62	2.20	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.50	2.96	0.94	0.00	5.04	1.27	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.30	39.50	4.03	1.14	0.00	6.35	1.47	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.50	1.40	0.61	0.00	3.02	0.90	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.50	1.40	0.59	0.00	3.02	0.80	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.50	1.40	0.50	5.50	3.02	0.68	6.75	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	30.00	3.85	0.30	0.27	6.55	0.58	0.48	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.61	0.10	0.00	1.62	0.18	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	3.02	0.21	0.00	5.03	0.36	0.00	0.00	90.00	2.00

**PRELIMINARY - NOT FOR CONSTRUCTION**

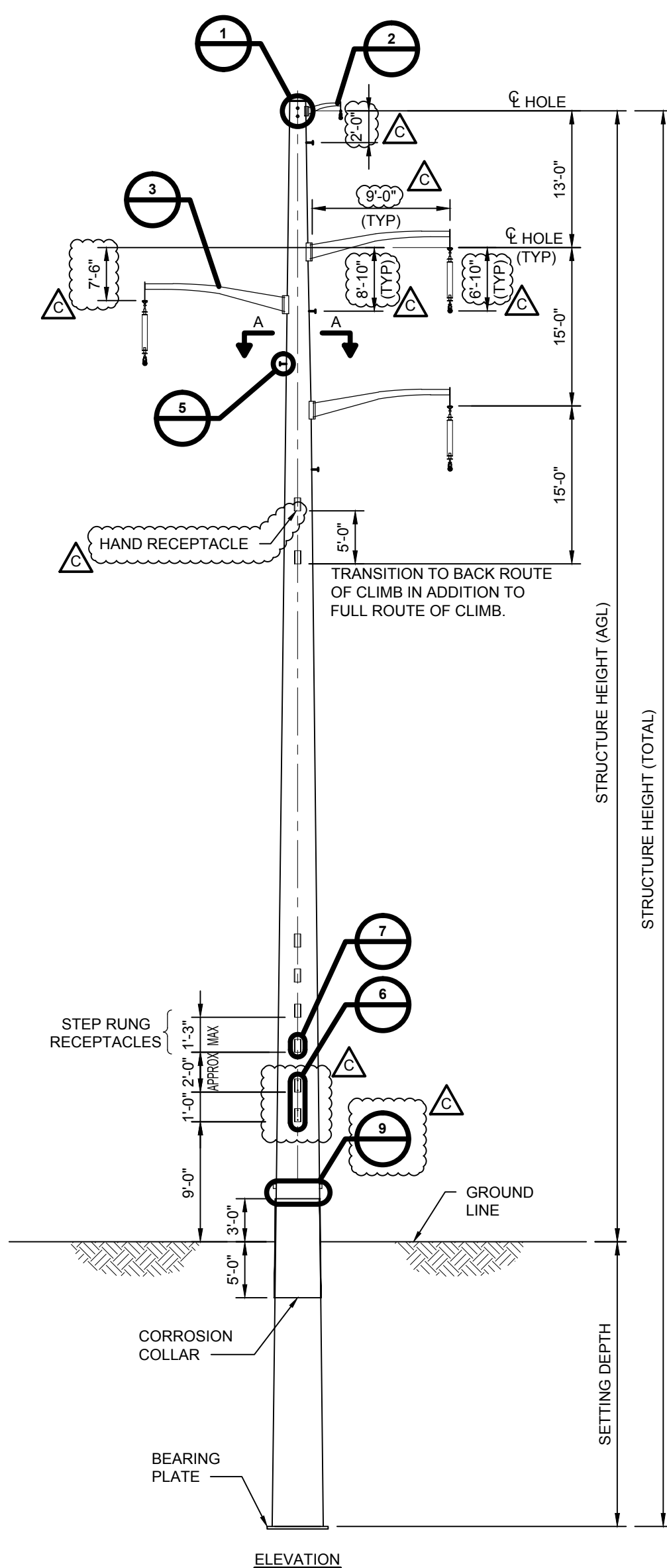
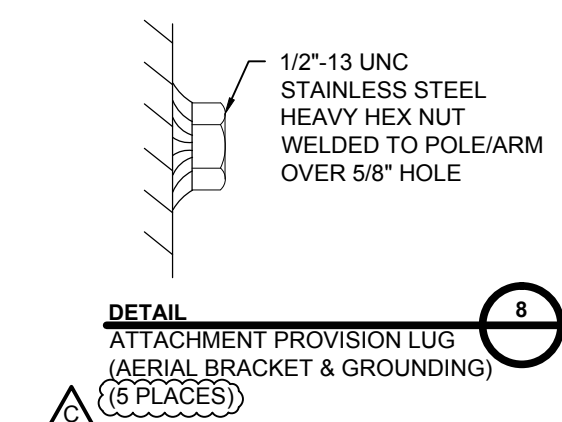
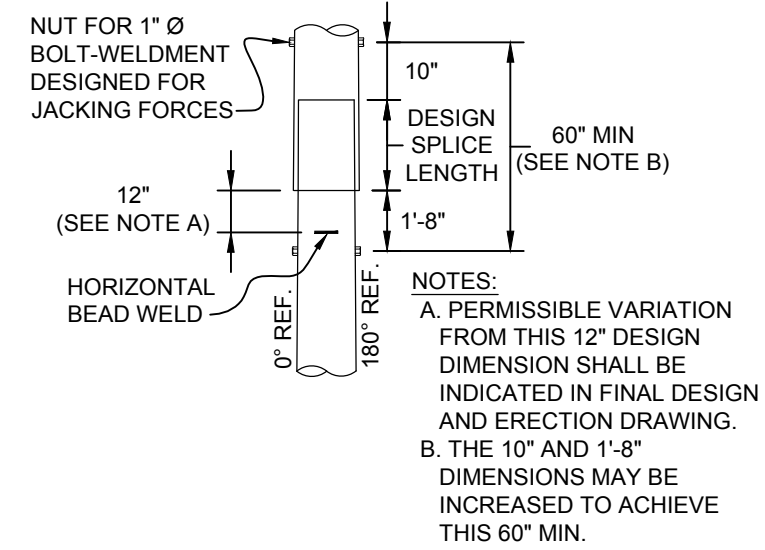
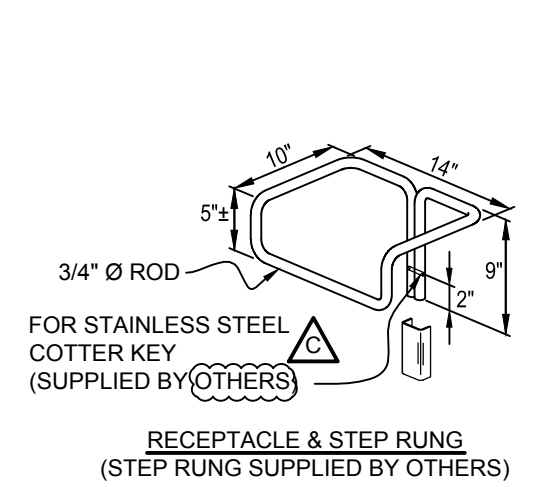
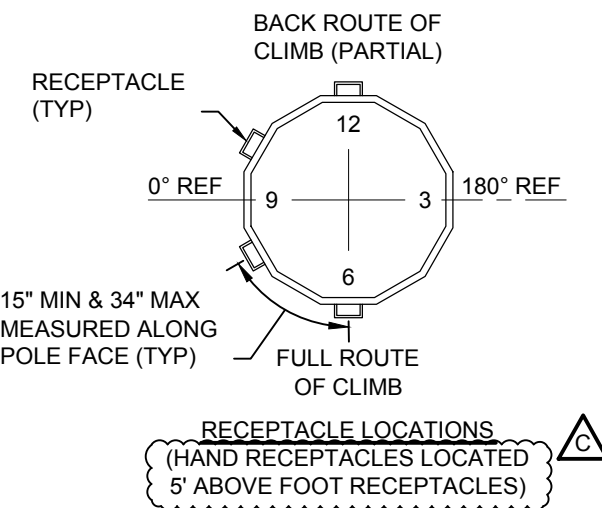
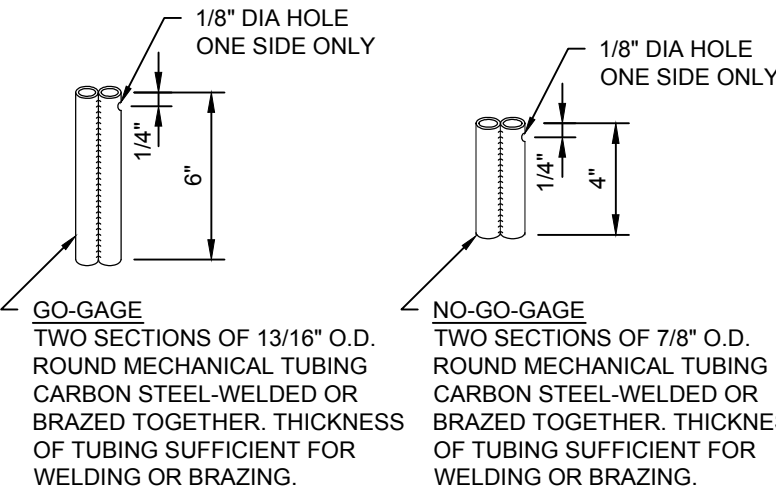
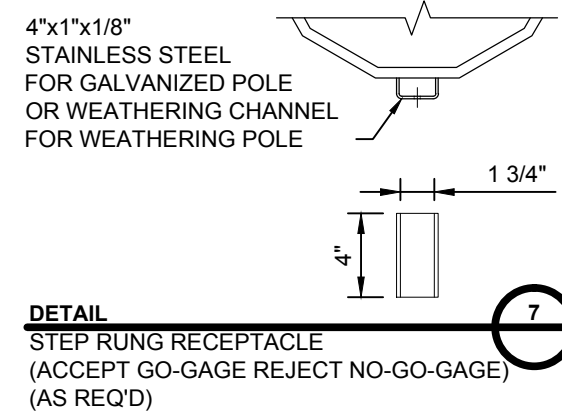
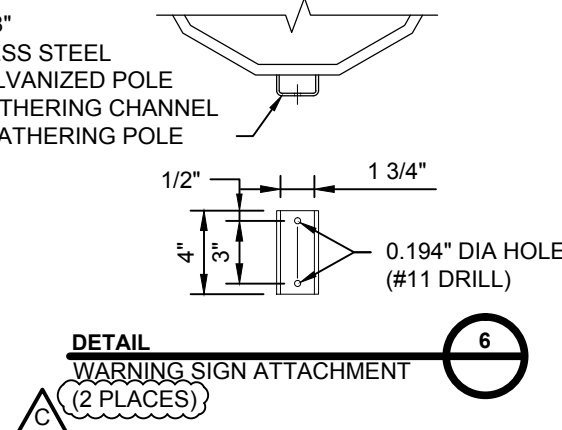
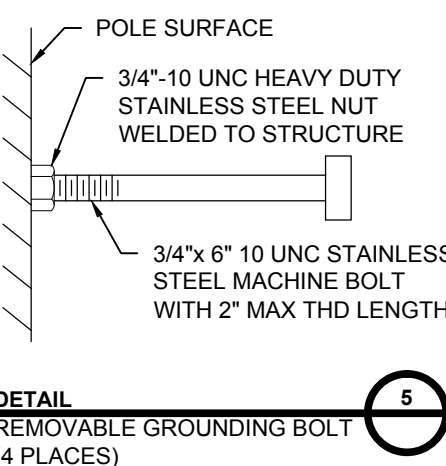
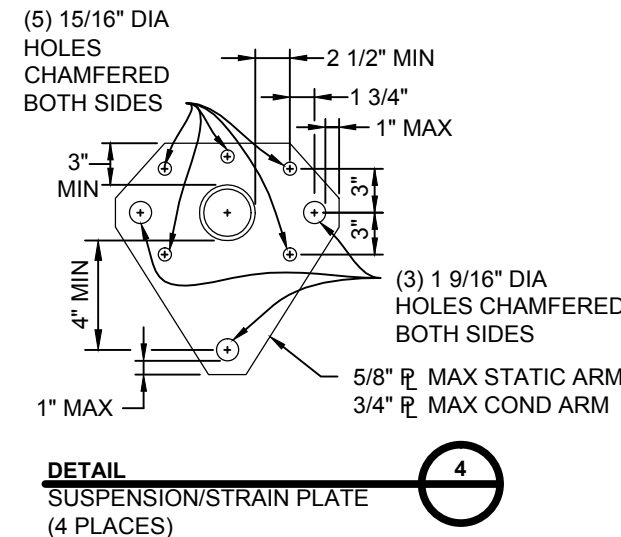
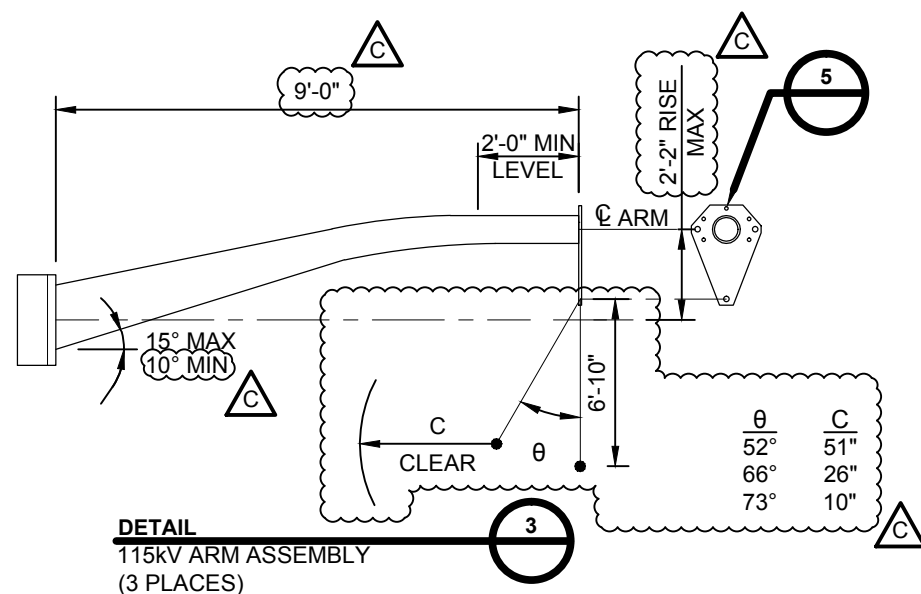
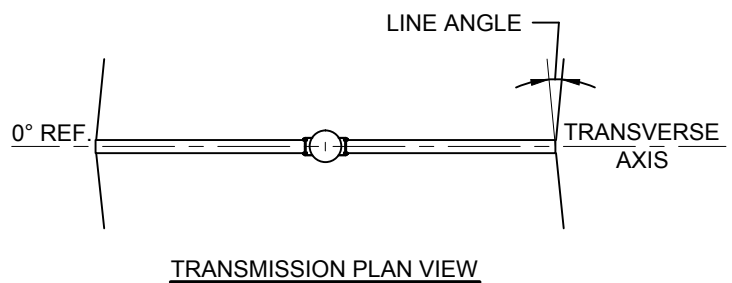
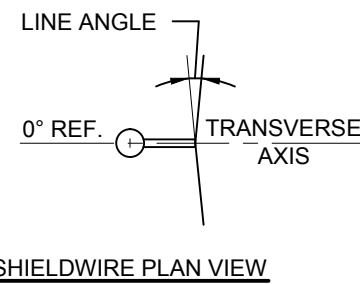
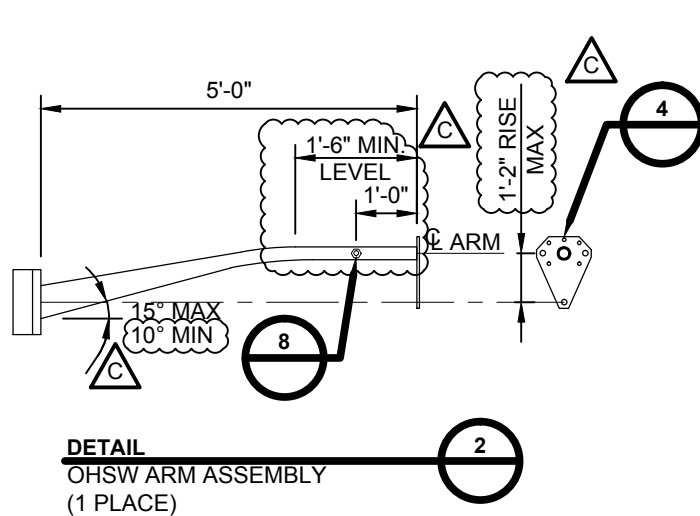
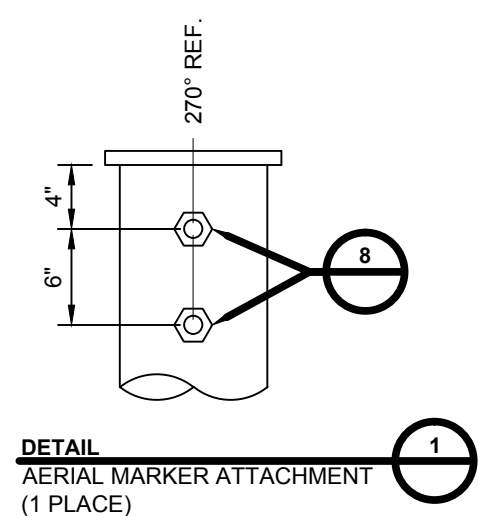
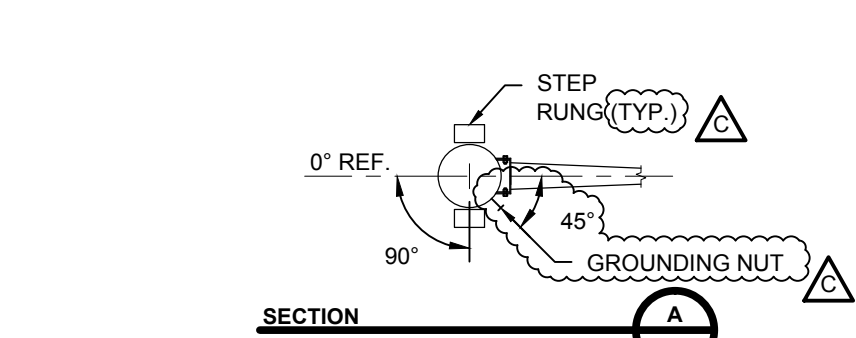
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REV							DRAWN			BLH	
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ENG/PE#							CHECKED			TAB	
DATE							APPROVED			DATE	
DRN							FILE: TSP-20.DWG			TSP-20-001	
CHKD							IMAGE:				
APPR							SCALE				
MISC. UPDATES							115kV AC TANGENT 0-2°				
MISC. REVISIONS							10-SCVSP-LTW-002				
RELEASE FOR RFP BID							LOAD & DESIGN DRAWING				
EPN/DESCRIPTION											
CONT/PE#											
DATE											
DRN											
CHKD											
APPR											





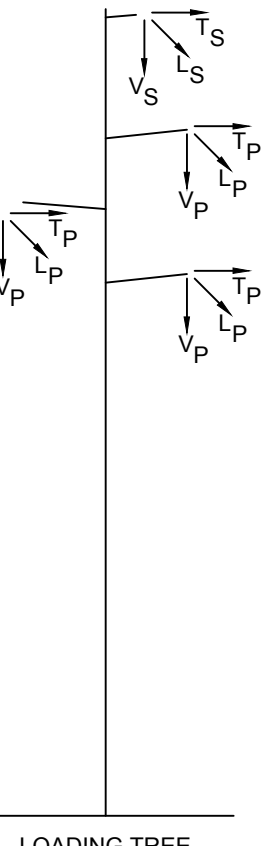
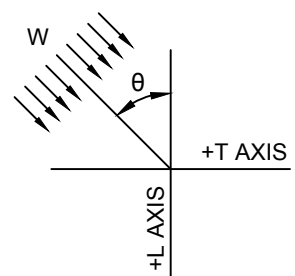
**PRELIMINARY - NOT  
FOR CONSTRUCTION**






STRUCTURE NAME: 10-SCDSP-LTW-002 115-KV AC CONDUCTOR: 1 - 795 KCMIL 26/7 "DRAKE" ACSR PER PHASE (9000# @ NESC HEAVY) OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY) WIND SPAN (FT): 800 WEIGHT SPAN (FT): 1000 LINE ANGLE: 0 - 2 DEGREES											
LOADING CASE				DESIGN LOADS							
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)
1	NESC 250B	0.00	0.50	39.50	1.69	1.34	0.00	3.74	1.96	0.00	10.00
2	NESC 250C	60.00	0.00	100.00	0.50	1.03	0.00	1.34	2.20	0.00	29.00
3	NESC 250D	15.00	1.00	39.50	2.38	0.94	0.00	4.11	1.27	0.00	4.00
4	NU EXTREME ICE	15.00	1.30	39.50	3.23	1.14	0.00	5.16	1.47	0.00	90.00
5	NESC 250B w/o OLF	0.00	0.50	39.50	1.13	0.61	0.00	2.49	0.90	0.00	4.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.50	1.13	0.59	0.00	2.49	0.80	0.00	4.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.50	1.13	0.50	5.50	2.49	0.68	6.75	4.00
8	CONSTRUCTION	30.00	0.00	30.00	3.68	0.30	0.27	6.14	0.58	0.48	3.45
9	DEFLECTION	60.00	0.00	0.00	0.50	0.10	0.00	1.34	0.18	0.00	90.00
10	MAINTENANCE	60.00	0.00	0.00	2.80	0.21	0.00	4.49	0.36	0.00	90.00

- REFERENCES:
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

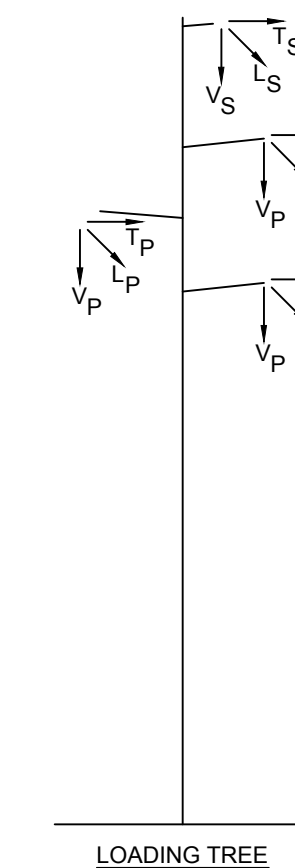
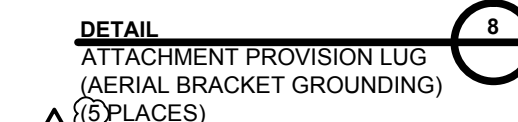
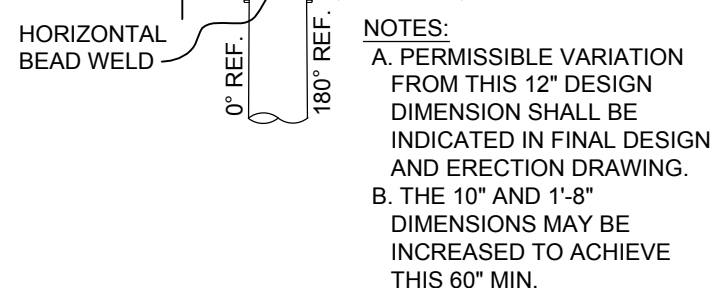
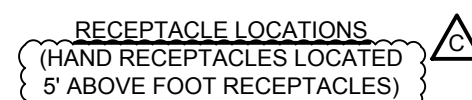
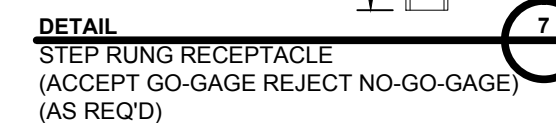
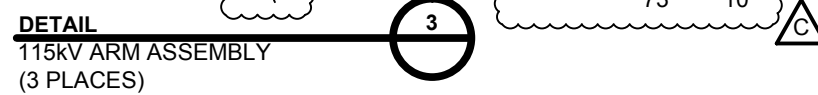
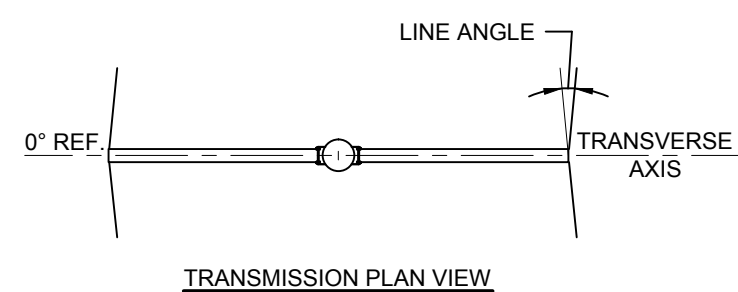


- NOTES:
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (TBD).
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  - CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - STEEL PLATE, A MINIMUM OF 1/4" THICKNESS GREATER THAN THAT REQUIRED FOR COLUMN STRENGTH SHALL BE IN PLACE IN THE AREA 3'-0" ABOVE AND 5'-0" BELOW THE NOMINAL GROUND LINE.
  - APPLY COAL TAR EPOXY ON INSIDE AND OUTSIDE OF POLE FROM BUTT OF POLE TO 12" ABOVE TOP OF CORROSION COLLAR.
  - BELOW GROUND CORROSION PROTECTION COATING MATERIAL SHALL BE SUPPLIED (ONE QUART PER TWO STRUCTURES) TO "TOUCH UP" SCRATCHES OCCURRING IN SHIPPING AND HANDLING. A COPY OF THE MSDS SHEET SHALL BE SUPPLIED WITH THE "TOUCH UP" MATERIALS.
  - FALL PROTECTION VANGS FOR CLIMBING AND WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  - 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.

CONTRACT SERVICES								 THE NORTHERN PASS		C	
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								ENGINEER CET			
								CHECKED TAB			
								APPROVED			
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DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR					
C	MISC. UPDATES		5/29/15	MSP							
B	MISC. REVISIONS		5/8/15	BLH							
A	RELEASE FOR RFP BID		5/1/15	BLH							

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LOADING CASE					DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.50	1.69	1.34	0.00	3.74	1.96	0.00	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.50	1.03	0.00	1.34	2.20	0.00	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.50	2.38	0.94	0.00	4.11	1.27	0.00	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.30	39.50	3.23	1.14	0.00	5.16	1.47	0.00	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.50	1.13	0.61	0.00	2.49	0.90	0.00	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.50	1.13	0.59	0.00	2.49	0.80	0.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.50	1.13	0.50	2.49	0.68	0.68	6.75	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	30.00	3.68	0.30	0.27	6.14	0.58	0.48	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.50	0.10	0.00	1.34	0.18	0.00	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.80	0.21	0.00	4.49	0.36	0.00	0.00	90.00	2.00

- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE : SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ATTACHMENT PROVISIONS FOR GOUNDING AND SIGNS: SKETCH F
  7. LIFTING VANG PROVISIONS: SKETCH J + K
  8. FALL PROTECTION VANGS: SKETCH N + Q
  9. JACKING NUT LOCATIONS: SKETCH I

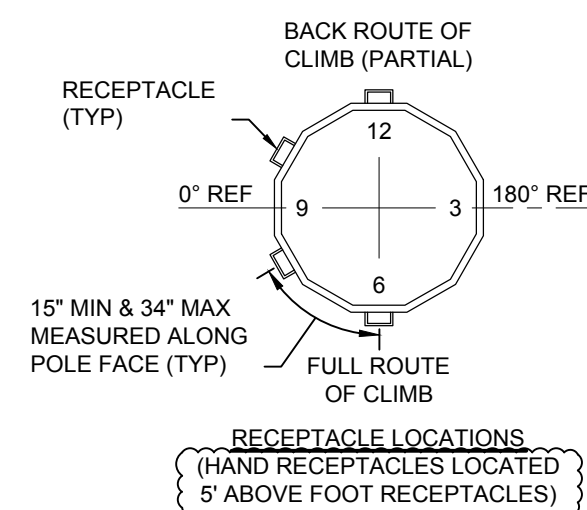
- NOTES:**

  1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TRUSS DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. **CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  16. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  17. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.

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**PRELIMINARY - NOT  
FOR CONSTRUCTION**





**PRELIMINARY - NOT  
FOR CONSTRUCTION**



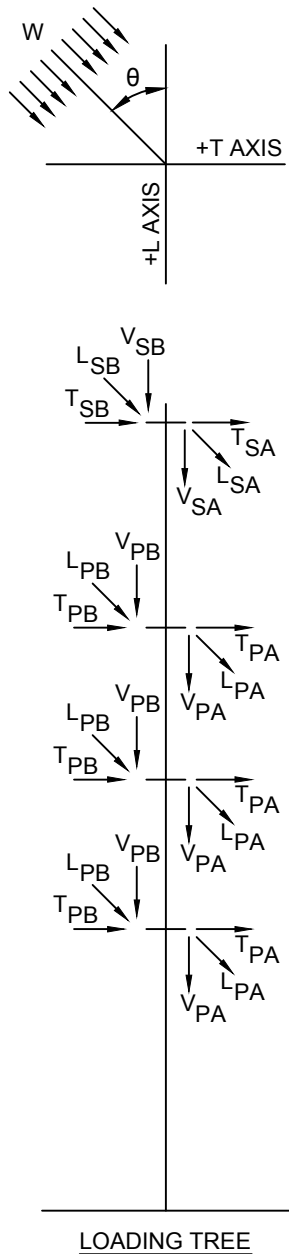






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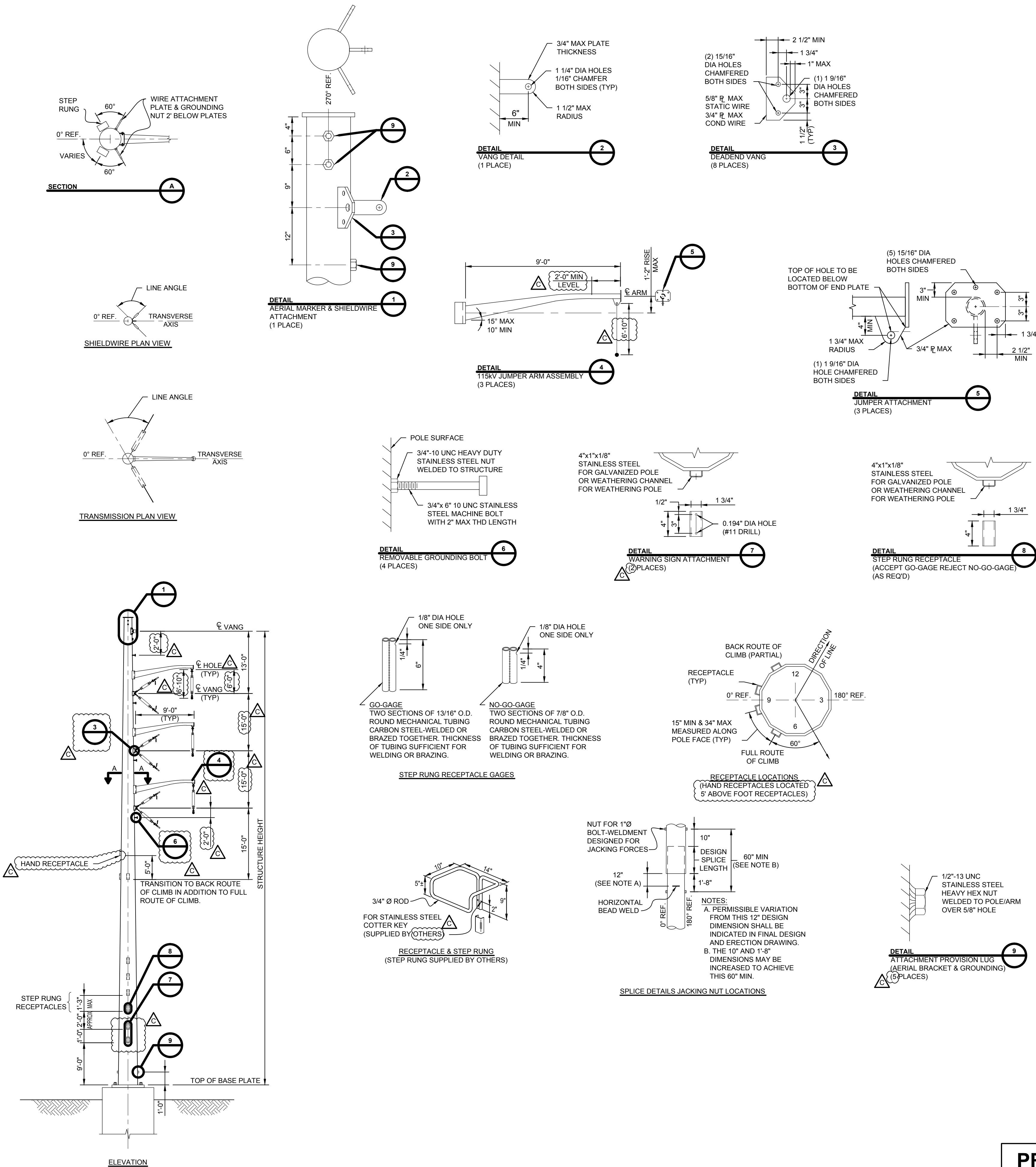
1. GROUNDING NUT: SKETCH B
2. STEP RUNG + RECEPTACLE : SKETCH E
3. GAGES FOR RECEPTACLE: SKETCH L
4. CLIMBING FACILITIES: SKETCH B
5. RECEPTACLE LOCATIONS: SKETCH C
6. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
7. LIFTING + GAGE PROVISIONS: SKETCH J + K
8. FALL PROTECTION VANGS: SKETCH N + Q
9. JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THE TA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-Axis AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE AT BROKEN INSTALLED.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (TBD).
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR AND LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.  
**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  13. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL BE PROJECTED ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  16. JUMPER ARMERS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  17. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  18. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
  19. 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

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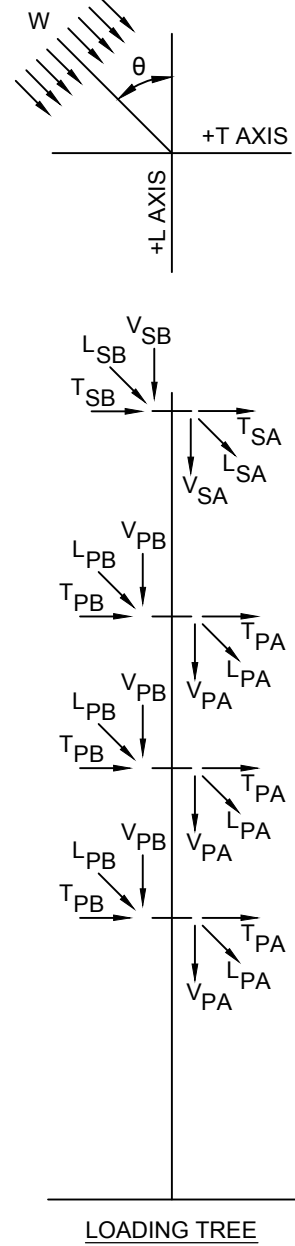




STRUCTURE NAME: 10-SCVSP-HDW-075  
115-KV AC CONDUCTOR: 1 - 795 KEMIL 26/7 "DRAKE" ACSR PER PHASE (9000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 375 WIND SPAN BACK (FT): 375  
WEIGHT SPAN AHEAD (FT): 725 WEIGHT SPAN BACK (FT): 725  
LINE ANGLE: 55 - 75 DEGREES


LOADING CASE				DESIGN LOADS															
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.25	6.33	8.54	1.25	6.33	-8.54	2.95	10.38	14.16	2.95	10.38	-14.16	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.38	3.15	4.00	0.38	3.15	-4.00	1.07	6.33	7.94	1.07	6.33	-7.94	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.74	5.09	6.97	1.74	5.09	-6.97	3.14	8.01	11.10	3.14	8.01	-11.10	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.36	6.24	8.54	2.36	6.24	-8.54	3.90	9.38	13.01	3.90	9.38	-13.01	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.83	3.74	5.17	0.83	3.74	-5.17	1.97	6.15	8.58	1.97	6.15	-8.58	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.83	3.54	4.88	0.83	3.54	-4.88	1.97	5.74	7.98	1.97	5.74	-7.98	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.83	3.54	4.88	0.83	0.19	0.00	1.97	5.74	7.98	1.97	0.26	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.98	1.40	0.24	1.91	3.24	-4.64	6.92	2.51	0.43	2.95	5.74	-8.19	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.38	1.80	2.62	0.38	1.80	-2.62	1.07	3.17	4.61	1.07	3.17	-4.61	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.55	3.60	5.25	2.55	3.60	-5.25	3.93	6.33	9.23	3.93	6.33	-9.23	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.38	2.70	3.93	0.38	2.70	-3.93	1.07	4.86	7.08	1.07	4.86	-7.08	0.00	90.00	1.00

- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  7. LIFTING VANG PROVISIONS: SKETCH J + K
  8. FALL PROTECTION VANGS: SKETCH N + Q
  9. JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (B/D).
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. CAUTION: "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  15. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  16. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  17. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  18. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  19. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
  20. 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

**PRELIMINARY - NOT FOR CONSTRUCTION**

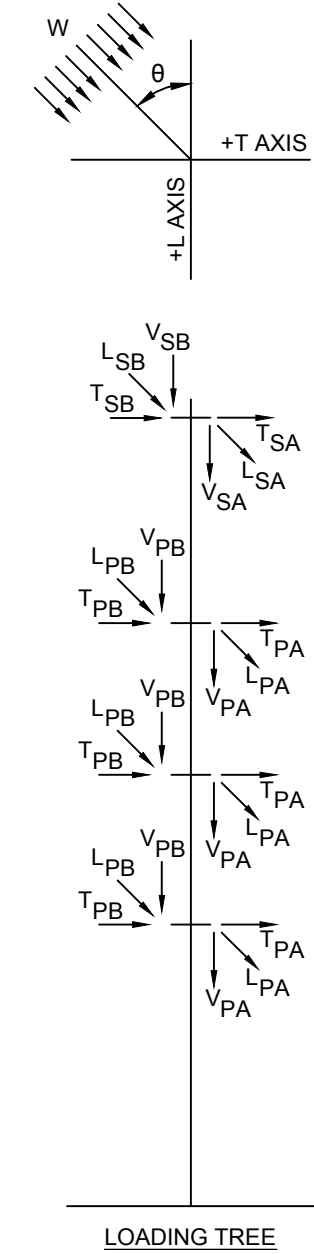
CONTRACT SERVICES								 THE NORTHERN PASS	C	
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										APPROVED
										DATE 5/1/15
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	115kV AC DEADEND 55-75° 10-SCVSP-HDW-075 LOAD & DESIGN DRAWING			
C	MISC. UPDATES		5/29/15	MSP						
B	MISC. REVISIONS		5/8/15	BLH						
A	RELEASE FOR RFP BID		5/1/15	BLH						
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	SCALE NTS	FILE: TSP-24.DWG IMAGE:	DRAWING NO. TSP-24-001	






**REFERENCES:**

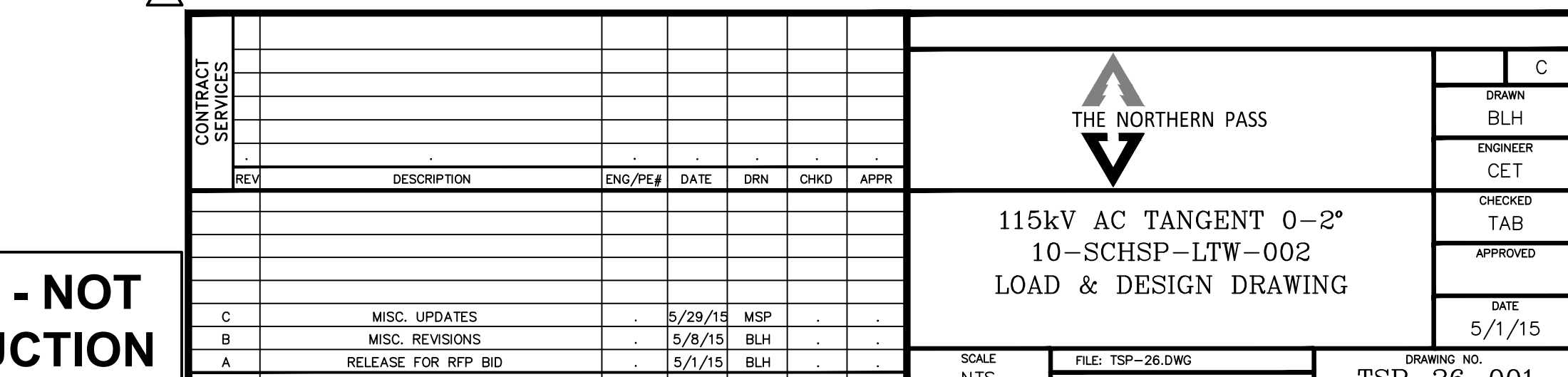
1. GROUNDING NUT: SKETCH B
2. STEP RUNG + RECEPTACLE : SKETCH E
3. GAGES FOR RECEPTACLE : SKETCH L
4. CLIMBING FACILITIES: SKETCH B
5. RECEPTACLE LOCATIONS: SKETCH C
6. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
7. LIFTING VANG PROVISIONS: SKETCH J + K
8. FALL PROTECTION VANGS: SKETCH N + Q
9. JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 0.3 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (Θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  7. SNUB ANGLES SHALL BE LIMITED TO A 45 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY STRUCTURES SHALL BE DESIGNED TO WITHSTAND THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.  
**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  13. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  16. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  17. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  18. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
  19. 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

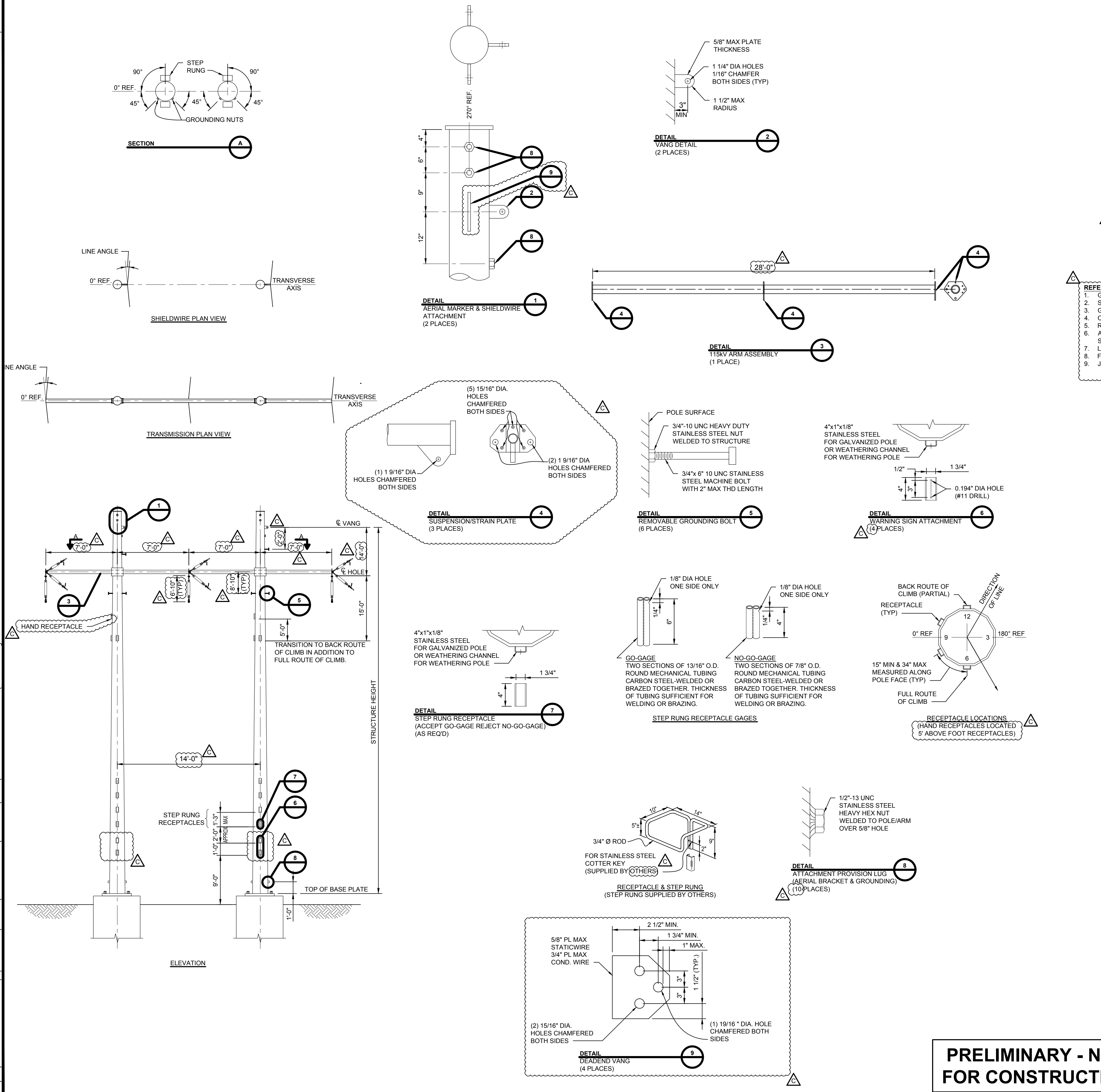
CONTRACT SERVICES										<div></div> <div>THE NORTHERN PASS</div>		C
											DRAWN BLH	
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											DATE 5/1/15	
	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	115kV AC DEADEND 0-60° 10-SCVSP-LDW-060 LOAD & DESIGN DRAWING				
	C	MISC. UPDATES	-	5/29/15	MSP	-	-					
	B	MISC. REVISIONS	-	5/8/15	BLH	-	-					
	A	RELEASE FOR RFP BID	-	5/1/15	BLH	-	-					
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR	SCALE NTS	FILE: TSP-25.DWG	IMAGE:	DRAWING NO.  TSP-25-001	





**PRELIMINARY - NOT  
FOR CONSTRUCTION**





STRUCTURE NAME: 10-SCHSP-LDW-015  
115-KV AC CONDUCTOR: 1 - 795 KCMIL 26/7 "DRAKE" ACSR PER PHASE (9000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 350 WIND SPAN BACK (FT): 350  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 0 - 15 DEGREES

LOADING CASE		DESIGN LOADS																	
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	1.70	9.62	0.84	1.70	-9.62	2.17	2.70	15.96	2.17	2.70	-15.96	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	0.97	4.51	0.26	0.97	-4.51	0.79	1.99	8.95	0.79	1.99	-8.95	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	1.32	7.85	1.15	1.32	-7.85	2.21	2.00	12.52	2.21	2.00	-12.52	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	1.61	9.63	1.56	1.61	-9.63	2.71	2.33	14.66	2.71	2.33	-14.66	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	0.94	5.83	0.56	0.94	-5.83	1.44	1.51	9.67	1.44	1.51	-9.67	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	0.89	5.50	0.56	0.89	-5.50	1.44	1.42	9.00	1.44	1.42	-9.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	0.89	5.50	0.56	0.18	0.00	1.44	1.42	9.00	1.44	0.25	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.44	0.27	1.74	0.73	-5.23	6.10	2.58	0.48	2.54	1.32	-9.24	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.26	0.39	2.96	0.26	0.39	-2.96	0.79	0.68	5.20	0.79	0.68	-5.20	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.33	0.77	5.92	2.33	0.77	-5.92	3.39	1.36	10.40	3.39	1.36	-10.40	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.26	0.58	4.43	0.26	0.58	-4.43	0.79	1.04	7.99	0.79	1.04	-7.99	0.00	90.00	1.00

**REFERENCES:**

- GROUNDING NUT: SKETCH B
- STEP RUNG + RECEPTACLE: SKETCH E
- GAGES FOR RECEPTACLE: SKETCH L
- CLIMBING FACILITIES: SKETCH B
- RECEPTACLE LOCATIONS: SKETCH C
- ATTACHMENT PROVISIONS FOR GOUNDING AND SIGNS: SKETCH F
- LIFTING VANG PROVISIONS: SKETCH J + K
- FALL PROTECTION VANGS: SKETCH N + Q
- JACKING NUT LOCATIONS: SKETCH I

**NOTES:**

- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
- V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
- W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
- THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
- THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
- SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
- MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 90°.
- ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
- STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
- TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
- PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
- CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
- VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
- POLE SPLICES SHALL USE FLANGED DESIGN.
- MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
- ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
- ARM AND X-BRACE SIZE, SHAPE AND MOUNTING HARDWARE REQUIRED SHALL BE DETERMINED AND FURNISHED BY POLE SUPPLIER.
- BRACING USE, CONFIGURATION AND LOCATIONS TO BE DETERMINED BY MANUFACTURER.
- FALL PROTECTION VANGS FOR CLIMBING AND WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND IN REFERENCE SKETCHES N + Q.
- 3'-2" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
- 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

**LOADING TREE**

**PRELIMINARY - NOT FOR CONSTRUCTION**

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
	C	MISC. UPDATES		5/29/15	MSP		
	B	MISC. REVISIONS		5/8/15	BLH		
	A	RELEASE FOR RFP BID		5/1/15	BLH		
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR

THE NORTHERN PASS

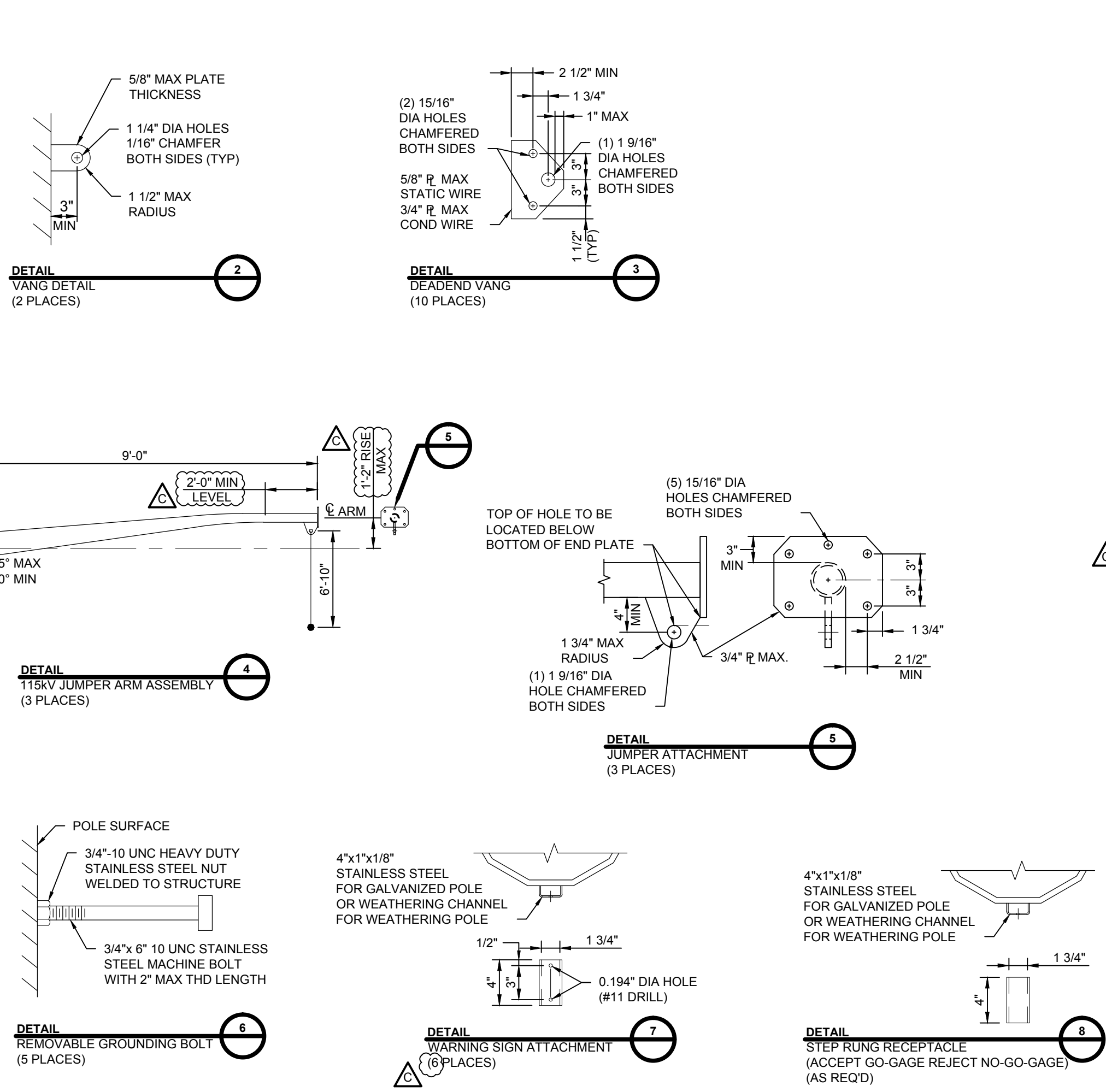
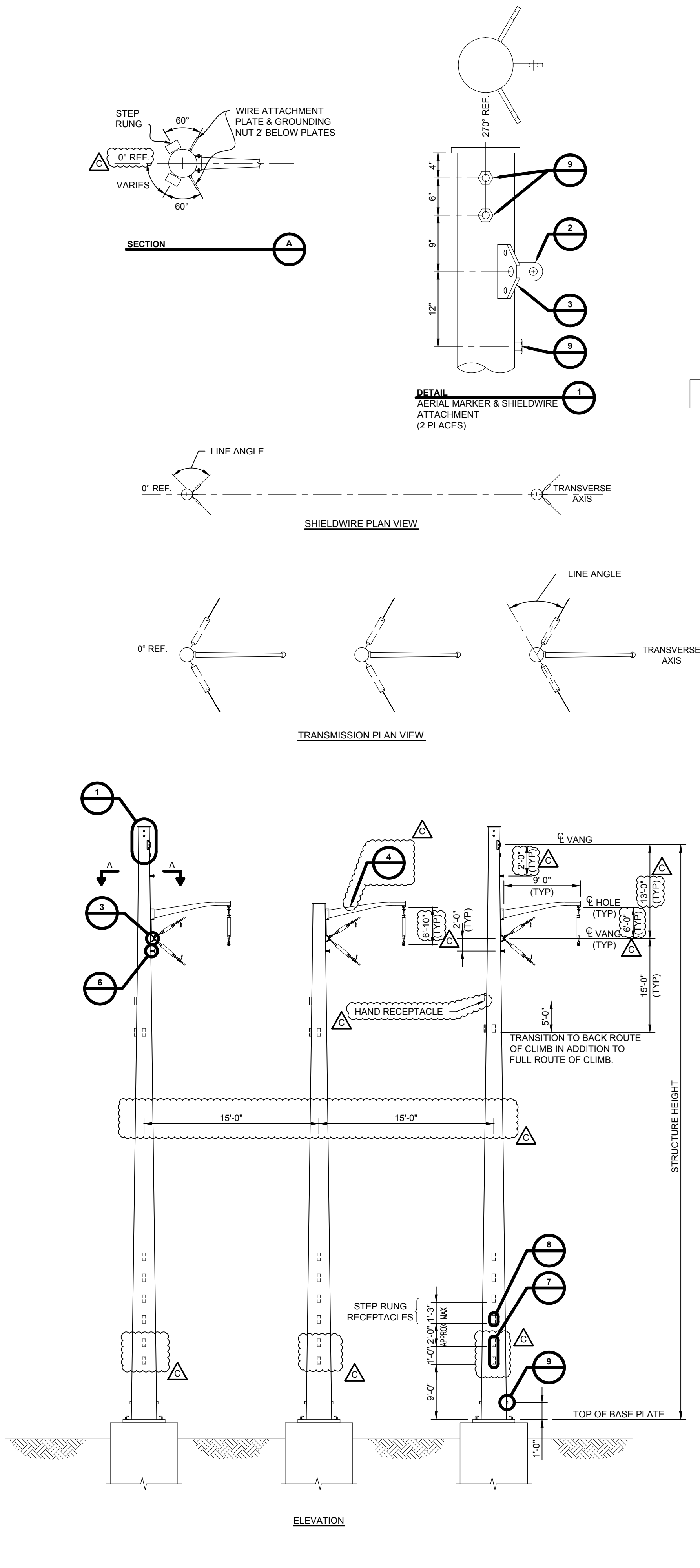
115kV AC DEADEND 0°-15°  
10-SCHSP-LDW-015  
LOAD & DESIGN DRAWING

SCALE: NTS  
FILE: TSP-27.DWG  
IMAGE:

DRAWING NO.: TSP-27-001

C	DRAWN	BLH
CET	ENGINEER	
TAB	CHECKED	
	APPROVED	
DATE	5/1/15	

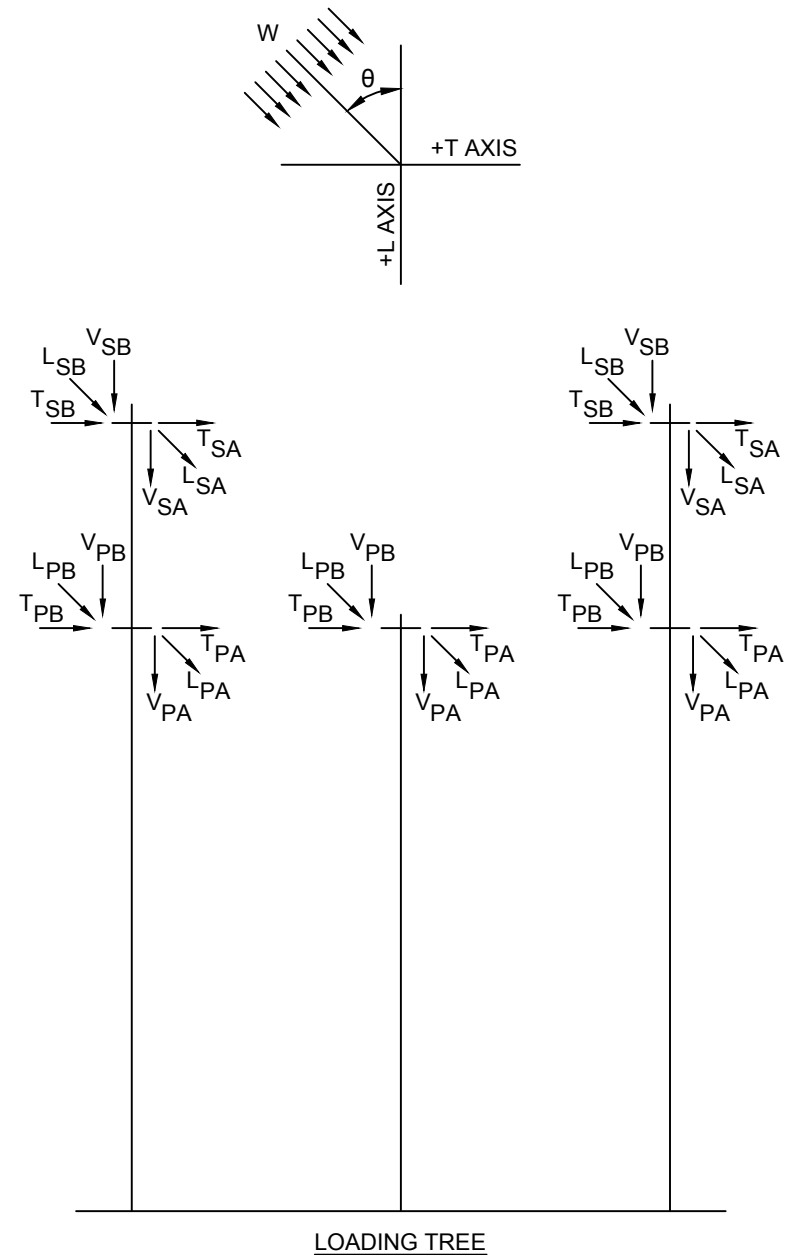




STRUCTURE NAME: 10-SCHSP-LDW-055  
115-KV AC CONDUCTOR: 1 - 795 KCMIL 26/7 "DRAKE" ACSR PER PHASE (9000# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 350 WIND SPAN BACK (FT): 350  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 0 - 55 DEGREES

LOADING CASE				DESIGN LOADS															
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	4.88	9.62	0.84	4.88	-9.62	2.17	7.99	15.96	2.17	7.99	-15.96	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	2.46	4.51	0.26	2.46	-4.51	0.79	4.96	8.95	0.79	4.96	-8.95	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	3.92	7.85	1.15	3.92	-7.85	2.21	6.14	12.52	2.21	6.14	-12.52	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	4.80	9.63	1.56	4.80	-9.63	2.71	7.19	14.66	2.71	7.19	-14.66	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	2.87	5.83	0.56	2.87	-5.83	1.44	4.71	9.67	1.44	4.71	-9.67	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	2.72	5.50	0.56	2.72	-5.50	1.44	4.40	9.00	1.44	4.40	-9.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	2.72	5.50	0.56	0.18	0.00	1.44	4.40	9.00	1.44	0.25	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.45	0.27	1.74	2.46	-5.23	6.10	2.60	0.48	2.54	4.38	-9.24	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.26	1.37	2.96	0.26	1.37	-2.96	0.79	2.40	5.20	0.79	2.40	-5.20	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.33	2.73	5.92	2.33	2.73	-5.92	3.39	4.80	10.40	3.39	4.80	-10.40	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.26	2.05	4.43	0.26	2.05	-4.43	0.79	3.69	7.99	0.79	3.69	-7.99	0.00	90.00	1.00

- REFERENCES:**
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I

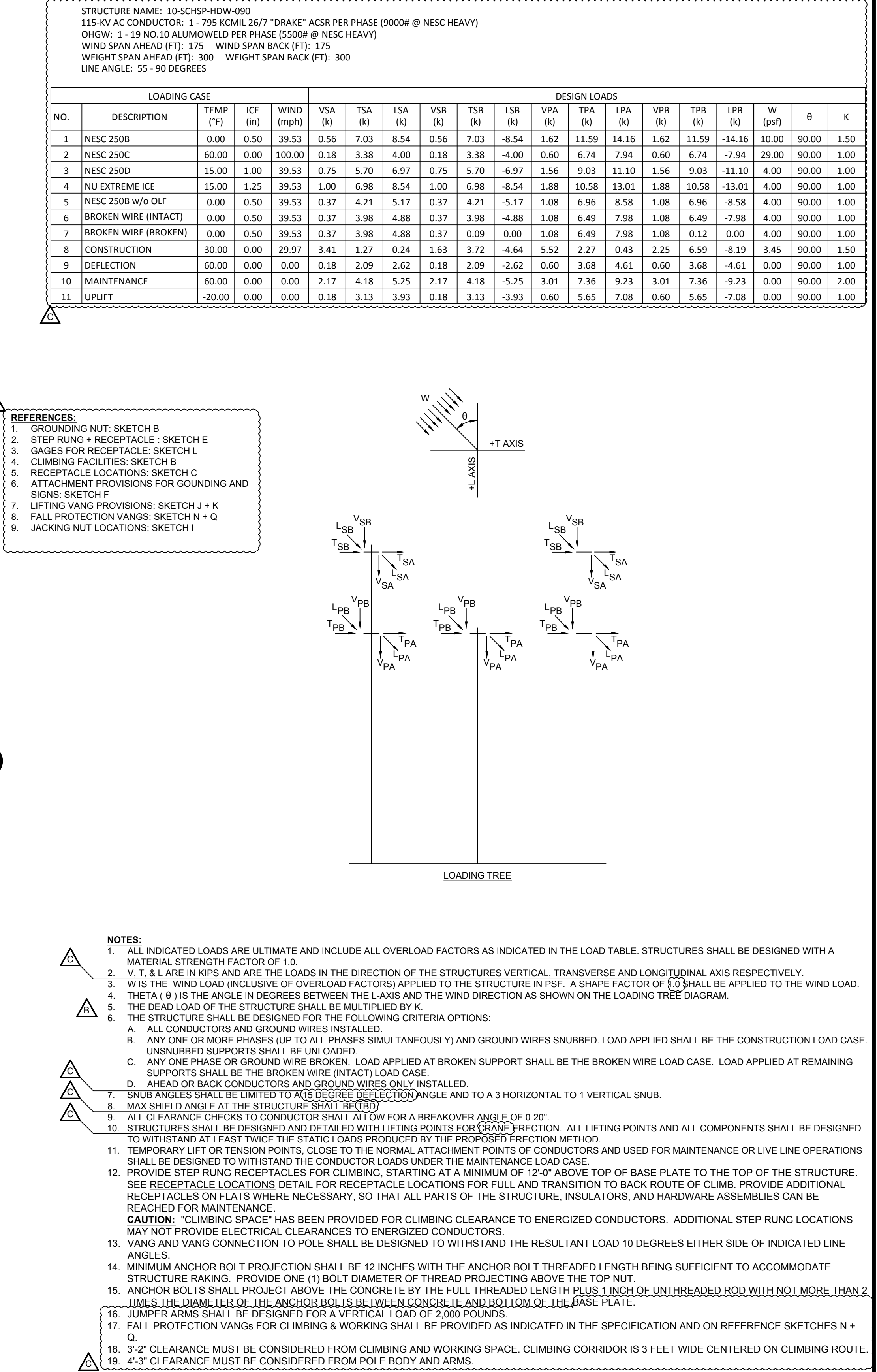


- NOTES:**
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  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
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  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
    - AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
  - SNUB ANGLES SHALL BE LIMITED TO A 60 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (TBD).
  - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  - PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.  
**CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  - VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  - MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  - JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  - FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  - 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
  - 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

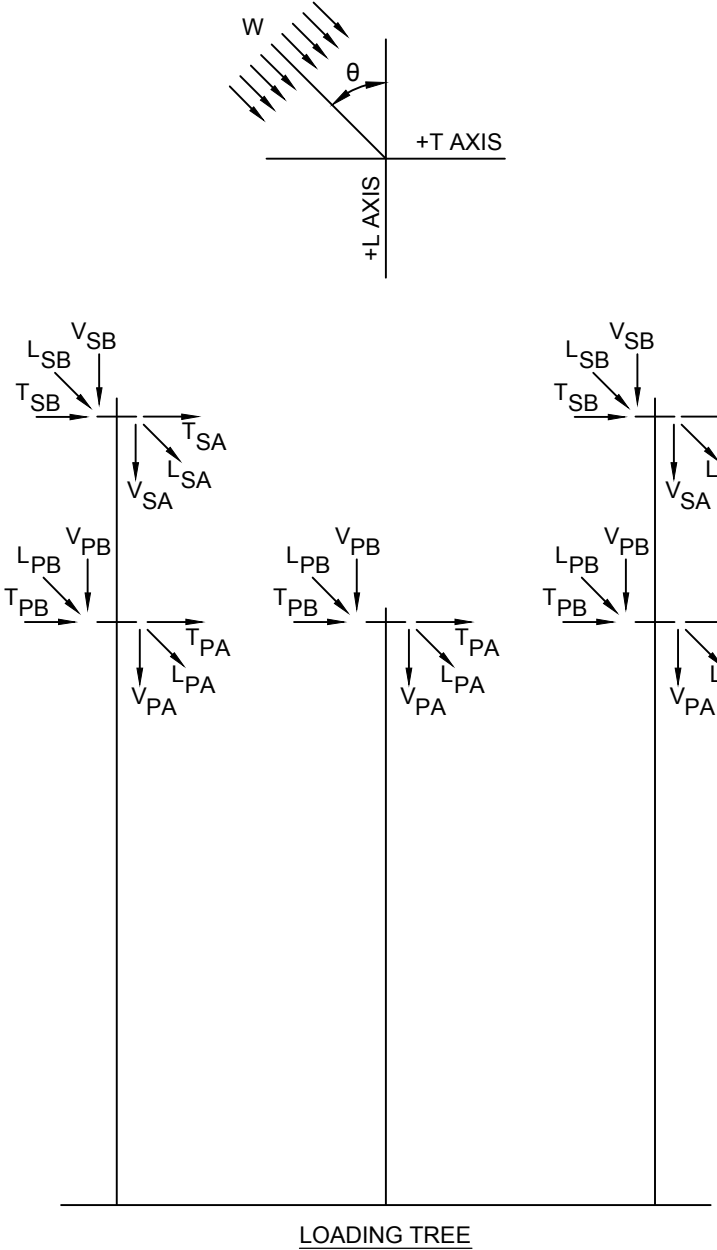
**PRELIMINARY - NOT FOR CONSTRUCTION**

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LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.56	7.03	8.54	0.56	7.03	-8.54	1.62	11.59	14.16	1.62	11.59	-14.16	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.18	3.38	4.00	0.18	3.38	-4.00	0.60	6.74	7.94	0.60	6.74	-7.94	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	0.75	5.70	6.97	0.75	5.70	-6.97	1.56	9.03	11.10	1.56	9.03	-11.10	4.00	90.00	1.00
4	NU EXTERCE ICE	15.00	1.25	39.53	1.00	6.98	8.54	1.00	6.98	-8.54	1.88	10.58	13.01	1.88	10.58	-13.01	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.37	4.21	5.17	0.37	4.21	-5.17	1.08	6.96	8.58	1.08	6.96	-8.58	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.37	3.98	4.88	0.37	3.98	-4.88	1.08	6.49	7.98	1.08	6.49	-7.98	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.37	3.98	4.88	0.37	0.09	0.00	1.08	6.49	7.98	1.08	0.12	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.41	1.27	0.24	1.63	3.72	-4.64	5.52	2.27	0.43	2.25	6.59	-8.19	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	1.18	2.09	2.62	0.18	2.09	-2.62	0.60	3.68	4.61	0.60	3.68	-4.61	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.17	4.18	5.25	2.17	4.18	-5.25	3.01	7.36	9.23	3.01	7.36	-9.23	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.18	3.13	3.93	0.18	3.13	-3.93	0.60	5.65	7.08	0.60	5.65	-7.08	0.00	90.00	1.00

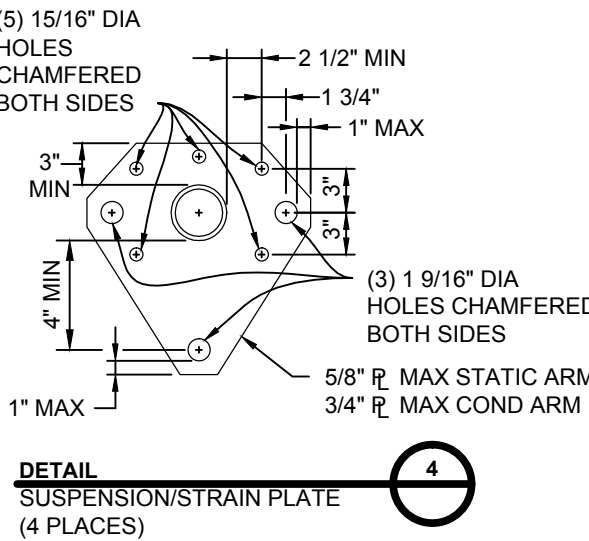
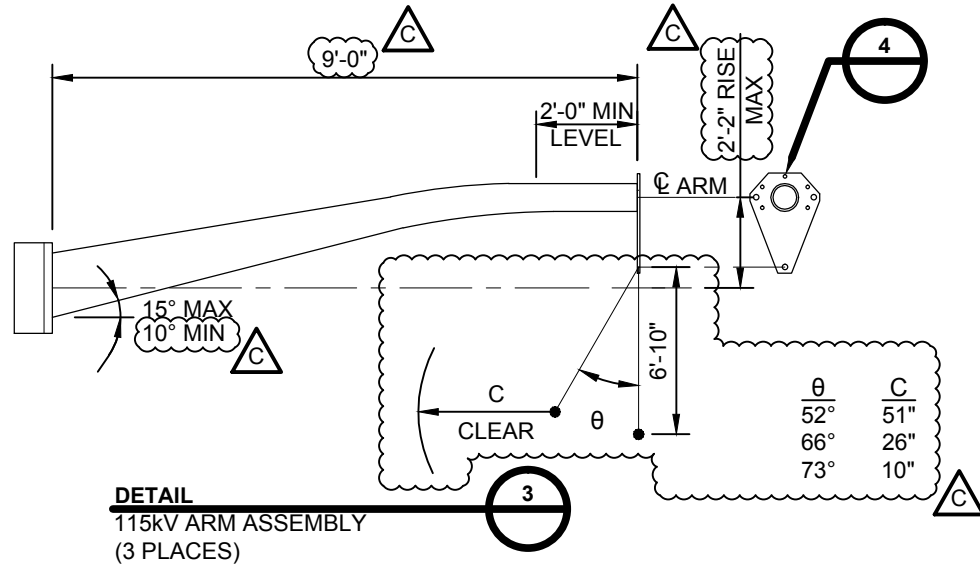
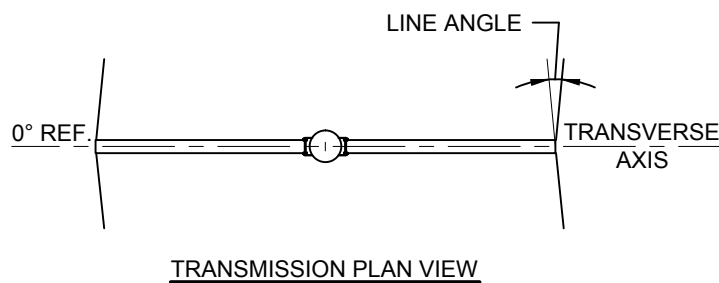
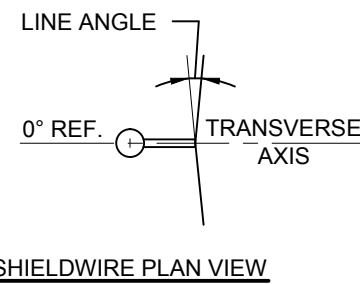
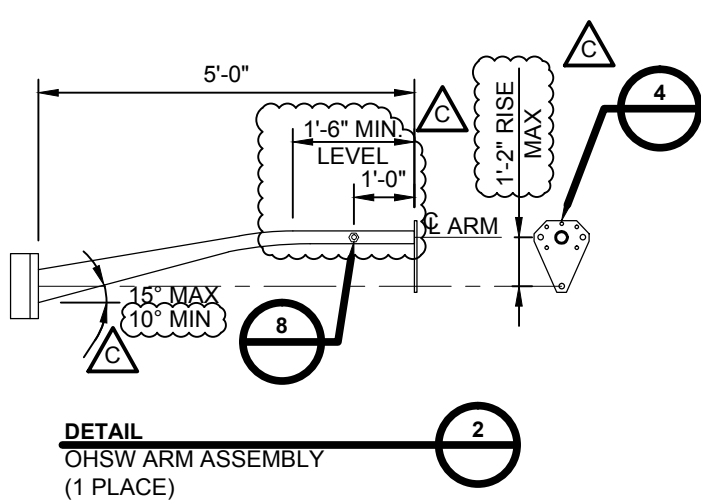
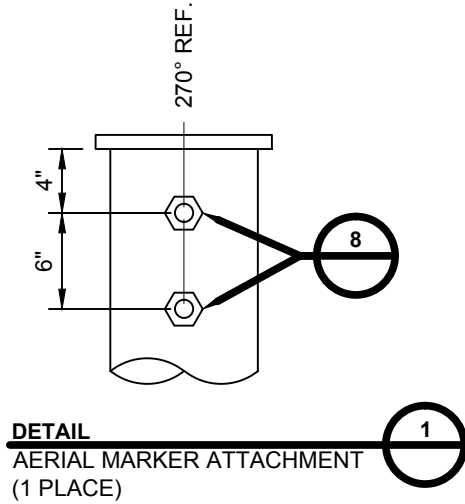
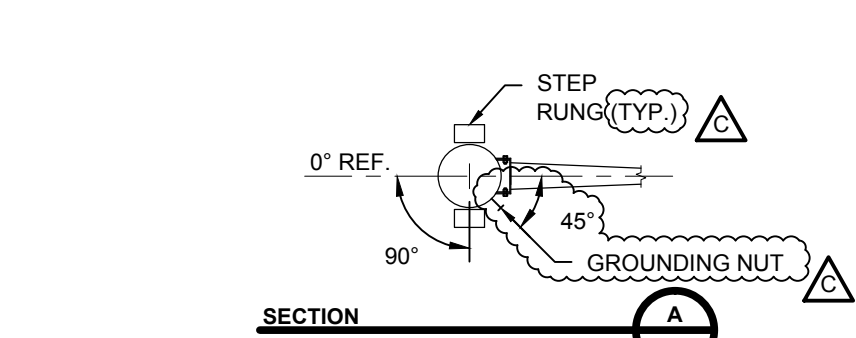


**NOTES:**

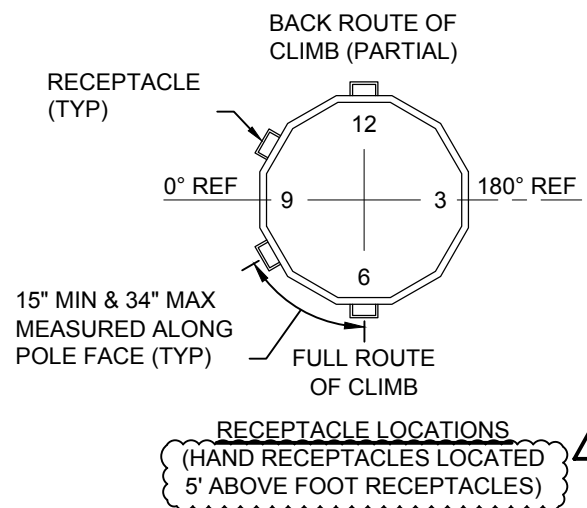
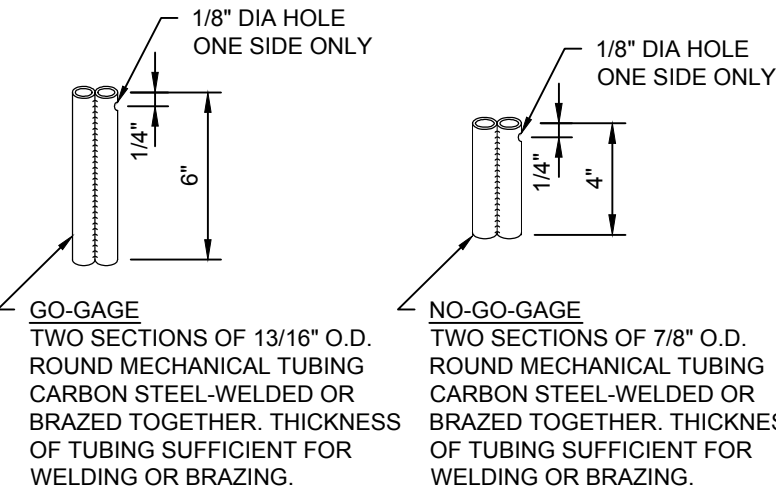
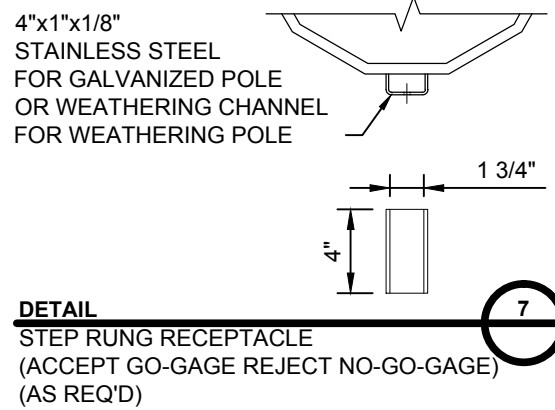
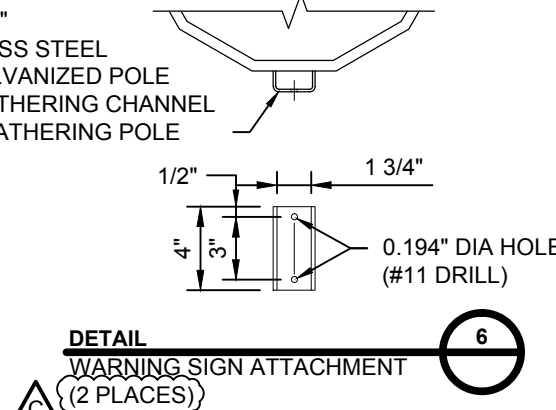
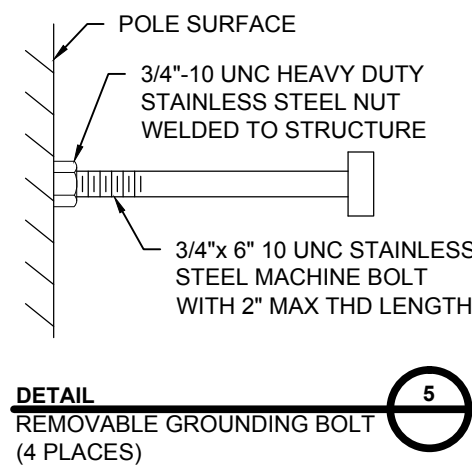
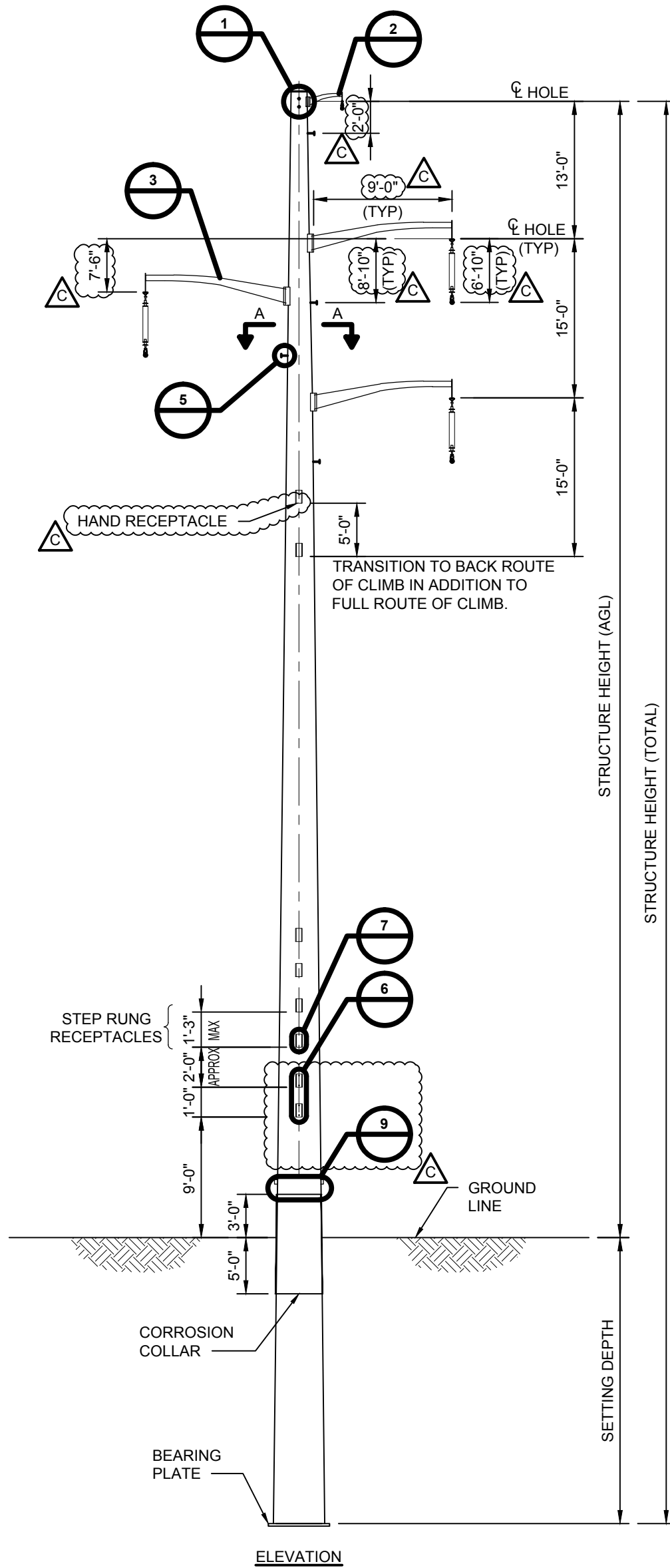
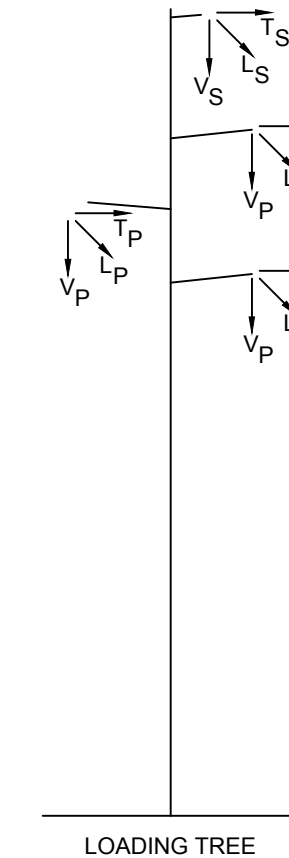
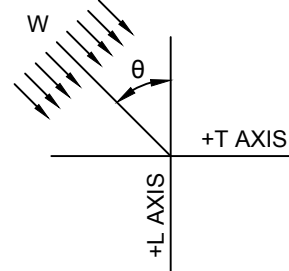
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2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
3. W IS THE WIND LOAD (IN KIPS) OF OVERLOAD FACTORS APPLIED TO THE STRUCTURE IN RSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
4. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
5. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
  - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
  - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE UNSNUBBED SUPPORTS SHALL BE UNLOADED.
  - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  - D. AHEAD OR BACK CONDUCTORS AND GROUND WIRES ONLY INSTALLED.
6. SNUB ANGLES SHALL BE LIMITED TO A 15 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
7. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE (B/D).
8. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
9. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND THE MAXIMUM LIFTING LOADS PROVIDED BY THE PROPOSED ERECTION METHOD.
10. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
11. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
12. **CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
13. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
14. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
15. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
16. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
17. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
18. 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
19. 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

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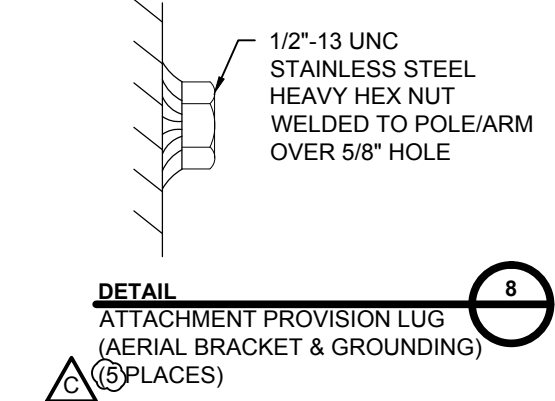
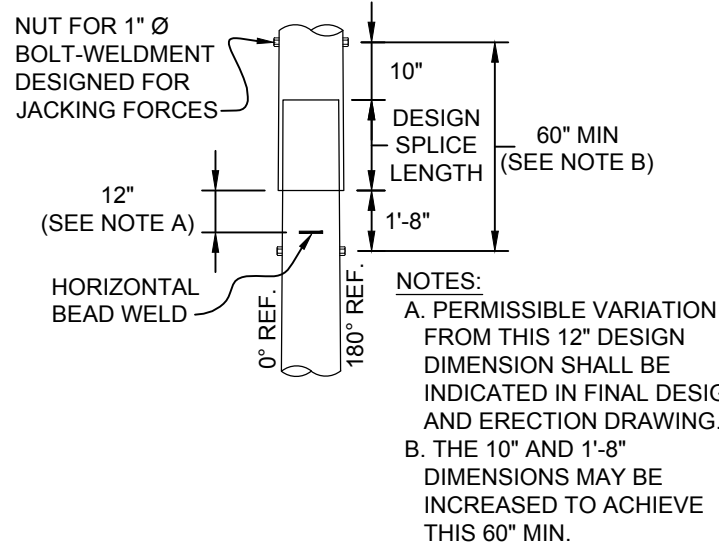
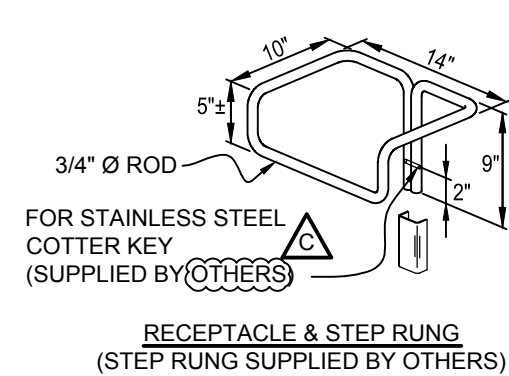




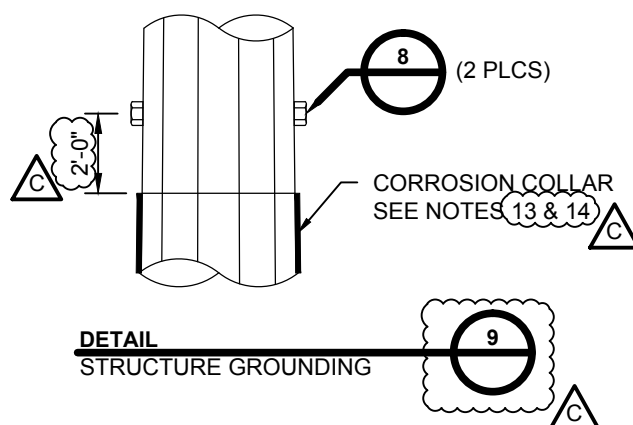
- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STEP RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  7. LIFTING VANG PROVISIONS: SKETCH J + K
  8. FALL PROTECTION VANGS: SKETCH N + Q
  9. JACKING NUT LOCATIONS: SKETCH I



STEP RUNG RECEPTACLE GAGES



SPLICE DETAILS JACKING NUT LOCATIONS



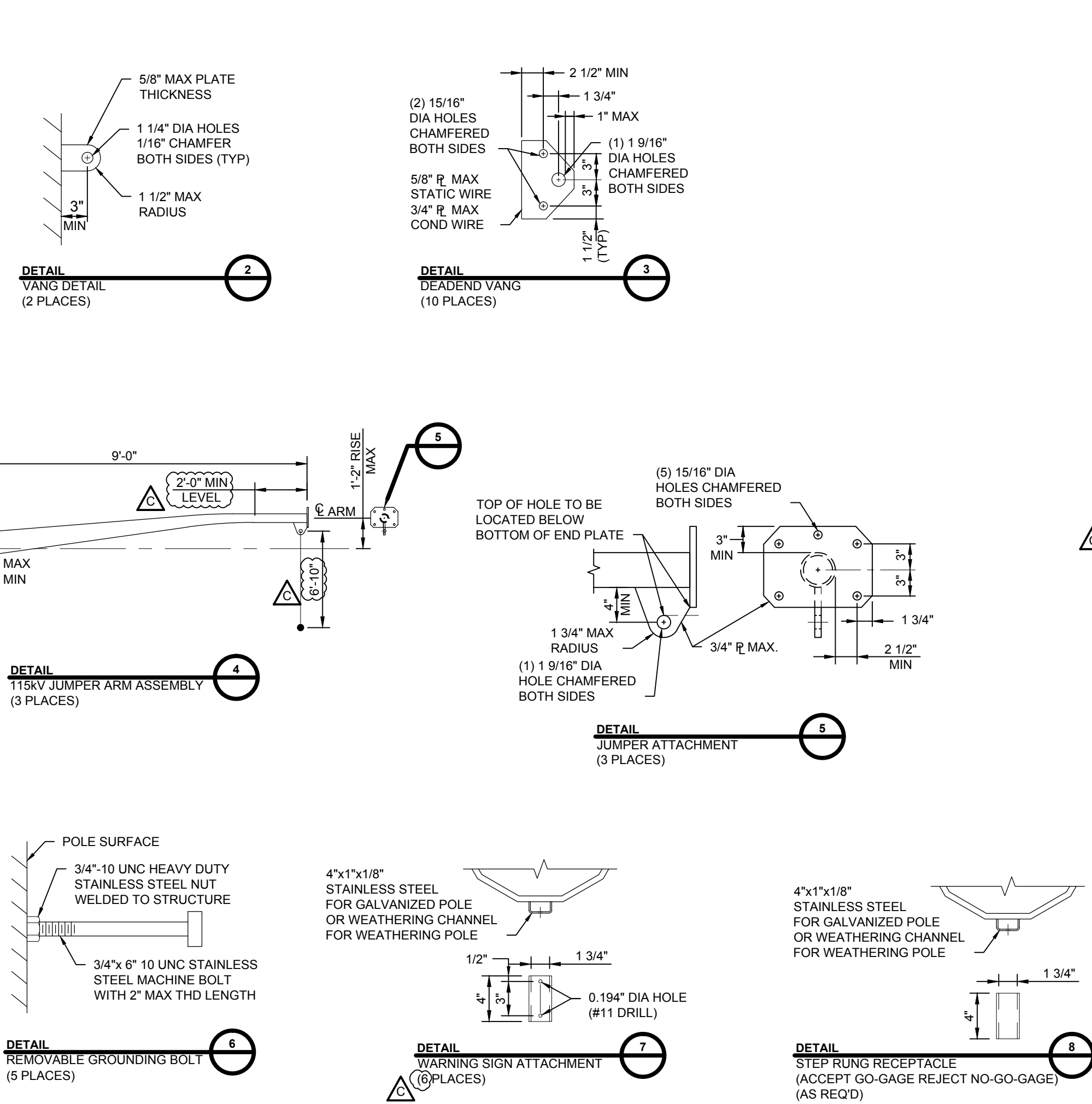
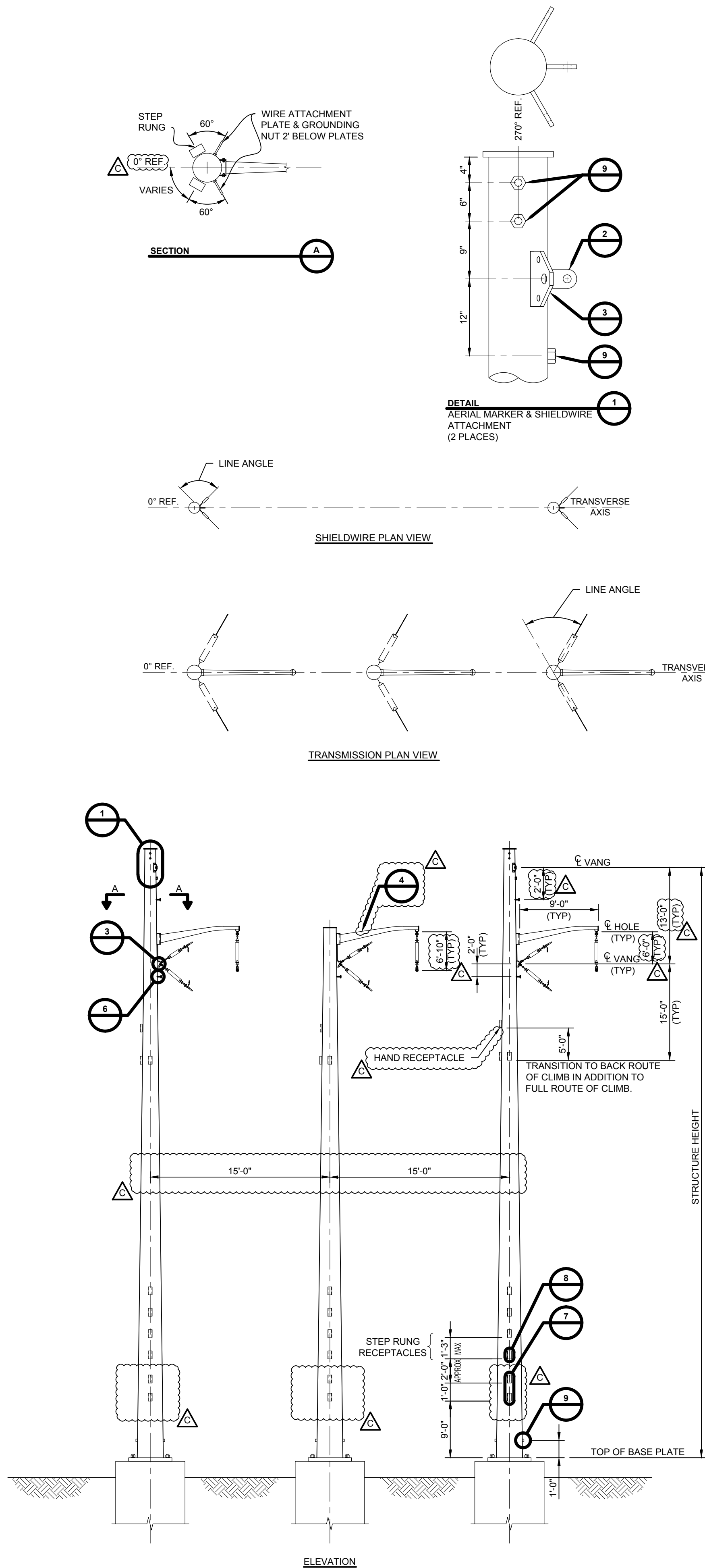
**PRELIMINARY - NOT FOR CONSTRUCTION**

STRUCTURE NAME: 10-SCDSP-LTW-002 115-KV AC CONDUCTOR: 1 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY) OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY) WIND SPAN (FT): 800 WEIGHT SPAN (FT): 1000 LINE ANGLE: 0 - 2 DEGREES												
LOADING CASE				DESIGN LOADS								
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VS (k)	TS (k)	LS (k)	VP (k)	TP (k)	LP (k)	W (psf)	θ
1	NESC 250B	0.00	0.50	39.53	1.69	1.34	0.00	5.15	2.39	0.00	10.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.50	1.03	0.00	2.04	2.97	0.00	29.00	1.00
3	NESC 250D	15.00	1.00	39.53	2.38	0.94	0.00	5.30	1.48	0.00	4.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	3.23	1.14	0.00	6.47	1.71	0.00	4.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	1.13	0.61	0.00	3.44	1.10	0.00	4.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	1.13	0.59	0.00	3.44	0.97	0.00	4.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	1.13	0.50	5.50	3.44	0.82	8.55	4.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.68	0.30	0.27	7.98	0.76	0.61	3.45	1.50
9	DEFLECTION	60.00	0.00	0.00	0.50	0.10	0.00	2.04	0.23	0.00	0.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.80	0.31	0.00	5.88	0.47	0.00	0.00	2.00

- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THE THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE OR GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 2 DEGREE LINE ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE GROUND LINE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. STEEL PLATE, A MINIMUM OF 1/4" THICKNESS GREATER THAN THAT REQUIRED FOR COLUMN STRENGTH SHALL BE IN PLACE IN THE AREA 3'-0" ABOVE AND 5'-0" BELOW THE NOMINAL GROUND LINE.
  14. APPLY COAL TAR EPOXY ON INSIDE AND OUTSIDE OF POLE FROM BUTT OF POLE TO 12" ABOVE TOP OF CORROSION COLLAR.
  15. BELOW GROUND CORROSION PROTECTION COATING MATERIAL SHALL BE SUPPLIED (ONE QUART PER TWO STRUCTURES) TO "TOUCH UP" SCRATCHES OCCURRING IN SHIPPING AND HANDLING. A COPY OF THE MSDS SHEET SHALL BE SUPPLIED WITH THE "TOUCH UP" MATERIALS.
  16. FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
  17. 3'-2" CLEARANCE SHALL BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR			C
										DRAWN
										BLH
										ENGINEER
								115kV AC TANGENT 0-2° 10-SCDSP-LTW-002 LOAD & DESIGN DRAWING		CET
										CHECKED
										TAB
										APPROVED
								SCALE NTS		DATE 5/1/15
C		MISC. UPDATES		5/29/15	MSP			FILE: TSP-30.DWG IMAGE:		DRAWING NO. TSP-30-001
B		MISC. REVISIONS		5/8/15	BLH					
A		RELEASE FOR RFP BID		5/1/15	BLH					
DWG REV		EPN/DESCRIPTION		CONT/PE#	DATE	DRN	CHKD	APPR		

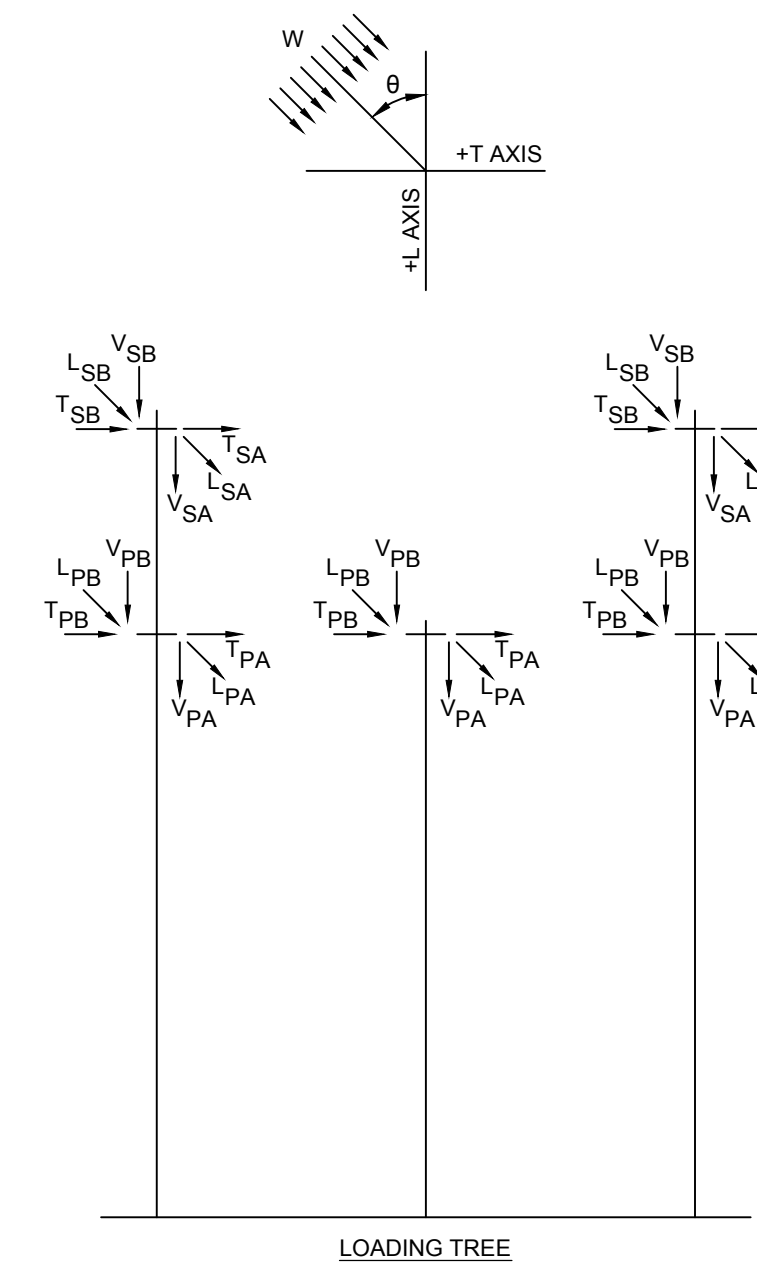




STRUCTURE NAME: 10-SCHSP-LDW-055  
115-KV AC CONDUCTOR: 1 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 350 WIND SPAN BACK (FT): 350  
WEIGHT SPAN AHEAD (FT): 475 WEIGHT SPAN BACK (FT): 475  
LINE ANGLE: 0 - 55 DEGREES

LOADING CASE						DESIGN LOADS													
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.84	4.88	9.62	0.84	4.88	-9.62	2.84	10.25	20.62	2.84	10.25	-20.62	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.26	2.46	4.51	0.26	2.46	-4.51	1.13	6.46	11.56	1.13	6.46	-11.56	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.15	3.92	7.85	1.15	3.92	-7.85	2.78	7.69	15.76	2.78	7.69	-15.76	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	1.56	4.80	9.63	1.56	4.80	-9.63	3.33	9.00	18.49	3.33	9.00	-18.49	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.56	2.87	5.83	0.56	2.87	-5.83	1.89	6.06	12.50	1.89	6.06	-12.50	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.56	2.72	5.50	0.56	2.72	-5.50	1.89	5.56	11.40	1.89	5.56	-11.40	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.56	2.72	5.50	0.56	0.18	0.00	1.89	5.56	11.40	1.89	0.29	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.65	1.45	0.27	1.74	2.46	-5.22	7.88	3.32	0.61	3.04	5.57	-11.74	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.26	1.37	2.96	0.26	1.37	-2.96	1.13	3.08	6.67	1.13	3.08	-6.67	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.33	2.73	5.92	2.33	2.73	-5.92	4.05	6.16	13.34	4.05	6.16	-13.34	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.26	2.05	4.43	0.26	2.05	-4.43	1.13	4.78	10.34	1.13	4.78	-10.34	0.00	90.00	1.00

- REFERENCES:**
- GROUNDING NUT: SKETCH B
  - STEP RUNG + RECEPTACLE: SKETCH E
  - GAGES FOR RECEPTACLE: SKETCH L
  - CLIMBING FACILITIES: SKETCH B
  - RECEPTACLE LOCATIONS: SKETCH C
  - ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  - LIFTING VANG PROVISIONS: SKETCH J + K
  - FALL PROTECTION VANGS: SKETCH N + Q
  - JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
- ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  - V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  - W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  - THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  - THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  - THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
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    - ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
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    - SNUB ANGLES SHALL BE LIMITED TO A 60 DEGREE DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
    - MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
    - ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°.
    - STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
    - TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
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    - ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
    - JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
    - FALL PROTECTION VANGS FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.
    - 3'-2" CLEARANCE MUST BE CONSIDERED FROM CLIMBING AND WORKING SPACE. CLIMBING CORRIDOR IS 3 FEET WIDE CENTERED ON CLIMBING ROUTE.
    - 4'-3" CLEARANCE MUST BE CONSIDERED FROM POLE BODY AND ARMS.

**PRELIMINARY - NOT FOR CONSTRUCTION**

CONTRACT SERVICES	REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR
C		MISC. UPDATES		5/29/15	MSP		
B		MISC. REVISIONS		5/8/15	BLH		
A		RELEASE FOR RFP BID		5/1/15	BLH		
DWG REV		EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR

THE NORTHERN PASS

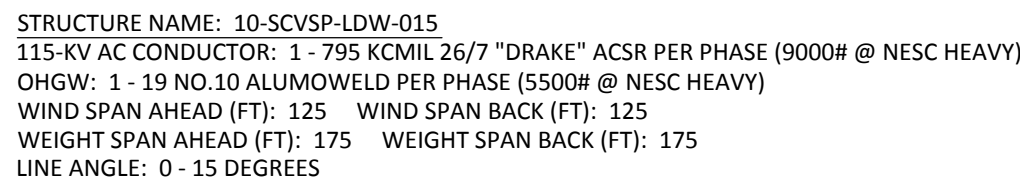
115kV AC DEADEND 0-55°  
10-SCHSP-LDW-055  
LOAD & DESIGN DRAWING

SCALE: NTS  
FILE: TSP-31.DWG  
IMAGE:

DRAWING NO.: TSP-31-001

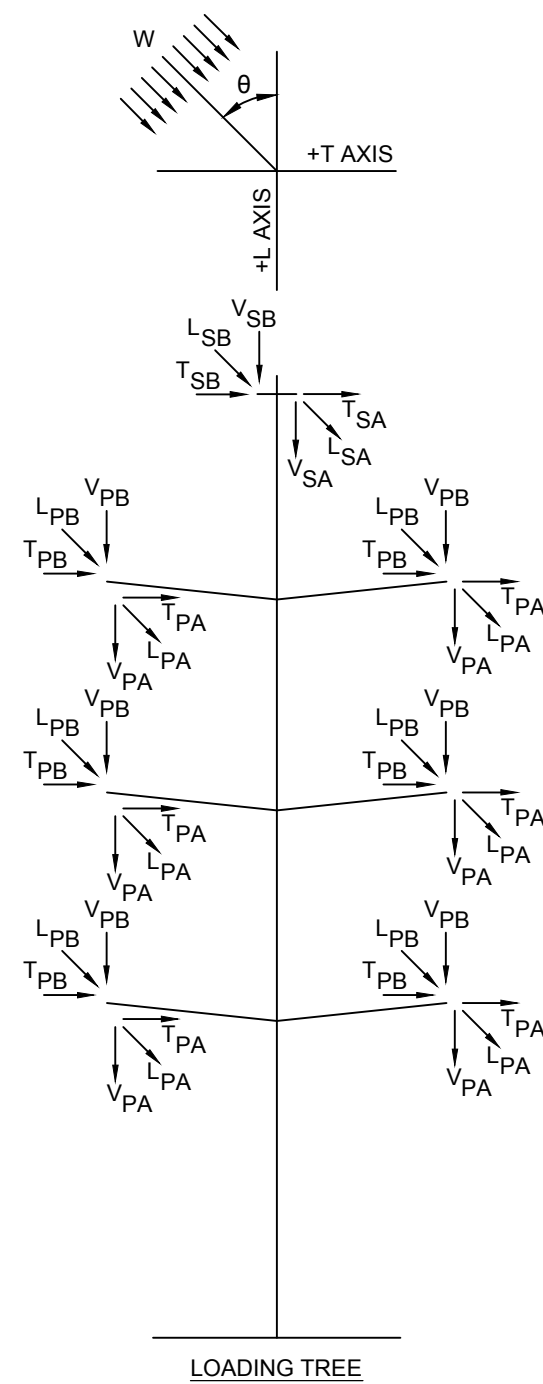
C	DRAWN	ENGINEER	CHECKED	APPROVED	DATE
BLH	CET	TAB			5/1/15





LOADING CASE					DESIGN LOADS														
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	0.36	1.41	9.62	0.36	1.41	-9.62	1.22	2.30	15.96	1.22	2.30	-15.96	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.13	0.72	4.51	0.13	0.72	-4.51	0.47	1.46	8.95	0.47	1.46	-8.95	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	0.46	1.13	7.85	0.46	1.13	-7.85	1.10	1.76	12.52	1.10	1.76	-12.52	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	0.61	1.38	9.63	0.61	1.38	-9.63	1.28	2.06	14.66	1.28	2.06	-14.66	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.24	0.82	5.83	0.24	0.82	-5.83	0.82	1.35	9.67	0.82	1.35	-9.67	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.24	0.78	5.50	0.24	0.78	-5.50	0.82	1.26	9.00	0.82	1.26	-9.00	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.24	0.78	5.50	0.24	0.06	0.00	0.82	1.26	9.00	0.82	0.09	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.24	1.37	0.27	1.54	0.70	-5.23	5.11	2.43	0.48	2.05	1.25	-9.24	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.13	0.39	2.96	0.13	0.39	-2.96	0.47	0.68	5.20	0.47	0.68	-5.20	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.06	0.77	5.92	2.06	0.77	-5.92	2.73	1.36	10.40	2.73	1.36	-10.40	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.13	0.58	4.43	0.13	0.58	-4.43	0.47	1.04	7.99	0.47	1.04	-7.99	0.00	90.00	1.00

- REFERENCES:**
1. CLIMBING FACILITIES: SKETCH B
  2. GROUNDING NUTS: SKETCH B
  3. HAND + FOOT RECEPTACLE LOCATIONS:  
SKETCH C
  4. STEP RUNG: SKETCH E
  5. ATTACHMENT PROVISIONS FOR SIGNS +  
GROUNDING: SKETCH F
  6. JACKING NUT LOCATIONS: SKETCH I
  7. LIFTING VANGS: SKETCH J + K
  8. STEP RUNG RECEPTACLE GAGES: SKETCH J
  9. FALL PROTECTION VANGS: SKETCH N + Q

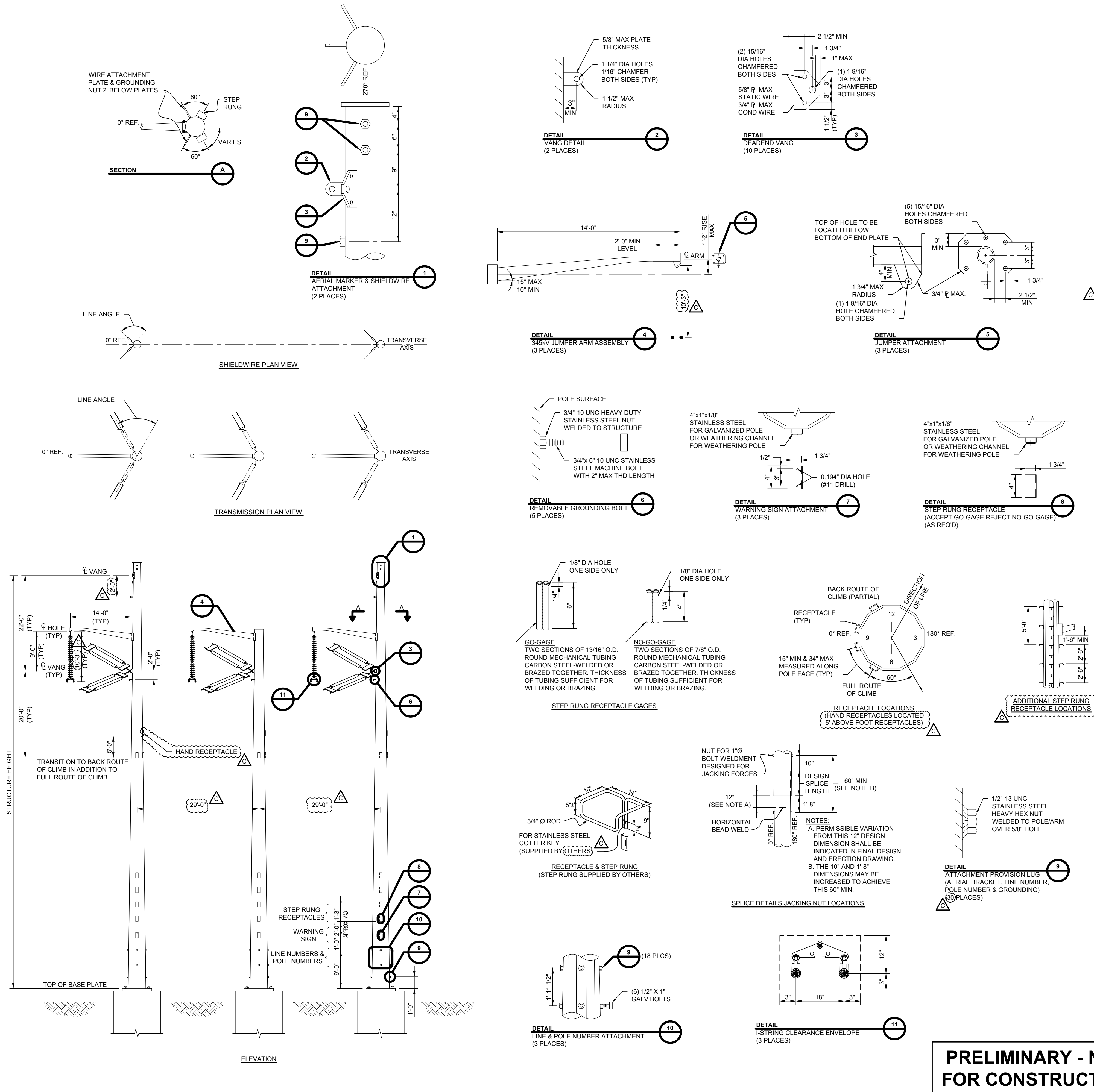


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  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 180°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKAWAY ANGLE OF 0-20°.
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**PRELIMINARY - NOT  
FOR CONSTRUCTION**

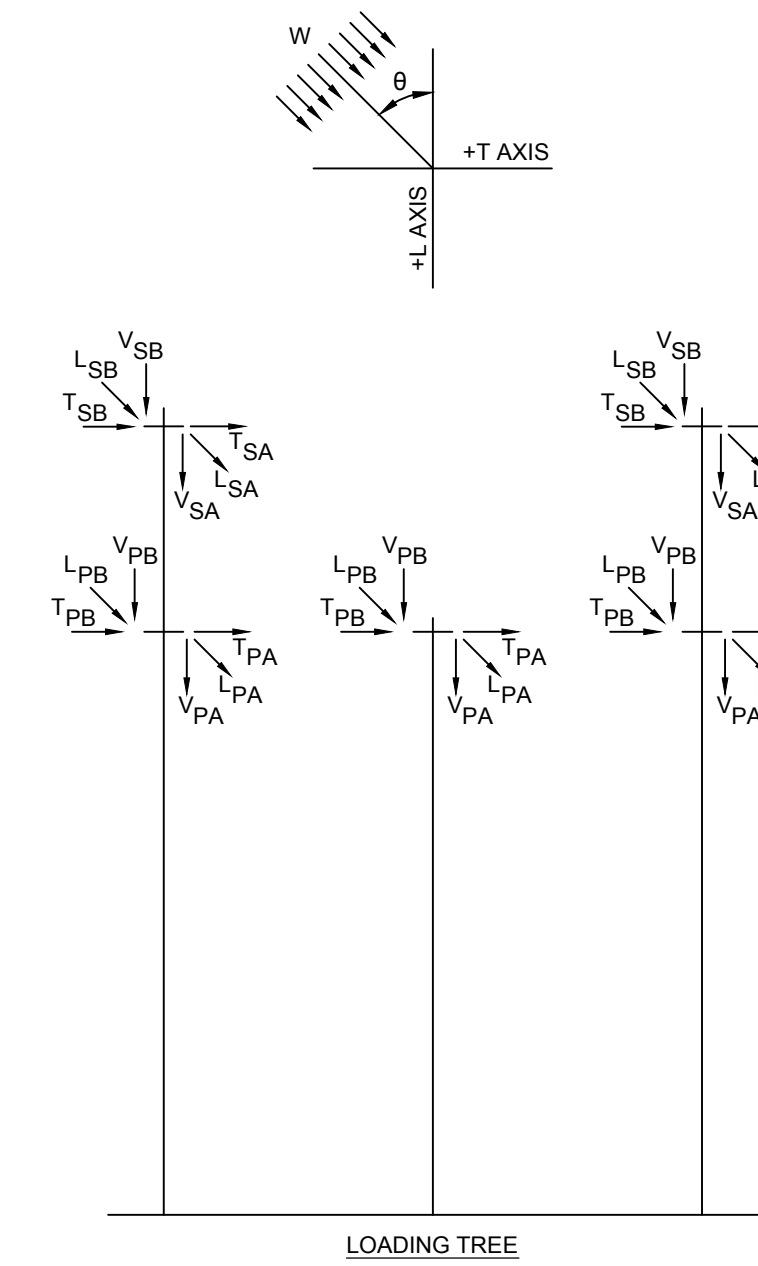




STRUCTURE NAME: 30-SCHSP-LSW-045  
345-KV AC CONDUCTOR: 2 - 1590 KCMIL 45/7 "LAPWING" ACSR PER PHASE (11400# @ NESC HEAVY)  
OHGW: 1 - 19 NO.10 ALUMOWELD PER PHASE (5500# @ NESC HEAVY)  
WIND SPAN AHEAD (FT): 475 WIND SPAN BACK (FT): 475  
WEIGHT SPAN AHEAD (FT): 625 WEIGHT SPAN BACK (FT): 625  
LINE ANGLE: 0 - 45 DEGREES

LOADING CASE				DESIGN LOADS															
NO.	DESCRIPTION	TEMP (°F)	ICE (in)	WIND (mph)	VSA (k)	TSA (k)	LSA (k)	VSB (k)	TSB (k)	LSB (k)	VPA (k)	TPA (k)	LPA (k)	VPB (k)	TPB (k)	LPB (k)	W (psf)	θ	K
1	NESC 250B	0.00	0.50	39.53	1.08	4.28	9.62	1.08	4.28	-9.62	7.87	17.76	41.24	7.87	17.76	-41.24	10.00	90.00	1.50
2	NESC 250C	60.00	0.00	100.00	0.33	2.24	4.51	0.33	2.24	-4.51	3.01	11.89	23.11	3.01	11.89	-23.11	29.00	90.00	1.00
3	NESC 250D	15.00	1.00	39.53	1.50	3.46	8.01	1.50	3.46	-8.01	7.58	13.17	31.53	7.58	13.17	-31.53	4.00	90.00	1.00
4	NU EXTREME ICE	15.00	1.25	39.53	2.04	4.27	9.92	2.04	4.27	-9.92	9.04	15.42	36.98	9.04	15.42	-36.98	4.00	90.00	1.00
5	NESC 250B w/o OLF	0.00	0.50	39.53	0.72	2.47	5.83	0.72	2.47	-5.83	5.25	10.36	24.99	5.25	10.36	-24.99	4.00	90.00	1.00
6	BROKEN WIRE (INTACT)	0.00	0.50	39.53	0.72	2.34	5.50	0.72	2.34	-5.50	5.25	9.52	22.80	5.25	9.52	-22.80	4.00	90.00	1.00
7	BROKEN WIRE (BROKEN)	0.00	0.50	39.53	0.72	2.34	5.50	0.72	0.24	0.00	5.25	9.52	22.80	5.25	0.79	0.00	4.00	90.00	1.00
8	CONSTRUCTION	30.00	0.00	29.97	3.85	1.50	0.27	1.85	2.07	-5.23	16.51	6.91	1.21	5.87	9.40	-23.49	3.45	90.00	1.50
9	DEFLECTION	60.00	0.00	0.00	0.33	1.13	2.96	0.33	1.13	-2.96	3.01	5.10	13.34	3.01	5.10	-13.34	0.00	90.00	1.00
10	MAINTENANCE	60.00	0.00	0.00	2.46	2.26	5.92	2.46	2.26	-5.92	7.83	10.21	26.68	7.83	10.21	-26.68	0.00	90.00	2.00
11	UPLIFT	-20.00	0.00	0.00	0.33	1.70	4.43	0.33	1.70	-4.43	3.01	7.92	20.69	3.01	7.92	-20.69	0.00	90.00	1.00

- REFERENCES:**
1. GROUNDING NUT: SKETCH B
  2. STED RUNG + RECEPTACLE: SKETCH E
  3. GAGES FOR RECEPTACLE: SKETCH L
  4. CLIMBING FACILITIES: SKETCH B
  5. RECEPTACLE LOCATIONS: SKETCH C
  6. ADDITIONAL RECEPTACLE LOCATION: SKETCH D
  7. ATTACHMENT PROVISIONS FOR GROUNDING AND SIGNS: SKETCH F
  8. LIFTING VANG PROVISIONS: SKETCH J + K
  9. FALL PROTECTION VANGS: SKETCH N + Q
  10. JACKING NUT LOCATIONS: SKETCH I



- NOTES:**
1. ALL INDICATED LOADS ARE ULTIMATE AND INCLUDE ALL OVERLOAD FACTORS AS INDICATED IN THE LOAD TABLE. STRUCTURES SHALL BE DESIGNED WITH A MATERIAL STRENGTH FACTOR OF 1.0.
  2. V, T, & L ARE IN KIPS AND ARE THE LOADS IN THE DIRECTION OF THE STRUCTURES VERTICAL, TRANSVERSE AND LONGITUDINAL AXIS RESPECTIVELY.
  3. W IS THE WIND LOAD (INCLUSIVE OF OVERLOAD FACTORS) APPLIED TO THE STRUCTURE IN PSF. A SHAPE FACTOR OF 1.0 SHALL BE APPLIED TO THE WIND LOAD.
  4. THETA (θ) IS THE ANGLE IN DEGREES BETWEEN THE L-AXIS AND THE WIND DIRECTION AS SHOWN ON THE LOADING TREE DIAGRAM.
  5. THE DEAD LOAD OF THE STRUCTURE SHALL BE MULTIPLIED BY K.
  6. THE STRUCTURE SHALL BE DESIGNED FOR THE FOLLOWING CRITERIA OPTIONS:
    - A. ALL CONDUCTORS AND GROUND WIRES INSTALLED.
    - B. ANY ONE OR MORE PHASES (UP TO ALL PHASES SIMULTANEOUSLY) AND GROUND WIRES SNUBBED. LOAD APPLIED SHALL BE THE CONSTRUCTION LOAD CASE. UNSNUBBED SUPPORTS SHALL BE UNLOADED.
    - C. ANY ONE PHASE AND GROUND WIRE BROKEN. LOAD APPLIED AT BROKEN SUPPORT SHALL BE THE BROKEN WIRE LOAD CASE. LOAD APPLIED AT REMAINING SUPPORTS SHALL BE THE BROKEN WIRE (INTACT) LOAD CASE.
  7. SNUB ANGLES SHALL BE LIMITED TO A 15° DEFLECTION ANGLE AND TO A 3 HORIZONTAL TO 1 VERTICAL SNUB.
  8. MAX SHIELD ANGLE AT THE STRUCTURE SHALL BE 15°.
  9. ALL CLEARANCE CHECKS TO CONDUCTOR SHALL ALLOW FOR A BREAKOVER ANGLE OF 0-20°. CLEARANCES MUST BE CHECKED TO SUBCONDUCTOR ENVELOPE SHOWN IN DETAIL 11.
  10. STRUCTURES SHALL BE DESIGNED AND DETAILED WITH LIFTING POINTS FOR CRANE ERECTION. ALL LIFTING POINTS AND ALL COMPONENTS SHALL BE DESIGNED TO WITHSTAND AT LEAST TWICE THE STATIC LOADS PRODUCED BY THE PROPOSED ERECTION METHOD.
  11. TEMPORARY LIFT OR TENSION POINTS, CLOSE TO THE NORMAL ATTACHMENT POINTS OF CONDUCTORS AND USED FOR MAINTENANCE OR LIVE LINE OPERATIONS SHALL BE DESIGNED TO WITHSTAND THE CONDUCTOR LOADS UNDER THE MAINTENANCE LOAD CASE.
  12. PROVIDE STEP RUNG RECEPTACLES FOR CLIMBING, STARTING AT A MINIMUM OF 12'-0" ABOVE TOP OF BASE PLATE TO THE TOP OF THE STRUCTURE. SEE RECEPTACLE LOCATIONS DETAIL FOR RECEPTACLE LOCATIONS FOR FULL AND TRANSITION TO BACK ROUTE OF CLIMB. PROVIDE ADDITIONAL RECEPTACLES ON FLATS WHERE NECESSARY, SO THAT ALL PARTS OF THE STRUCTURE, INSULATORS, AND HARDWARE ASSEMBLIES CAN BE REACHED FOR MAINTENANCE.
  13. **CAUTION:** "CLIMBING SPACE" HAS BEEN PROVIDED FOR CLIMBING CLEARANCE TO ENERGIZED CONDUCTORS. ADDITIONAL STEP RUNG LOCATIONS MAY NOT PROVIDE ELECTRICAL CLEARANCES TO ENERGIZED CONDUCTORS.
  14. VANG AND VANG CONNECTION TO POLE SHALL BE DESIGNED TO WITHSTAND THE RESULTANT LOAD 10 DEGREES EITHER SIDE OF INDICATED LINE ANGLES.
  15. MINIMUM ANCHOR BOLT PROJECTION SHALL BE 12 INCHES WITH THE ANCHOR BOLT THREADED LENGTH BEING SUFFICIENT TO ACCOMMODATE STRUCTURE RAKING. PROVIDE ONE (1) BOLT DIAMETER OF THREAD PROJECTING ABOVE THE TOP NUT.
  16. ANCHOR BOLTS SHALL PROJECT ABOVE THE CONCRETE BY THE FULL THREADED LENGTH PLUS 1 INCH OF UNTHREADED ROD WITH NOT MORE THAN 2 TIMES THE DIAMETER OF THE ANCHOR BOLTS BETWEEN CONCRETE AND BOTTOM OF THE BASE PLATE.
  17. JUMPER ARMS SHALL BE DESIGNED FOR A VERTICAL LOAD OF 2,000 POUNDS.
  18. FALL PROTECTION VANG FOR CLIMBING & WORKING SHALL BE PROVIDED AS INDICATED IN THE SPECIFICATION AND ON REFERENCE SKETCHES N + Q.

**PRELIMINARY - NOT FOR CONSTRUCTION**

CONTRACT SERVICES						THE NORTHERN PASS		C	
REV	DESCRIPTION	ENG/PE#	DATE	DRN	CHKD	APPR	DRAWN	ENGINEER	CHECKED
C	MISC. UPDATES		5/27/15	MSP			BLH	CET	TAB
B	MISC. REVISIONS		5/8/15	BLH					
A	RELEASE FOR RFP BID		5/1/15	BLH					
DWG REV	EPN/DESCRIPTION	CONT/PE#	DATE	DRN	CHKD	APPR			

345kV AC LIGHT STRAIN 0-45°  
30-SCHSP-LSW-045  
LOAD & DESIGN DRAWING

SCALE: NTS  
FILE: TSP-33.DWG  
IMAGE:

DRAWING NO.: TSP-33-001  
DATE: 5/1/15